SAR EVALUATION REPORT

For

VeriFone Inc.

3755 Atherton Road
Rocklin, CA 95765

FCC ID: B32OMNI3600G

2003-07-17

This Report Concerns:	Equipment Type:
☒ Original Report	Wireless Point of Sale Terminal

Test Engineer:	Eric Hong
Report No.:	R0305223S
Test Date:	2003-07-11, 2003-07-14
Reviewed By:	Hans Mellberg
Prepared By:	Bay Area Compliance Laboratory Corporation 230 Commercial Street Sunnyvale, CA 94085 Tel: (408) 732-9162 Fax: (408) 732 9164

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SUMMARY

The US Federal Communications Commission has released the report and order “Guidelines for Evaluating the Environmental Effects of RF Radiation", ET Docket No. 93-62 in August 1996 [1].

The order requires routine SAR evaluation prior to equipment authorization of portable transmitter devices, including portable telephones. For consumer products, the applicable limit is 1.6 mW/g as recommended by the ANSI/IEEE standard C95.1-1992 [6] for an uncontrolled environment (Paragraph 65). According to the Supplement C of OET Bulletin 65 “Evaluating Compliance with FCC Guide-lines for Human Exposure to Radio frequency Electromagnetic Fields", released on Jun 29, 2001 by the FCC, the device should be evaluated at maximum output power (radiated from the antenna) under “worst-case” conditions for normal or intended use, incorporating normal antenna operating positions, device peak performance frequencies and positions for maximum RF energy coupling.

This report describes the methodology and results of experiments performed on wireless data terminal. The objective was to determine if there is RF radiation and if radiation is found, what is the extent of radiation with respect to safety limits. SAR (Specific Absorption Rate) is the measure of RF exposure determined by the amount of RF energy absorbed by human body (or its parts) – to determine how the RF energy couples to the body or head which is a primary health concern for body worn devices. The limit below which the exposure to RF is considered safe by regulatory bodies in North America is 1.6 mW/g average over 1 gram of tissue mass.

The test configurations were laid out on a specially designed test fixture to ensure the reproducibility of measurements. Each configuration was scanned for SAR. Analysis of each scan was carried out to characterize the above effects in the device.

There was no SAR of any concern measured on the device for any of the investigated configurations.

1 - REFERENCE

[1] Federal Communications Commission, \Report and order: Guidelines for evaluating the environmental effects of radiofrequency radiation", Tech. Rep. FCC 96-326, FCC, Washington, D.C. 20554, 1996.

[2] David L. Means Kwok Chan, Robert F. Cleveland, \Evaluating compliance with FCC guidelines for human exposure to radiofrequency electromagnetic fields", Tech. Rep., Federal Communication Commission, O_ce of Engineering & Technology, Washington, DC, 1997.

[3] Thomas Schmid, Oliver Egger, and Niels Kuster, \Automated E-_eld scanning system for dosimetric assessments", IEEE Transactions on Microwave Theory and Techniques, vol. 44, pp. 105{113, Jan. 1996.

[4] Niels Kuster, Ralph K.astle, and Thomas Schmid, \ Dosimetric evaluation of mobile communications equipment with known precision", IEICE Transactions on Communications, vol. E80-B, no. 5, pp. 645{652, May 1997.

[5] CENELEC, \Considerations for evaluating of human exposure to electromagnetic fields (EMFs) from mobile telecommunication equipment (MTE) in the frequency range 30MHz - 6GHz", Tech. Rep., CENELEC, European Committee for Electrotechnical Standardization, Brussels, 1997.

[6] ANSI, ANSI/IEEE C95.1-1992: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz, The Institute of Electrical and Electronics Engineers, Inc., New York, NY 10017, 1992.

[7] Katja Pokovic, Thomas Schmid, and Niels Kuster, \Robust setup for precise calibration of E-field probes in tissue simulating liquids at mobile communications frequencies", in ICECOM _ 97, Dubrovnik, October 15{17, 1997, pp. 120-24.

[8] Katja Pokovic, Thomas Schmid, and Niels Kuster, \E-field probe with improved isotropy in brain simulating liquids", in Proceedings of the ELMAR, Zadar, Croatia, 23{25 June, 1996, pp. 172-175.

[9] Volker Hombach, Klaus Meier, Michael Burkhardt, Eberhard K. uhn, and Niels Kuster, \The depen-dence of EM energy absorption upon human head modeling at 900 MHz", IEEE Transactions on Microwave Theory and Techniques, vol. 44, no. 10, pp. 1865-1873, Oct. 1996.

[10] Klaus Meier, Ralf Kastle, Volker Hombach, Roger Tay, and Niels Kuster, \The dependence of EM energy absorption upon human head modeling at 1800 MHz", IEEE Transactions on Microwave Theory and Techniques, Oct. 1997, in press.

[11] W. Gander, Computermathematik, Birkhaeuser, Basel, 1992.

[12] W. H. Press, S. A. Teukolsky,W. T. Vetterling, and B. P. Flannery, Numerical Recepies in C, The Art of Scientific Computing, Second Edition, Cambridge University Press, 1992.Dosimetric Evaluation of Sample device, month 1998 9

[13] NIS81 NAMAS, \The treatment of uncertainity in EMC measurement", Tech. Rep., NAMAS Executive, National Physical Laboratory, Teddington, Middlesex, England, 1994.

[14] Barry N. Taylor and Christ E. Kuyatt, \Guidelines for evaluating and expressing the uncertainty of NIST measurement results", Tech. Rep., National Institute of Standards and Technology, 1994. Dosimetric Evaluation of Sample device, month 1998 10

2 - TESTING EQUIPMENT

2.1 Equipments List & Calibration Info

Type / Model	Cal. Date	S/N:
DASY3 Professional Dosimetric System	N/A	N/A
Robot RX60L	N/A	F00/5H31A1/A/01
Robot Controller	N/A	F01/5J72A1/A/01
Dell Computer Optiplex GX110	N/A	N/A
Pentium III, Windows NT	N/A	N/A
SPEAG EDC3	N/A	N/A
SPEAG DAE3	08/26/02	456
SPEAG E-Field Probe ET3DV6	08/26/02	1604
SPEAG Dummy Probe	N/A	N/A
SPEAG Generic Twin Phantom	N/A	N/A
SPEAG Light Alignment Sensor	N/A	278
SPEAG Validation Dipole D-1800-S-2	11/6/01	BCL-049
SPEAG Validation Dipole D900V2	9/3/02	122
Brain Equivalent Matter (800MHz)	Daily	N/A
Brain Equivalent Matter (1900MHz)	Daily	N/A
Muscle Equivalent Matter (800MHz)	Daily	N/A
Muscle Equivalent Matter (1900MHz)	Daily	N/A
Robot Table	N/A	N/A
Phone Holder	N/A	N/A
Phantom Cover	N/A	N/A
HP Spectrum Analyzer HP8593GM	6/20/02	3009A00791
Microwave Amp. 8349B	N/A	2644A02662
Power Meter HP436A	4/2/02	2709A29209
Power Sensor HP8482A	4/2/02	2349A08568
Signal Generator RS SMIQ O3	2/10/02	1084800403
Network Analyzer HP-8753ES	7/30/02	820079
Dielectric Probe Kit HP85070A	N/A	N/A
Hewlett Packard HP8566B Spectrum Analyzer	7/23/02	None
Hewlett Packard HP 7470A Plotter	7/23/02	None
A.H. System SAS0200 Horn Antenna	7/23/02	None
Com-Power AB-100 Dipole Antenna	7/23/02	None
Agilent E4419b	4/8/02	GB40202891
Agilent E4412a	4/8/02	US38486529

2.2 Equipment Calibration Certificate

Please see the attached file for detailed information.

Schmid & Partner
Engineering AG

Zeughausstrasse 43, 8004 Zurich, Switzerland, Phone +41 1 245 97 00, Fax +41 1 245 97 79

Calibration Certificate

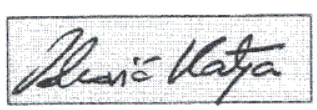
Dosimetric E-Field Probe

Type:	**ET3DV6**
Serial Number:	**1604**
Place of Calibration:	**Zurich**
Date of Calibration:	**August 26, 2002**
Calibration Interval	**12 months**

Schmid & Partner Engineering AG hereby certifies, that this device has been calibrated on the date indicated above. The calibration was performed in accordance with specifications and procedures of Schmid & Partner Engineering AG.

Wherever applicable, the standards used in the calibration process are traceable to international standards. In all other cases the standards of the Laboratory for EMF and Microwave Electronics at the Swiss Federal Institute of Technology (ETH) in Zurich, Switzerland have been applied.

Calibrated by 

Approved by 

Schmid & Partner
Engineering AG

Zeughausstrasse 43, 8004 Zurich, Switzerland, Telephone +41 1 245 97 00, Fax +41 1 245 97 79

Probe ET3DV6

SN:1604

Manufactured:	July 30, 2001
Last calibration:	September 7, 2001
Recalibrated:	August 26, 2002

Calibrated for System DASY3

ET3DV6 SN:1604 August 26, 2002

DASY3 - Parameters of Probe: ET3DV6 SN:1604

Sensitivity in Free Space

NormX	1.73 $\mu V/(V/m)^2$
NormY	1.68 $\mu V/(V/m)^2$
NormZ	1.72 $\mu V/(V/m)^2$

Diode Compression

DCP X	93	mV
DCP Y	93	mV
DCP Z	93	mV

Sensitivity in Tissue Simulating Liquid

Head	900 MHz	ε_r = 41.5 ± 5%	σ = 0.97 ± 5% mho/m
Head	835 MHz	ε_r = 41.5 ± 5%	σ = 0.90 ± 5% mho/m

ConvF X	**6.5** ± 9.5% (k=2)	Boundary effect:	
ConvF Y	**6.5** ± 9.5% (k=2)	Alpha	**0.36**
ConvF Z	**6.5** ± 9.5% (k=2)	Depth	**2.82**

Head	1800 MHz	ε_r = 40.0 ± 5%	σ = 1.40 ± 5% mho/m
Head	1900 MHz	ε_r = 40.0 ± 5%	σ = 1.40 ± 5% mho/m

ConvF X	**5.5** ± 9.5% (k=2)	Boundary effect:	
ConvF Y	**5.5** ± 9.5% (k=2)	Alpha	**0.50**
ConvF Z	**5.5** ± 9.5% (k=2)	Depth	**2.46**

Boundary Effect

Head **900 MHz** **Typical SAR gradient: 5 % per mm**

Probe Tip to Boundary		1 mm	2 mm
SAR_{be} [%]	Without Correction Algorithm	11.1	6.6
SAR_{be} [%]	With Correction Algorithm	0.4	0.6

Head **1800 MHz** **Typical SAR gradient: 10 % per mm**

Probe Tip to Boundary		1 mm	2 mm
SAR_{be} [%]	Without Correction Algorithm	12.3	8.1
SAR_{be} [%]	With Correction Algorithm	0.1	0.1

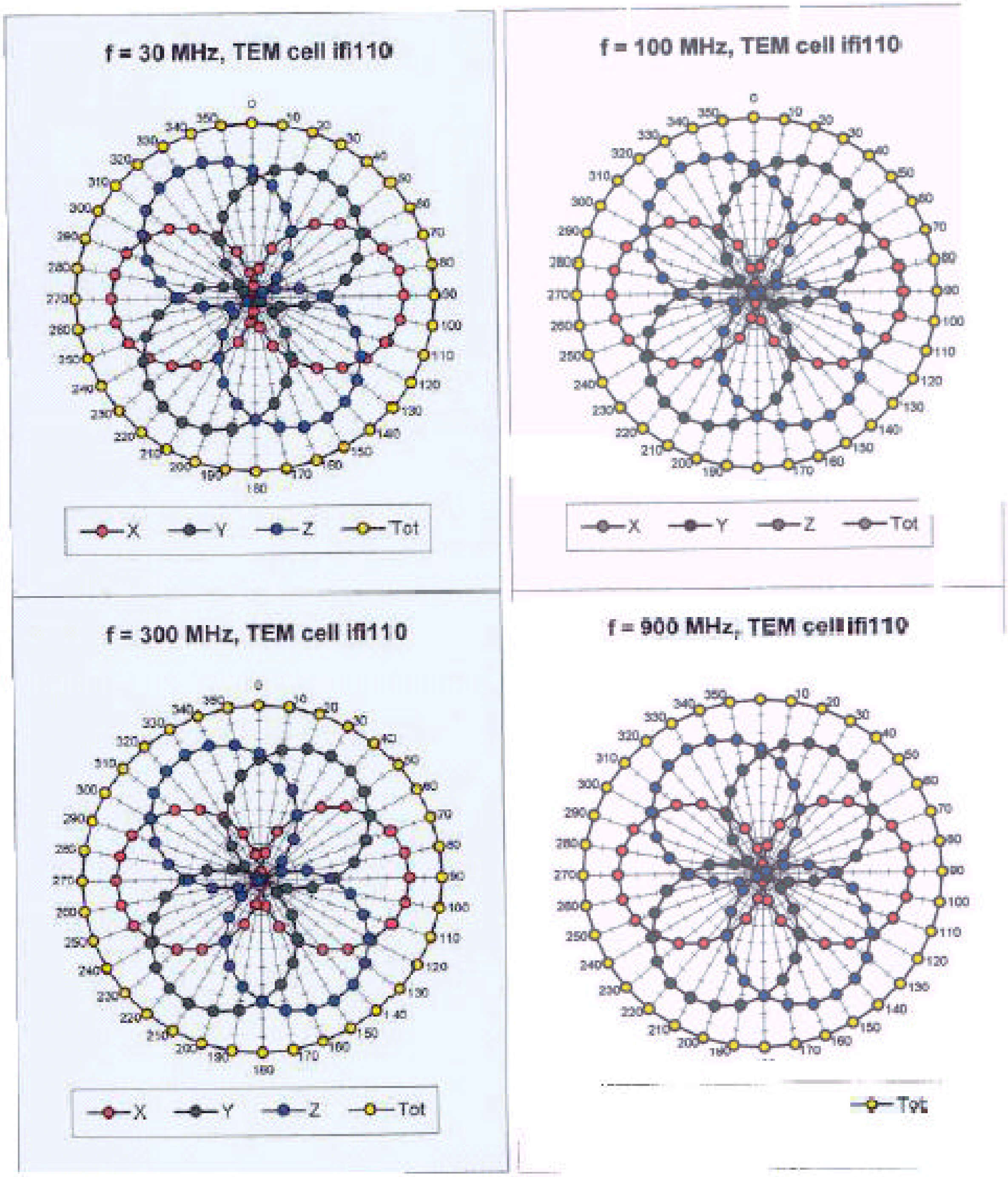
Sensor Offset

Probe Tip to Sensor Center	**2.7**	mm
Optical Surface Detection	**1.3 ± 0.2**	mm

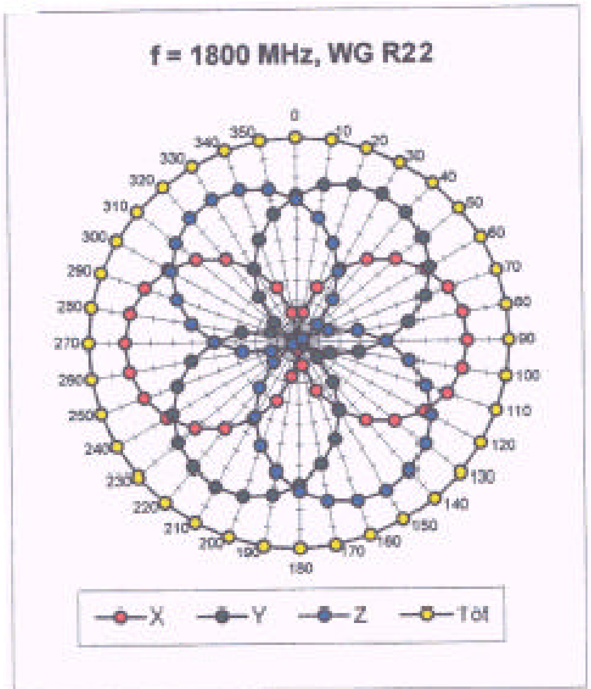
ET3DV6 SN:1604

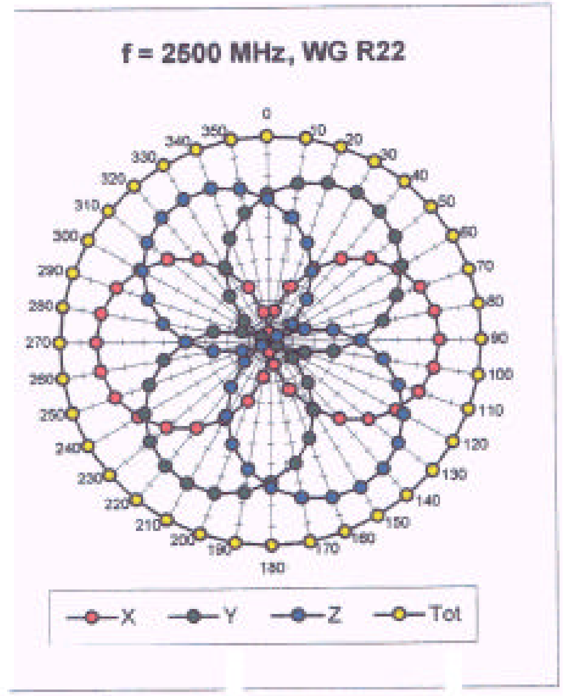
August 26, 2002

Receiving Pattern (ϕ), θ = 0°

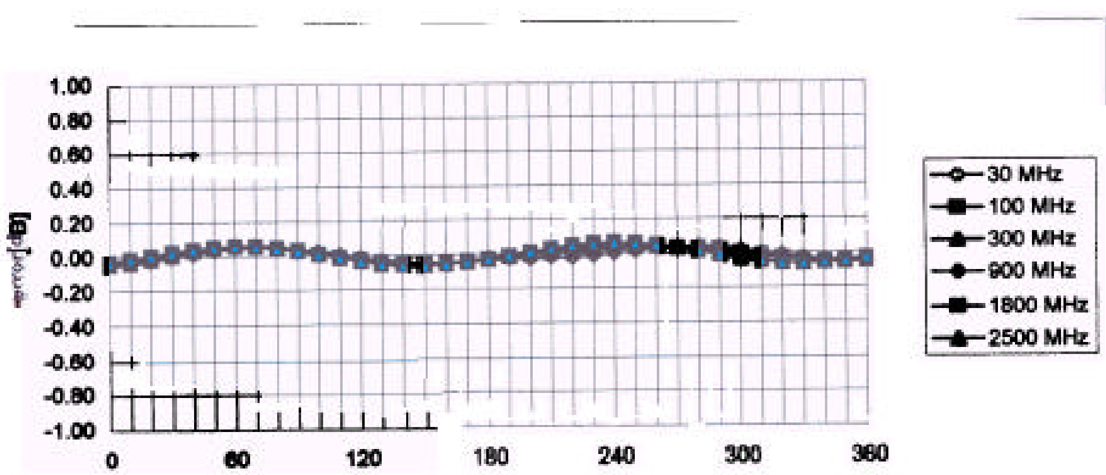


ET3DV6 SN:1604 **August 26, 2002**





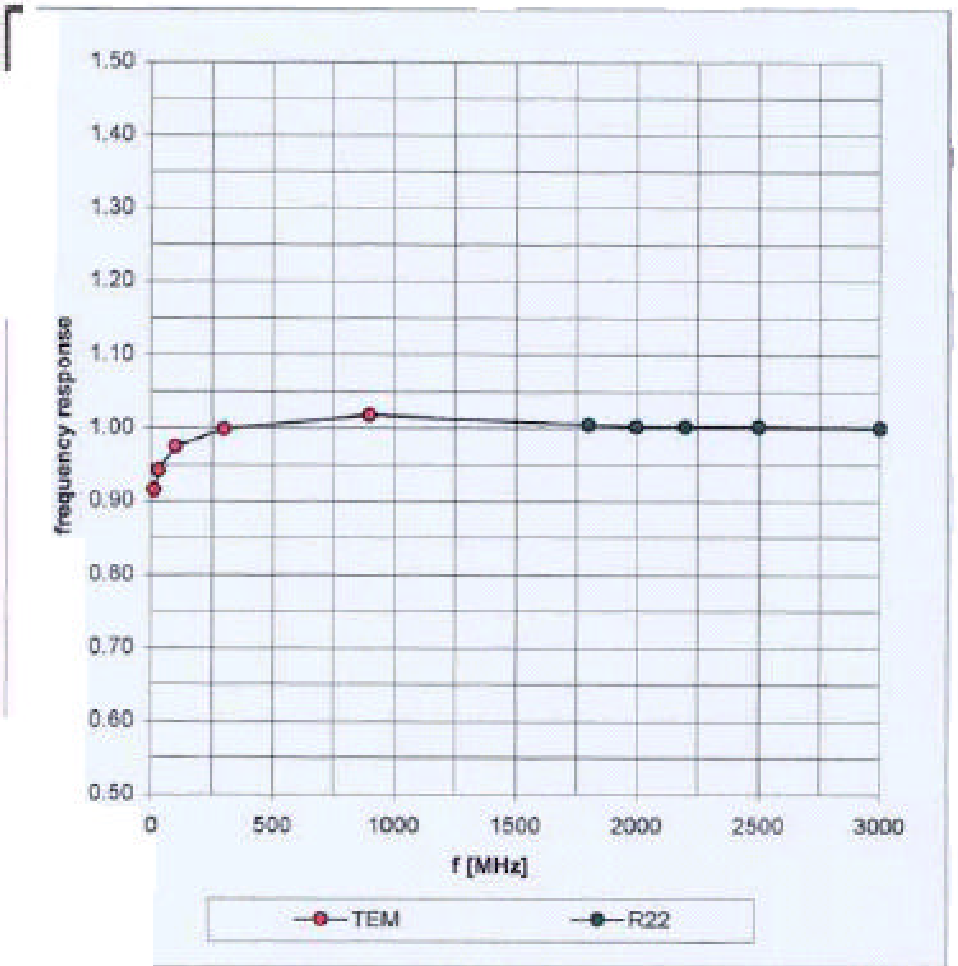
Isotropy Error (ϕ), θ = 0°



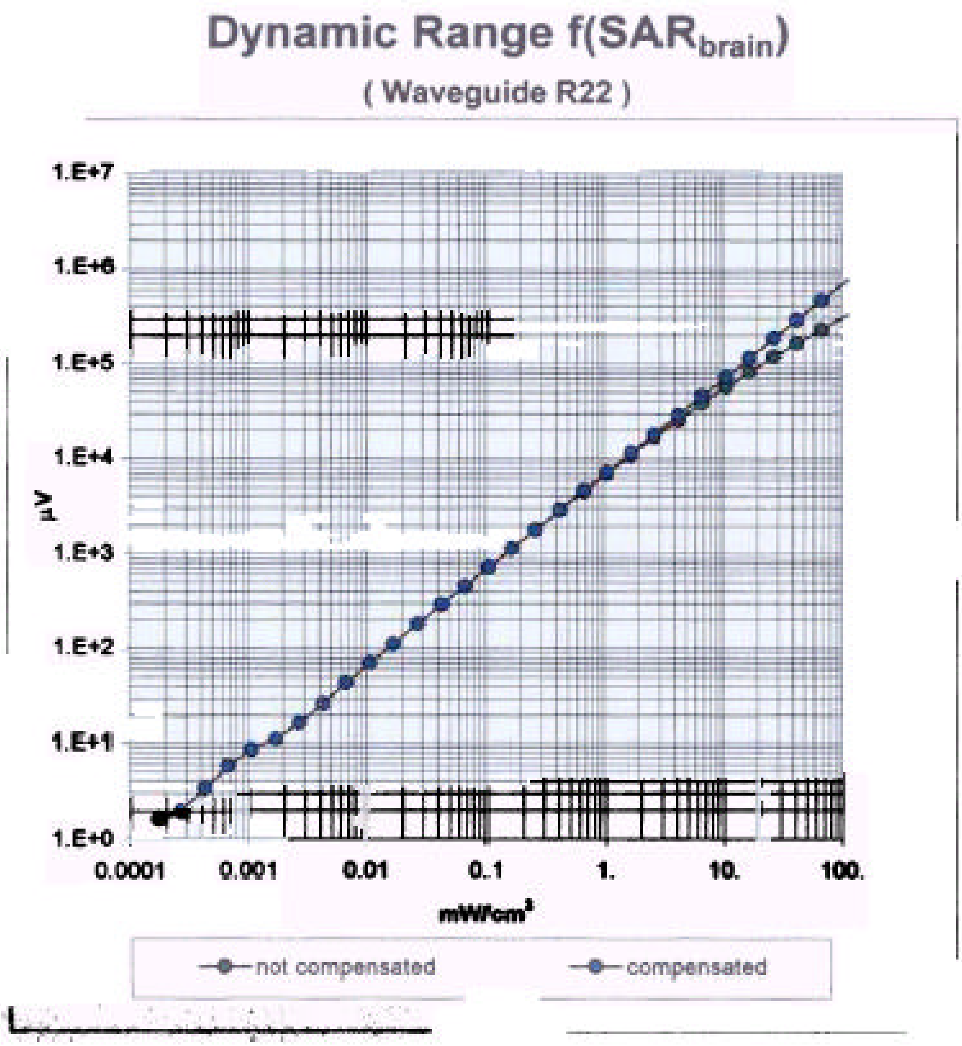
ET3DV6 SN:1604 August 26, 2002

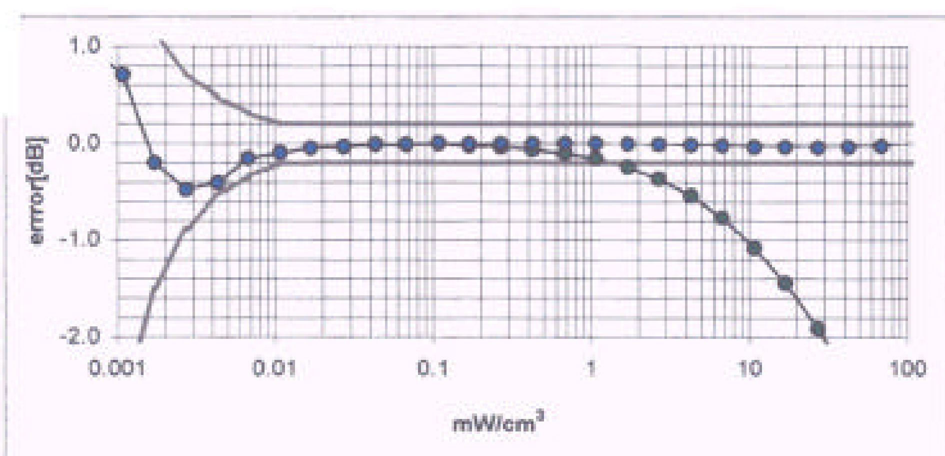
Frequency Response of E-Field

(TEM-Cell:ifi110, Waveguide R22)



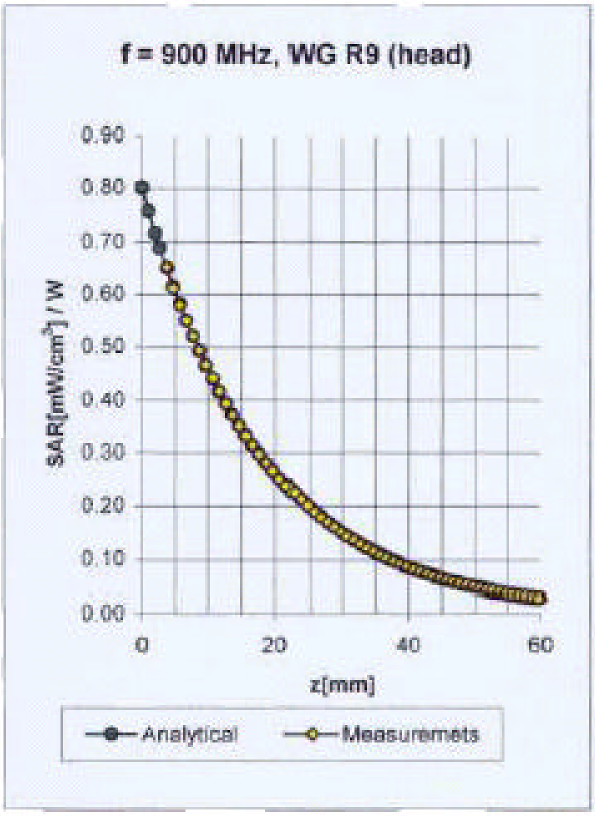
ET3DV6 SN:1604 August 26, 2002

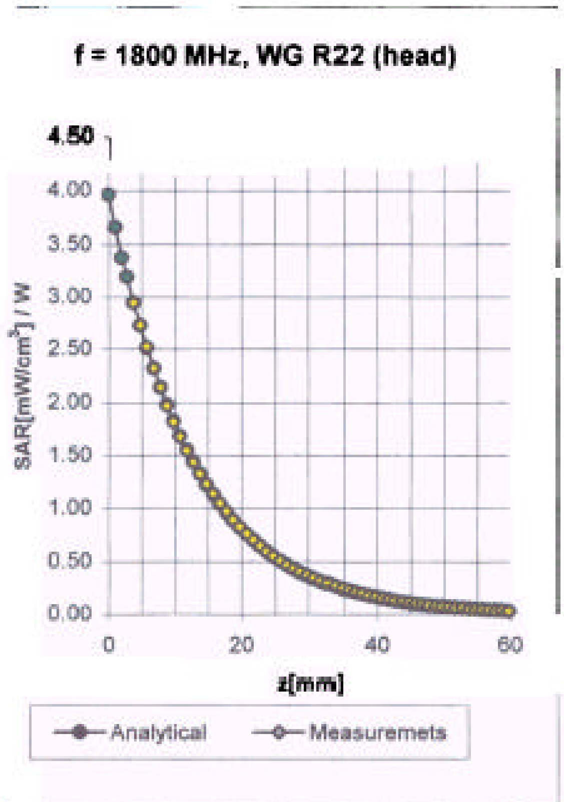




ET3DV6 SN:1604 **August 26, 2002**

Conversion Factor Assessment



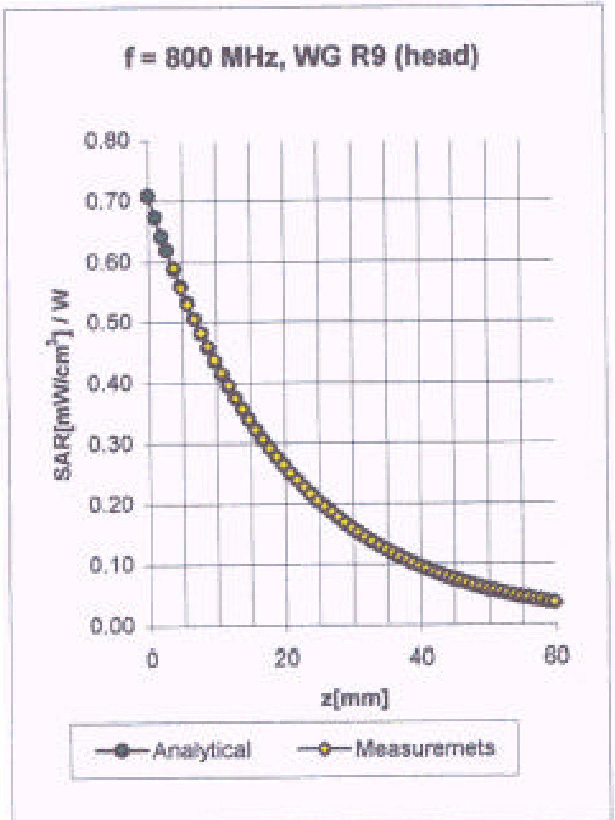


Head	900 MHz		ε_r = 41.5 ± 5%	σ = 0.97 ± 5% mho/m	
Head	835 MHz		ε_r = 41.5 ± 5%	σ = 0.90 ± 5% mho/m	
	ConvF X	**6.5** ± 9.5% (k=2)		Boundary effect:	
	ConvF Y	**6.5** ± 9.5% (k=2)		Alpha	
	ConvF Z	**6.5** ± 9.5% (k=2)		Depth	

Head	1800 MHz		ε_r = 40.0 ± 5%	σ = 1.40 ± 5% mho/m	
Head	1900 MHz		ε_r = 40.0 ± 5%	σ = 1.40 ± 5% mho/m	
	ConvF X	**5.5** ± 9.5% (k=2)		Boundary effect:	
	ConvF Y	**5.5** ± 9.5% (k=2)		Alpha	**0.50**
	ConvF Z	**5.5** ± 9.5% (k=2)		Depth	**2.46**

ET3DV6 SN:1604 August 26, 2002

Conversion Factor Assessment



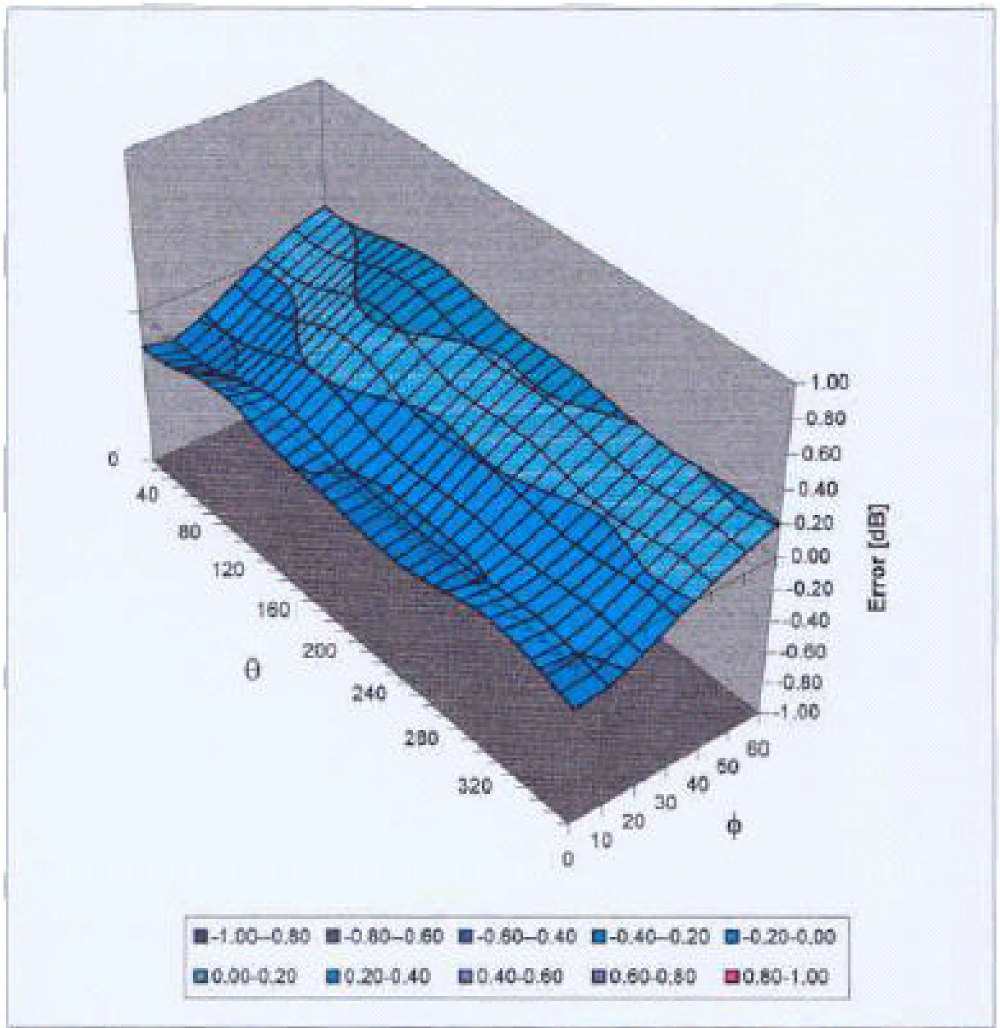
Head	800 MHz	ε_r = 41.5 ± 5%	σ = 0.88 ± 5% mho/m

ConvF X	**6.7** ± 8.9% (k=2)	Boundary effect:
ConvF Y	**6.7** ± 8.9% (k=2)	Alpha
ConvF Z	**6.7** ± 8.9% (k=2)	Depth

ET3DV6 SN:1604 **August 26, 2002**

Deviation from Isotropy in HSL

Error (θ,ϕ), f = 900 MHz



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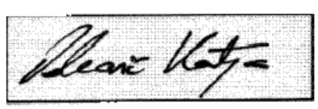
Additional Conversion Factors

for Dosimetric E-Field Probe

Type	ET3DV6
Serial Number:	1604
Place of Assessment	Zurich
Date of Assessment:	October 4, 2002
Probe Calibration Date	August 26, 2002

Schmid & Partner Engineering AG hereby certifies that conversion factor(s) of this probe have been evaluated on the date indicated above. The assessment was performed using the FDTD numerical code SEMCAD of Schmid & Partner Engineering AG. Since the evaluation is coupled with measured conversion factors, it has to be recalculated yearly, i.e., following the re-calibration schedule of the probe. The uncertainty of the numerical assessment is based on the extrapolation from measured value at 900 MHz or at 1800 MHz.

Assessed by



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Conversion factor (± standard deviation)

835 MHz	**ConvF**	**6.4 ± 8%**	ε_r = 55.2 ± 5% σ = 0.97 ± 5% mho/m (body tissue)
1900 MHz	**ConvF**	**4.9 ± 8%**	ε_r = 53.3 ± 5% σ = 1.52 ± 5% mho/m (body tissue)

835MHz Body Liquid Validation

frequency	e'	e''
800000000.0000	56.3000	22.4343
801000000.0000	56.2557	22.3793
802000000.0000	56.2522	22.4031
803000000.0000	56.2533	22.3533
804000000.0000	56.2025	22.3589
805000000.0000	56.2101	22.3580
806000000.0000	56.2116	22.3271
807000000.0000	56.1551	22.3028
808000000.0000	56.1488	22.2477
809000000.0000	56.1907	22.2763
810000000.0000	56.1773	22.2439
811000000.0000	56.1206	22.1917
812000000.0000	56.0592	22.1846
813000000.0000	56.1018	22.1420
814000000.0000	55.9775	22.1491
815000000.0000	55.9708	22.1653
816000000.0000	55.9394	22.0442
817000000.0000	55.9279	22.0865
818000000.0000	55.9173	22.0767
819000000.0000	55.9498	21.9975
820000000.0000	55.9214	22.0160
821000000.0000	55.8700	21.9997
822000000.0000	55.8853	21.9857
823000000.0000	55.8238	22.0030
824000000.0000	55.8710	21.9256
825000000.0000	55.7474	21.9572
826000000.0000	55.7130	21.9370
827000000.0000	55.6978	21.9440
828000000.0000	55.7422	21.9055
829000000.0000	55.6791	21.9009
830000000.0000	55.6310	21.9068
831000000.0000	55.5860	21.8834
832000000.0000	55.5858	21.8919
833000000.0000	55.5261	21.8579
834000000.0000	55.5372	21.8366
835000000.0000	55.5407	21.1533
836000000.0000	55.4695	21.7423
837000000.0000	55.4615	21.7876
838000000.0000	55.4683	21.7740
839000000.0000	55.4613	21.8554
840000000.0000	55.3921	21.7857
841000000.0000	55.3768	21.8163
842000000.0000	55.3768	21.7466
843000000.0000	55.3923	21.7745
844000000.0000	55.3179	21.7633
845000000.0000	55.3022	21.7757
846000000.0000	55.3406	21.7775
847000000.0000	55.3105	21.7885
848000000.0000	55.3005	21.8024
849000000.0000	55.3548	21.8505
850000000.0000	55.2766	21.8142

$s = w e_o e'' = 2 p f e_o e'' = 0.98$

where $f = 835 \times 10^6$

$e_o = 8.854 \times 10^{-12}$

$e'' = 21.1533$

835MHz Head Liquid Validation

frequency	e'	e''
800000000.0000	43.2949	19.6508
801000000.0000	43.3057	19.6936
802000000.0000	43.2904	19.6493
803000000.0000	43.3079	19.6554
804000000.0000	43.2202	19.6739
805000000.0000	43.2897	19.6509
806000000.0000	43.2293	19.6416
807000000.0000	43.1952	19.6346
808000000.0000	43.2085	19.6087
809000000.0000	43.2843	19.6758
810000000.0000	43.3085	19.6876
811000000.0000	43.2658	19.6378
812000000.0000	43.2472	19.6373
813000000.0000	43.2504	19.6281
814000000.0000	43.2565	19.6680
815000000.0000	43.2576	19.6638
816000000.0000	43.2253	19.6185
817000000.0000	43.2532	19.6495
818000000.0000	43.2709	19.6553
819000000.0000	43.2173	19.6398
820000000.0000	43.2505	19.5808
821000000.0000	43.1981	19.6192
822000000.0000	43.2153	19.6544
823000000.0000	43.2079	19.6494
824000000.0000	43.2764	19.6260
825000000.0000	43.2084	19.6459
826000000.0000	43.2382	19.6299
827000000.0000	43.2370	19.6599
828000000.0000	43.1946	19.6402
829000000.0000	43.2356	19.5906
830000000.0000	43.2225	19.6419
831000000.0000	43.1904	19.6265
832000000.0000	43.1937	19.5965
833000000.0000	43.1164	19.5915
834000000.0000	43.1214	19.5857
835000000.0000	43.0883	19.5874
836000000.0000	43.1022	19.6028
837000000.0000	43.1115	19.5870
838000000.0000	43.0318	19.5751
839000000.0000	43.0664	19.5407
840000000.0000	43.0047	19.5421
841000000.0000	43.0132	19.5144
842000000.0000	43.0101	19.5081
843000000.0000	43.0354	19.5309
844000000.0000	43.0172	19.5472
845000000.0000	42.9937	19.5410
846000000.0000	43.0026	19.4847
847000000.0000	43.0086	19.5195
848000000.0000	42.9795	19.4995
849000000.0000	42.9513	19.4425
850000000.0000	42.9201	19.5539

$s = w e_o e'' = 2 p f e_o e'' = 0.91$

where $f = 835x\,10^{6}$

$e_o = 8.854 \times 10^{-12}$

$e'' = 19.5874$

1900MHz Body Liquid Validation

frequency	e'	e''
1875000000.0000	53.1688	13.3440
1876000000.0000	53.1586	13.3327
1877000000.0000	53.1448	13.3351
1878000000.0000	53.0899	13.3103
1879000000.0000	53.0674	13.3176
1880000000.0000	53.0561	13.3162
1881000000.0000	53.0263	13.3186
1882000000.0000	53.0386	13.3382
1883000000.0000	53.0149	13.3233
1884000000.0000	53.0148	13.3132
1885000000.0000	52.9961	13.3069
1886000000.0000	52.9912	13.3203
1887000000.0000	52.9712	13.2918
1888000000.0000	52.9864	13.3398
1889000000.0000	52.9652	13.3373
1890000000.0000	52.9429	13.3285
1891000000.0000	52.9405	13.3382
1892000000.0000	52.9382	13.3639
1893000000.0000	52.9233	13.3440
1894000000.0000	52.9170	13.3191
1895000000.0000	52.8815	13.3389
1896000000.0000	52.8891	13.3657
1897000000.0000	52.8917	13.3680
1898000000.0000	52.8622	13.3704
1899000000.0000	52.8911	13.4057
1900000000.0000	52.8628	13.4144
1901000000.0000	52.8346	13.4229
1902000000.0000	52.8386	13.4312
1903000000.0000	52.8572	13.4172
1904000000.0000	52.8516	13.4404
1905000000.0000	52.8502	13.4080
1906000000.0000	52.8448	13.4473
1907000000.0000	52.8601	13.4789
1908000000.0000	52.8787	13.4648
1909000000.0000	52.8890	13.4718
1910000000.0000	52.8857	13.4751
1911000000.0000	52.8469	13.5085
1912000000.0000	52.8743	13.5053
1913000000.0000	52.8811	13.5258
1914000000.0000	52.8680	13.5281
1915000000.0000	52.8795	13.5330
1916000000.0000	52.8777	13.5505
1917000000.0000	52.8905	13.5536
1918000000.0000	52.9079	13.5331
1919000000.0000	52.8821	13.5880
1920000000.0000	52.8874	13.5862
1921000000.0000	52.8793	13.5519
1922000000.0000	52.8987	13.6065
1923000000.0000	52.9424	13.6109
1924000000.0000	52.9204	13.6312
1925000000.0000	52.9514	13.6060

$s = w e_o e'' = 2 p f e_o e'' = 1.42$

where $f = 1900 \times 10^6$

$e_o = 8.854 \times 10^{-12}$

$e'' = 13.4144$

1900MHz Head Liquid Validation

frequency	e'	e''
1875000000.0000	40.6477	12.9164
1876000000.0000	40.6833	12.9153
1877000000.0000	40.6628	12.8982
1878000000.0000	40.6298	12.8220
1879000000.0000	40.6597	12.7749
1880000000.0000	40.6381	12.7278
1881000000.0000	40.6707	12.7065
1882000000.0000	40.6516	12.7539
1883000000.0000	40.6067	12.7697
1884000000.0000	40.6278	12.7541
1885000000.0000	40.6032	12.7385
1886000000.0000	40.6100	12.7372
1887000000.0000	40.5968	12.7502
1888000000.0000	40.5921	12.7718
1889000000.0000	40.5961	12.7105
1890000000.0000	40.5858	12.6864
1891000000.0000	40.5841	12.6879
1892000000.0000	40.5368	12.6895
1893000000.0000	40.5122	12.7994
1894000000.0000	40.4703	12.8351
1895000000.0000	40.4743	12.8538
1896000000.0000	40.4555	12.8781
1897000000.0000	40.4623	12.9339
1898000000.0000	40.4492	12.9640
1899000000.0000	40.4133	12.9711
1900000000.0000	40.4146	12.9298
1901000000.0000	40.4159	12.9626
1902000000.0000	40.4201	12.9699
1903000000.0000	40.3530	12.9228
1904000000.0000	40.3999	12.8929
1905000000.0000	40.4041	12.8603
1906000000.0000	40.3714	12.9159
1907000000.0000	40.5841	13.0852
1908000000.0000	40.6482	13.1010
1909000000.0000	40.6610	13.1053
1910000000.0000	40.6168	13.1268
1911000000.0000	40.6555	13.1679
1912000000.0000	40.6742	13.1950
1913000000.0000	40.6641	13.1992
1914000000.0000	40.5656	13.2296
1915000000.0000	40.3925	13.1371
1916000000.0000	40.4771	13.2435
1917000000.0000	40.2671	13.0205
1918000000.0000	40.2575	13.0698
1919000000.0000	40.2219	12.9804
1920000000.0000	40.2165	12.9832
1921000000.0000	40.2122	12.9563
1922000000.0000	40.2351	12.9619
1923000000.0000	40.2182	12.9676
1924000000.0000	40.2240	12.9959
1925000000.0000	40.2142	13.0031

$s = w e_o e'' = 2 p f e_o e'' = 1.37$

where $f = 1900 \times 10^6$

$e_o = 8.854 \times 10^{-12}$

$e'' = 12.9298$

3 - EUT DESCRIPTION

Applicant:	VeriFone Inc.
Product Description:	Wireless Point of Sale Terminal
Product Model Number:	OMNI 3600G
FCC ID:	B32OMNI3600G
Serial Number:	None
Maximum RF Output Power:	23.67 dBm for PMS
	27.65 dBm for PCS
RF Exposure environment:	General Population/Uncontrolled
Applicable Standard	FCC CFR 47, Part 22, & 24
Application Type:	Certification

4 - SYSTEM TEST CONFIGURATION

4.1 Justification

The system was configured for testing in a typical fashion (as normally used by a typical user).

4.2 EUT Exercise Procedure

The EUT exercising program used during SAR testing was designed to exercise the various system components in a manner similar to a typical use. The EUT was tested by pushing the PTT bottom during the testing.

4.3 Equipment Modifications

No modification(s) were made to ensure that the EUT complies with the applicable limits.

5 – CONDUCTED OUTPUT POWER MEASUREMENTS

5.1 Provision Applicable

According to §15.247(b) (3), for systems using digital modulation, the maximum peak output power of the intentional radiator shall not exceed 1 Watt.

According to FCC §22.913 (a), the ERP of mobile transmitters and auxiliary test transmitters must not exceed 7 watts. According to FCC § 24.232(b), EIRP peak power for mobile/portable stations are limited to 2 watts.

5.2 Test Procedure

The RF output of the transmitter was connected to the input of the spectrum analyzer through sufficient attenuation.

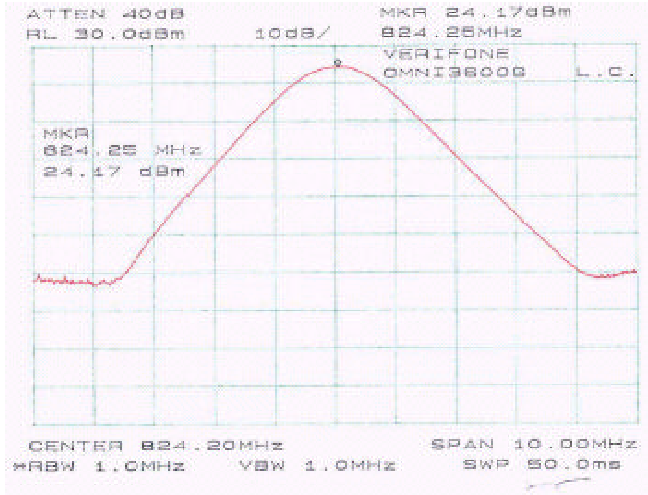
5.3 Test equipment

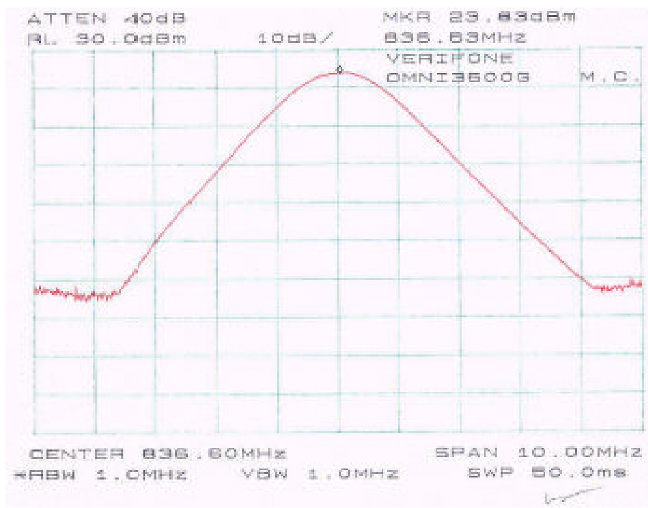
Hewlett Packard HP8564E Spectrum Analyzer, Calibration Due Date: 2003-08-01.
Hewlett Packard HP 7470A Plotter, Calibration not required.
A.H. Systems SAS200 Horn Antenna, Calibration Due Date: 2003-05-31
Com-Power AB-100 Dipole Antenna, Calibration Due Date: 2003-09-05

5.4 Test Results

Modulation Type	Channel	Frequency (MHz)	Output Power in dBm	Output Power in W	Limit (W)
PMS	Low	824.25	24.17	0.261	7
	Middle	836.63	23.83	0.242	7
	High	848.82	23.67	0.233	7
PCS	Low	1850.20	27.17	0.521	2
	Middle	1880.00	28.00	0.631	2
	High	1909.87	28.33	0.681	2

Please refer to the following plots.


ATTEN 40dB
RL 30.0dBm
10dB/
MKR 24.17dBm
824.25MHz
VERIFONE
OMNI3600G
L.C.
MKR
824.25 MHz
24.17 dBm
CENTER 824.20MHz
SPAN 10.00MHz
*RBW 1.0MHz
VBW 1.0MHz
SWP 50.0ms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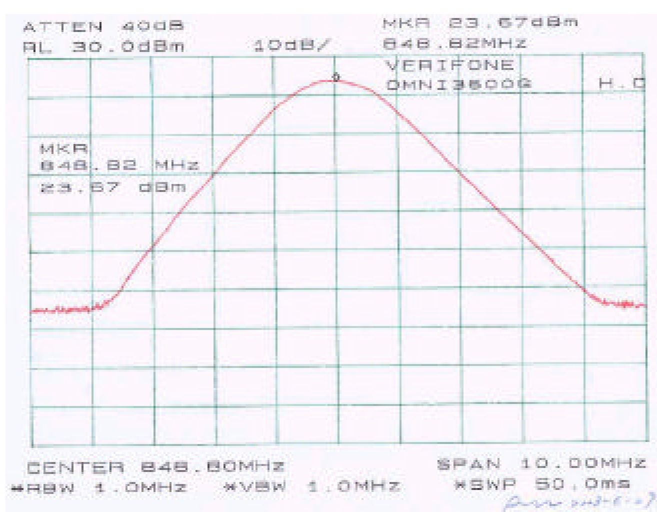
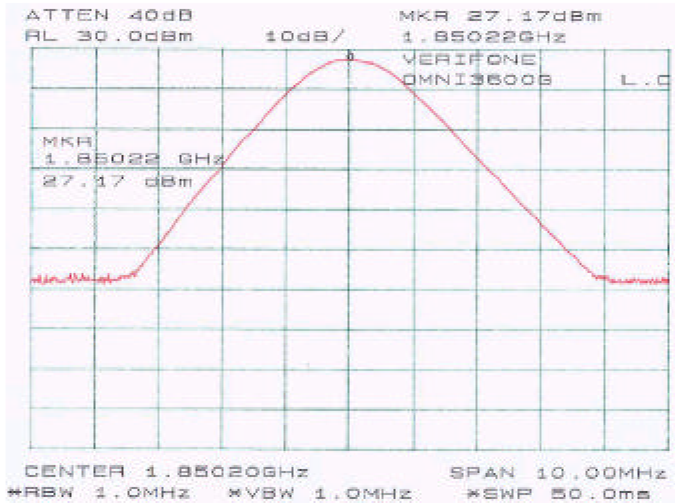
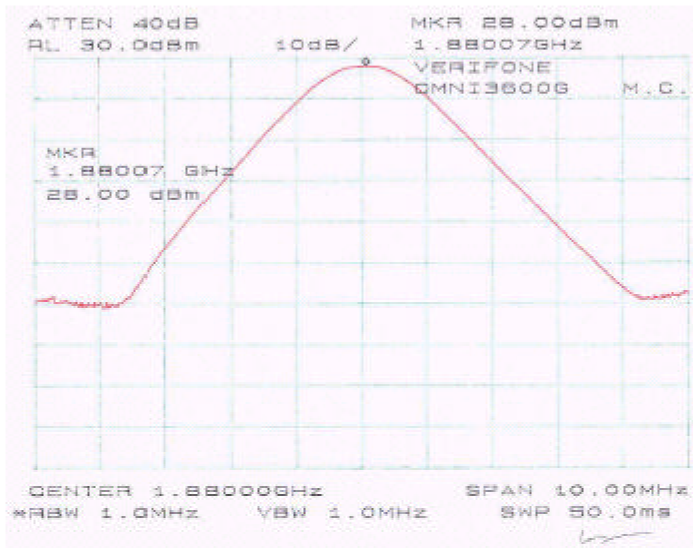
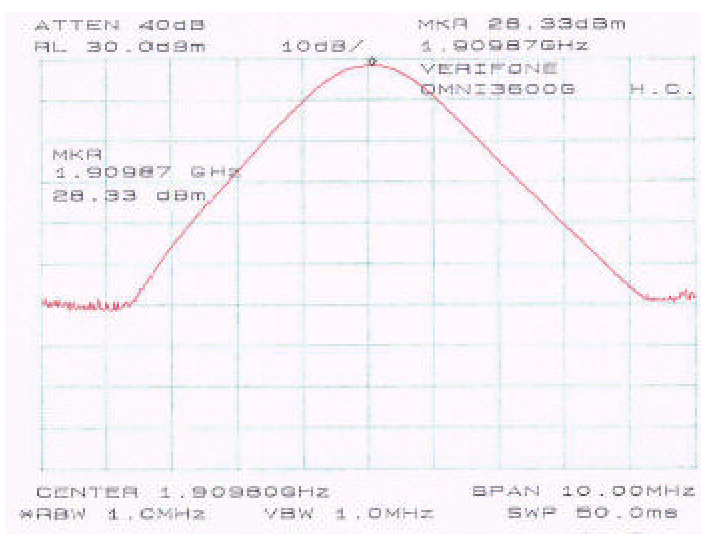
RL 30.0dBm
10dB/
MKR 23.83dBm
836.63MHz
VERIFONE
OMNI3600G
M.C.
CENTER 836.60MHz
SPAN 10.00MHz
*RBW 1.0MHz
VBW 1.0MHz
SWP 50.0ms


ATTEN 40dB
RL 30.0dBm
10dB/
MKR 23.67dBm
848.82MHz
VERIFONE
OMNI3600G
H.C
MKR
848.82 MHz
23.67 dBm
CENTER 848.80MHz
SPAN 10.00MHz
*RBW 1.0MHz
*VBW 1.0MHz
*SWP 50.0ms


ATTEN 40dB
RL 30.0dBm
10dB/
MKR 27.17dBm
1.85022GHz
VERIFONE
OMNI3600G
L.C
MKR
1.85022 GHz
27.17 dBm
CENTER 1.85020GHz
SPAN 10.00MHz
*RBW 1.0MHz
*VBW 1.0MHz
*SWP 50.0ms


ATTEN 40dB
RL 30.0dBm
10dB/
MKR 28.00dBm
1.88007GHz
VERIFONE
OMNI3600G
M.C.
MKR
1.88007 GHz
28.00 dBm
CENTER 1.88000GHz
SPAN 10.00MHz
*RBW 1.0MHz
VBW 1.0MHz
SWP 50.0ms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10dB/
MKR 28.33dBm
1.90987GHz
VERIFONE
OMNI3600G
H.C.
MKR
1.90987 GHz
28.33 dBm
CENTER 1.90980GHz
SPAN 10.00MHz
*RBW 1.0MHz
VBW 1.0MHz
SWP 50.0ms

6 - DOSIMETRIC ASSESSMENT SETUP

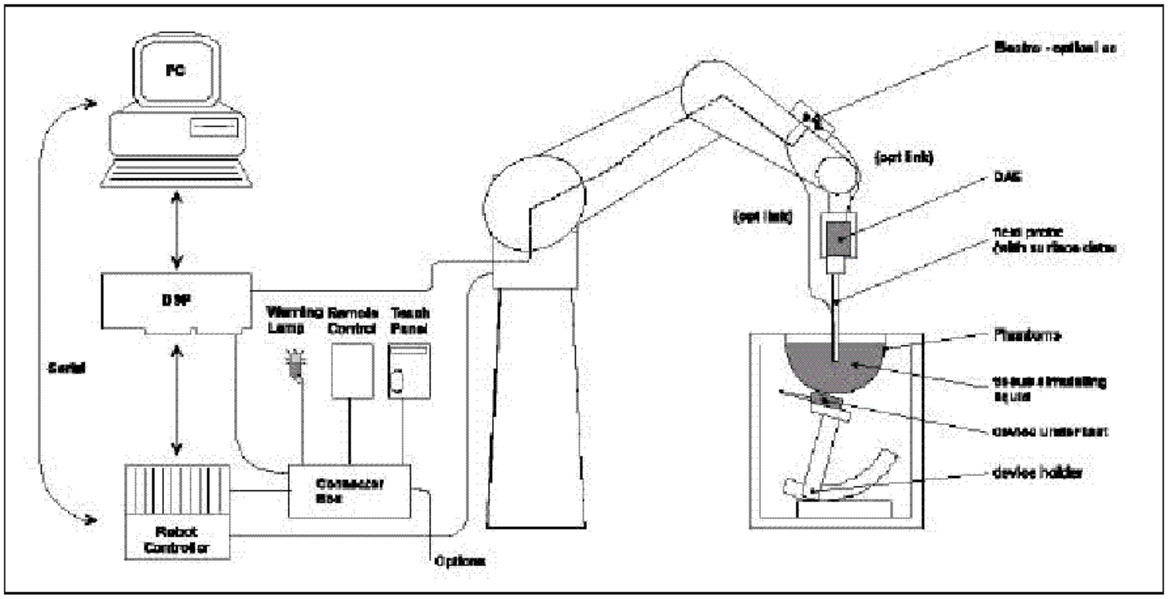
These measurements were performed with the automated near-field scanning system DASY3 from Schmid & Partner Engineering AG (SPEAG). The system is based on a high precision robot (working range greater than 0.9m) which positions the probes with a positional repeatability of better than ±0.02mm. Special E- and H-field probes have been developed for measurements close to material discontinuity, the sensors of which are directly loaded with a Schottky diode and connected via highly resistive lines to the data acquisition unit. The system is described in detail in [3].

The SAR measurements were conducted with the dosimetric probe ET3DV6 SN: 1577 (manufactured by SPEAG), designed in the classical triangular configuration [3] and optimized for dosimetric evaluation. The probe has been calibrated according to the procedure described in [7] with accuracy of better than ±10%. The spherical isotropy was evaluated with the procedure described in [8] and found to be better than ±0.25dB.

The phantom used was the \Generic Twin Phantom” described in [4]. The ear was simulated as a spacer of 4 mm thickness between the earpiece of the phone and the tissue simulating liquid. The Tissue simulation liquid used for each test is in according with the FCC OET65 supplement C as listed below.

Ingredients (% by weight)	Frequency (MHz)									
	450		835		915		1900		2450	
Tissue Type	Head	Body	Head	Body	Head	Body	Head	Body	Head	Body
Water	38.56	51.16	41.45	52.4	41.05	56.0	54.9	40.4	62.7	73.2
Salt (Nacl)	3.95	1.49	1.45	1.4	1.35	0.76	0.18	0.5	0.5	0.04
Sugar	56.32	46.78	56.0	45.0	56.5	41.76	0.0	58.0	0.0	0.0
HEC	0.98	0.52	1.0	1.0	1.0	1.21	0.0	1.0	0.0	0.0
Bactericide	0.19	0.05	0.1	0.1	0.1	0.27	0.0	0.1	0.0	0.0
Triton x-100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	36.8	0.0
DGBE	0.0	0.0	0.0	0.0	0.0	0.0	44.92	0.0	0.0	26.7
Dielectric Constant	43.42	58.0	42.54	56.1	42.0	56.8	39.9	54.0	39.8	52.5
Conductivity (s/m)	0.85	0.83	0.91	0.95	1.0	1.07	1.42	1.45	1.88	1.78

6.1 Measurement System Diagram

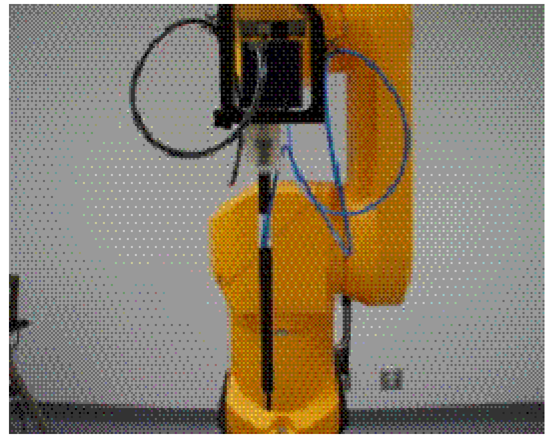


The DASY3 system for performing compliance tests consist of the following items:

1. A standard high precision 6-axis robot (Stäubli RX family) with controller and software.
2. An arm extension for accommodating the data acquisition electronics (DAE).
3. A dosimetric probe, i.e., an isotropic E-field probe optimized and calibrated for usage in tissue simulating liquid. The probe is equipped with an optical surface detector system.
4. A data acquisition electronic (DAE), which performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. The unit is battery powered with standard or rechargeable batteries. The signal is optically transmitted to the EOC.
5. A unit to operate the optical surface detector, which is connected to the EOC. The Electro-optical coupler (EOC) performs the conversion from the optical into a digital electric signal of the DAE. The EOC is connected to the PC plug-in card. The functions of the PC plug-in card based on a DSP is to perform the time critical task such as signal filtering, surveillance of the robot operation fast movement interrupts.
6. A computer operating Windows 95 or larger
7. DASY3 software
8. Remote control with teaches pendant and additional circuitry for robot safety such as warning lamps, etc.
9. The generic twin phantom enabling testing left-hand and right-hand usage.
10. The device holder for handheld EUT.
11. Tissue simulating liquid mixed according to the given recipes (see Application Note).
12. System validation dipoles to validate the proper functioning of the system.

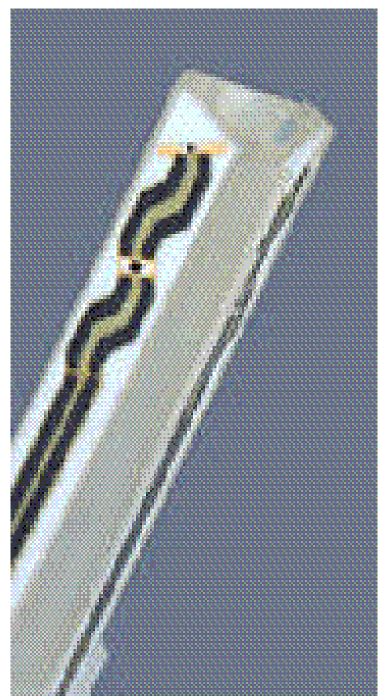
6.2. System Components

ET3DV6 Probe Specification
Construction Symmetrical design with triangular core
Built-in optical fiber for surface detection System
Built-in shielding against static charges
Calibration In air from 10 MHz to 2.5 GHz
In brain and muscle simulating tissue at
Frequencies of 450 MHz, 900 MHz and
1.8 GHz (accuracy ± 8%)
Frequency 10 MHz to > 6 GHz; Linearity: ± 0.2 dB
(30 MHz to 3 GHz)
Directivity ± 0.2 dB in brain tissue (rotation around
probe axis)
± 0.4 dB in brain tissue (rotation normal probe axis)
Dynamic 5 mW/g to > 100 mW/g;
Range Linearity: ± 0.2 dB
Surface ± 0.2 mm repeatability in air and clear liquids
Detection over diffuse reflecting surfaces.
Dimensions Overall length: 330 mm
Tip length: 16 mm
Body diameter: 12 mm
Tip diameter: 6.8 mm
Distance from probe tip to dipole centers: 2.7 mm
Application General dosimetric up to 3 GHz
Compliance tests of mobile phones
Fast automatic scanning in arbitrary phantoms



Photograph of the probe

The SAR measurements were conducted with the dosimetric probe ET3DV6 designed in the classical triangular configuration and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multi-fiber line ending at the front of the probe tip. It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY3 software reads the reflection during a software approach and looks for the maximum using a 2 nd order fitting. The approach is stopped when reaching the maximum.



Inside view of ET3DV6 E-field Probe

E-Field Probe Calibration Process

Each probe is calibrated according to a dosimetric assessment procedure described in [6] with accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure described in [7] and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe are tested.

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies bellow 1 GHz, and in a waveguide above 1 GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity and at the proper orientation with the field. The probe is then rotated 360 degrees.

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium correlates to temperature rise in dielectric medium. For temperature correlation calibration a RF transparent thermistor-based temperature probe is used in conjunction with the E-field probe.

Data Evaluation

The DASY3 software automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software:

Probe Parameter:	-Sensitivity	$Norm_i$, a_{i0}, a_{i1}, a_{i2}
	-Conversion Factor	ConvFi
	-Diode compression point	Dcp_i
Device parameter:	-Frequency	f
	-Crest Factor	cf
Media parameter:	-Conductivity	ó
	-Density	ñ

These parameters must be set correctly in the software. They can either be found in the component documents or be imported into the software from the configuration files issued for the DASY3 components. In the direct measuring mode of the multi-meter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as:

$$Vi = Ui + (Ui)^2 \, cf / dcp_i$$

With Vi = compensated signal of channel i (i =x, y, z)
Ui = input signal of channel i (i =x, y, z)
cf = crest factor of exciting field (DASY parameter)
dcp_i = diode compression point (DASY parameter)

From the compensated input signals the primary field data for each channel can be evaluated:

E-field probes: $$E_i = \sqrt{\frac{V_i}{Norm_i \cdot ConvF}}$$

H-field probes: $$H_i = \sqrt{Vi} \cdot \frac{a_{i0} + a_{i1} f + a_{i2} f^2}{f}$$

With Vi = compensated signal of channel i (i =x, y, z)
$Norm_i$ = sensor sensitivity of channel i (i =x, y, z)
ìV/ $(V/m)^2$ for E-field probes
ConF = sensitivity enhancement in solution
a_{ij} = sensor sensitivity factors for H-field probes
f = carrier frequency [GHz]
Ei = electric field strenggy of channel i in V/m
H_i = diode compression point (DASY parameter)

The RSS value of the field components gives the total field strength (Hermitian magnitude):

E_{tot} = Square Root $[(E_x)^2 + (E_y)^2 + (E_z)^2]$

The primary field data are used to calculate the derived field units.

SAR = $(E_{tot})^2$ ó/(ñ 1000)

With SAR = local specific absorption rate in mW/g
E_{tot} = total field strength in V/m
ó = conductivity in [mho/m] or [Siemens/m]
ñ = equivalent tissue density in g/cm^3

Note that the density is normally set to 1 (or 1.06), to account for actual brain density rather than the density of the simulation liquid.

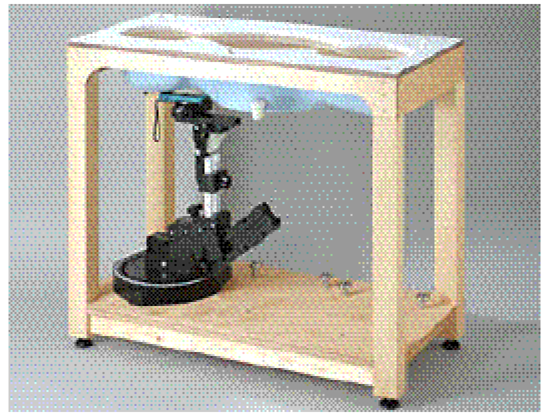
The power flow density is calculated assuming the excitation field as a free space field.

$P_{pwe} = (E_{tot})^2 / 3770$ or $P_{pwe} = (H_{tot})2$ 37.7

With P_{pwe} = equivalent power density of a plane wave in mW/cm3
E_{tot} = total electric filed strength in V/m
H_{tot} = total magnetic filed strength in V/m

Generic Twin Phantom

The Generic Twin Phantom is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least 90% of all users [9][10]. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid. Reference markings on the Phantom allows the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot.
Shell Thickness 2 ± 0.1 mm
Filling Volume Approx. 20 liters
Dimensions 810 x 1000 x 500 mm (H x L x W)

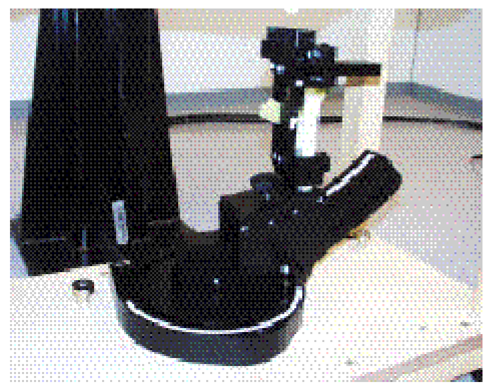


Generic Twin Phantom

Device Holder

In combination with the Generic Twin Phantom V3.0, the Mounting Device enables the rotation of the mounted transmitter in spherical coordinates whereby the rotation points is the ear opening. The devices can be easily, accurately, and repeatedly positioned according to the FCC and CENELEC specifications. The device holder can be locked at different phantom locations (left head, right head, flat phantom).

* Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produced infinite number of configurations [10]. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.



Device Holder

6.3 Measurement Uncertainty

The uncertainty budget has been determined for the DASY3 measurement system according to the NIS81 [13] and the NIST1297 [14] documents and is given in the following Table.

Measurement Uncertainty Analysis per IEEE P1528-2002								
Description	Section	Reported Variance (%)	Probability Distribution type	Divisor	Ci (1g)	Ui (1g)	Vi	welc/satt series term
Probe Calibration	E.2.1	4.80	N	1	1	4.80	1.00E+09	5.30842E-07
Axial isotropy	E.2.2	4.70	R	1.732	0.707107	1.92	1.00E+09	1.35563E-08
Hemispherical isotropy	E.2.2	9.60	R	1.732	0.707107	3.92	1.00E+09	2.35957E-07
Boundary effects	E.2.3	8.30	R	1.732	1	4.79	1.00E+09	5.27377E-07
Linearity	E.2.4	4.70	R	1.732	1	2.71	1.00E+09	5.4225E-08
System Detection Limit	E.2.5	1.00	R	1.732	1	0.58	1.00E+09	1.11124E-10
Readout Electronics	E.2.6	0.00	N	1	1	0.00	1.00E+09	0
Response time	E.2.7	0.00	R	1.732	1	0.00	1.00E+09	0
Integration time	E.2.8	0.00	R	1.732	1	0.00	1.00E+09	0
RF Ambient conditions	E.6.1	3.00	R	1.732	1	1.73	1.00E+09	9.00106E-09
Probe positioning mechanical tolerance	E.6.2	0.40	R	1.732	1	0.23	1.00E+09	2.84478E-12
Probe positioning wrt phantom shell	E.6.3	2.90	R	1.732	1	1.67	1.00E+09	7.8596E-09
Extra/inter-polation & integration algorithmsfor max SAR evaluation	E.5.2	3.90	R	1.732	1	2.25	1.00E+09	2.57079E-08
Test sample positioning	8, E.4.2	6.00	R	1.732	1	3.46	1.00E+09	1.44017E-07
Device holder distance tolerance	E.4.1	5.00	N	1	1	5.00	1.00E+09	0.000000625
Output power and SAR drift measurement	8, E.6.6.2	5.00	R	1.732	1	2.89	1.00E+09	6.94526E-08
Phantom uncertainty, shell thickness tolerance	E.3.1	4.00	R	1.732	1	2.31	1.00E+09	2.84478E-08
Liquid conductivity, deviation from target values	E.3.2	5.00	R	1.732	0.64	1.85	1.00E+09	1.16522E-08
Liquid conductivity, measurement uncertainty	E.3.3	5.00	N	1	0.64	3.20	5	20.97152
Liquid permitivity, deviation from target values	E.3.2	5.00	R	1.732	0.6	1.73	1.00E+09	9.00106E-09
Liquid permitivity, measurement uncertainty	E.3.3	5.00	N	1	0.6	3.00	5	16.2
								689
Probe isotropy sensitivity coefficient	**0.5**							
Combined Standard Uncertainty						**12.65**	**%**	
Expanded Uncertainty, 95% confidence		**k=**	**2.004**			**25.34**	**%**	

7 - EVALUATION PROCEDURE

7.1 SAR Evaluation Procedure

The evaluation was performed with the following procedure:

Step 1: Measurement of the SAR value at a fixed location above the ear point or central position was used as a reference value for assessing the power drop.

Step 2: The SAR distribution at the exposed side of the head was measured at a distance of 3.9 mm from the inner surface of the shell. The area covered the entire dimension of the head or EUT and the horizontal grid spacing was 20 mm x 20 mm. Based on these data, the area of the maximum absorption was determined by spline interpolation.

Step 3: Around this point, a volume of 32 mm x 32 mm x 34 mm was assessed by measuring 5 x 5 x 7 points. On the basis of this data set, the spatial peak SAR value was evaluated under the following procedure:

1. The data at the surface were extrapolated, since the center of the dipoles is 2.7 mm away from the tip of the probe and the distance between the surface and the lowest measuring point is 1.2 mm. The extrapolation was based on a least square algorithm [11]. A polynomial of the fourth order was calculated through the points in z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.

2. The maximum interpolated value was searched with a straightforward algorithm. Around this maximum the SAR values averaged over the spatial volumes (1 g or 10 g) were computed by the 3D-Spline interpolation algorithm. The 3D-Spline is composed of three onedimensional splines with the “Not a knot"-condition (in x, y and z-directions) [11], [12]. The volume was integrated with the trapezoidal-algorithm. One thousand points (10 x 10 x 10) were interpolated to calculate the average.

3. All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

Step 4: Re-measurement of the SAR value at the same location as in Step 1. If the value changed by more than 5%, the evaluation was repeated.

7.2 Exposure Limits

Table 1: Limits for Occupational/Controlled Exposure (W/kg)

Whole-Body	Partial-Body	Hands. Wrists. Feet and Ankles
0.4	8.0	20.0

Table 2: Limits for General Population/Uncontrolled Exposure (W/kg)

Whole-Body	Partial-Body	Hands. Wrists. Feet and Ankles
0.08	1.6	4.0

Note: Whole-body SAR is averaged over the entire body, partial-body SAR is averaged over any 1 gram of tissue defined as a tissue volume in the shape of a cube SAR for hands, writs, feet and ankles is averaged over any 10 grams of tissue defined as a tissue volume in the shape of a cube.

Population/Uncontrolled Environments are defined as locations where there is the exposure of individual who have no knowledge or control of their exposure.

Occupational/Controlled Environments are defined as locations where there is exposure that may be incurred by people who are aware of the potential for exposure (i.e. as a result of employment or occupation).

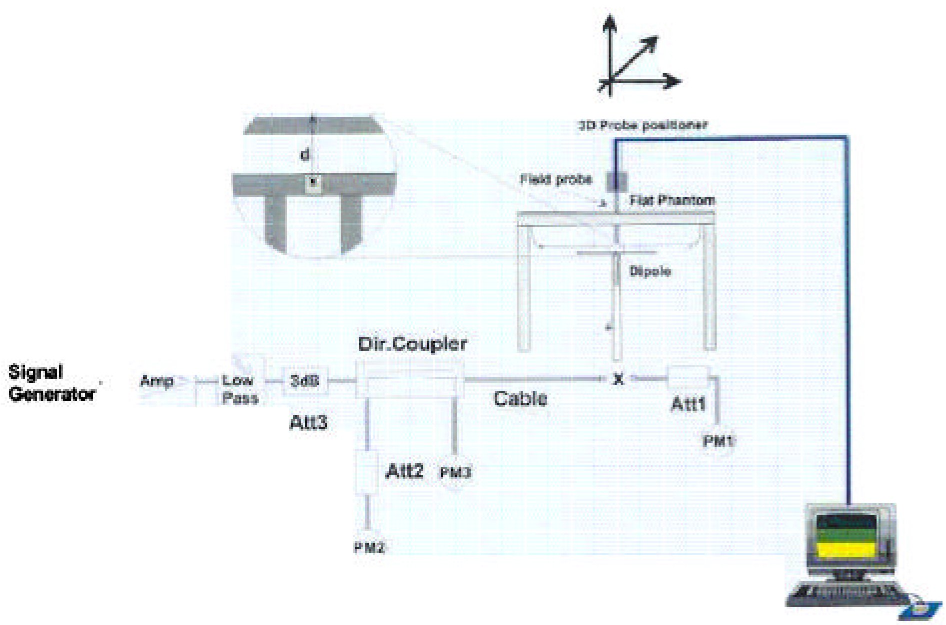
Population/uncontrolled environments Partial-body limit 1.6W/kg applied to the EUT.

7.3 Simulated Tissue Liquid Parameter Confirmation

The dielectric parameters were checked prior to assessment using the HP85070A dielectric probe kit. The dielectric parameters measured are reported in each correspondent section:

7.4 SAR Measurement

The SAR measurement was performed with the E-field probe in mechanical detection mode only. The setup and determination of the forward power into the dipole was performed using the following procedures.



First, the power meter PM1 (including attenuator Att1) is connected to the cable to measure the forward power at the location of the dipole connector (X). The signal generator is adjusted for the desired forward power at he dipole connector (taking into account the attenuation of Att1) as read by power meter PM2. after connecting the cable to the dipole, the signal generator is readjusted for the same reading at power meter PM2. If the signal generator does not allow adjustment in 0.01dB steps, the remaining difference at PM 2 must be taken into consideration. PM3 records the reflected power from the dipole to ensure that the value is not changed form the previous value. The reflected power should be 20dB below the forward power.

The SAR measurements were performed in order to achieve repeatability and to establish an average target value.

7.5 System Accuracy Verification

Prior to the assessment, the system validation kit was used to test whether the system was operating within its specifications of ±10%. The validation results are tabulated below. And also the corresponding SAR plot is attached as well in the SAR plots files.

IEEE P1528 recommended reference value for head

Frequency (MHz)	1 g SAR	10 g SAR	Local SAR at surface (above feed point)	Local SAR at surface (v=2cm offset from feed point)
300	3.0	2.0	4.4	2.1
450	4.9	3.3	7.2	3.2
835	9.5	6.2	14.1	4.9
900	10.8	6.9	16.4	5.4
1450	29.0	16.0	50.2	6.5
1800	38.1	19.8	69.5	6.8
1900	39.7	20.5	72.1	6.6
2000	41.1	21.1	74.6	6.5
2450	52.4	24.0	104.2	7.7
3000	63.8	25.7	140.2	9.5

Validation Dipole SAR Reference Test Result for Body (835 MHz)

Validation Measurement	SAR @ 0.025W Input averaged over 1g	SAR @ 1W Input averaged over 1g	SAR @ 0.025W Input averaged over 10g	SAR @ 1W Input averaged over 10g
Test 1	0.222	8.88	0.112	4.48
Test 2	0.221	8.84	0.111	4.44
Test 3	0.222	8.88	0.112	4.48
Test 4	0.220	8.80	0.111	4.44
Test 5	0.223	8.92	0.113	4.52
Test 6	0.222	8.88	0.115	4.60
Test 7	0.221	8.84	0.114	4.56
Test 8	0.222	8.88	0.114	4.56
Test 9	0.223	8.92	0.113	4.52
Test 10	0.222	8.88	0.112	4.48
Average	0.2218	8.872	0.1127	4.51

Validation Dipole SAR Reference Test Result for Body (1900 MHz)

Validation Measurement	SAR @ 0.126W Input averaged over 1g	SAR @ 1W Input averaged over 1g	SAR @ 0.126W Input averaged over 10g	SAR @ 1W Input averaged over 10g
Test 1	3.1	24.61	1.42	11.27
Test 2	3.1	24.61	1.41	11.20
Test 3	3.2	25.41	1.43	11.35
Test 4	3.2	25.41	1.42	11.27
Test 5	3.1	24.61	1.42	11.27
Test 6	3.2	25.61	1.41	11.20
Test 7	3.2	25.61	1.43	11.35
Test 8	3.1	24.61	1.42	11.27
Test 9	3.1	24.61	1.42	11.27
Test 10	3.1	24.61	1.43	11.35
Average	3.14	24.97	1.421	11.28

7.6 Liquid Measurement Result

7/11/03:

Simulant	Freq [MHz]	Parameters	Liquid Temp [°C]	Target Value	Measured Value	Deviation	Limits [%]
Body	835	ε_r	22	56.1	55.5	-1.07	±5
		σ	22	0.95	0.98	3.16	±5
		1g SAR	22	8.872	8.00	9.83	±10
Head	835	ε_r	22	42.54	43.1	1.32	±5
		σ	22	0.91	0.91	0	±5
		1g SAR	22	9.5	10.2	7.37	±10

7/14/03:

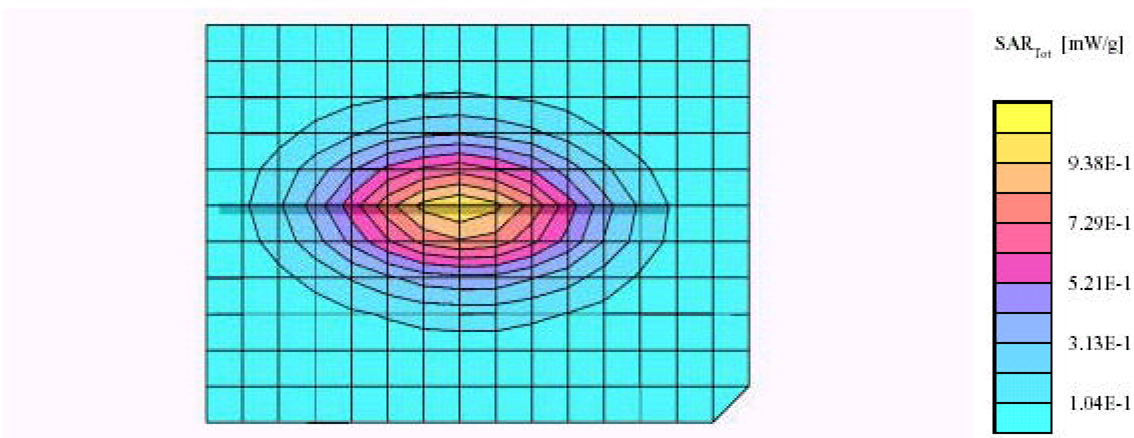
Simulant	Freq [MHz]	Parameters	Liquid Temp [°C]	Target Value	Measured Value	Deviation	Limits [%]
Body	1900	ε_r	22	54.0	52.9	-2.04	±5
		σ	22	1.45	1.52	4.83	±5
		1g SAR	22	24.97	25.38	1.64	±10
Head	1900	ε_r	22	39.9	40.4	1.27	±5
		σ	22	1.42	1.37	-3.52	±5
		1g SAR	22	39.7	37.52	-5.49	±10

ε_r = relative permittivity, σ = conductivity and ρ=1000kg/m^3

835 MHz Body Liquid Forward Power = 155 mW
835 MHz Head Liquid Forward Power = 124 mW
1900 MHz Body Liquid Forward Power = 160 mW
1900 MHz Head Liquid Forward Power = 105 mW

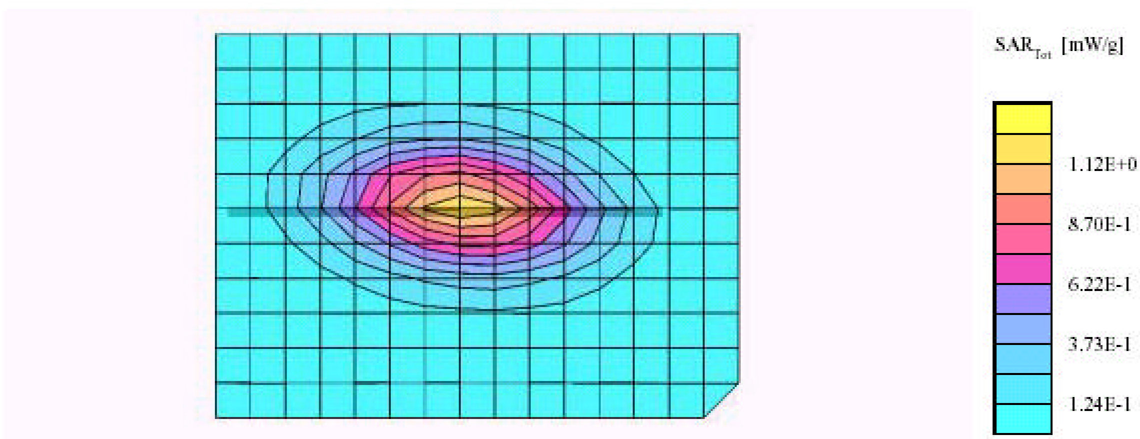
System Validation 835 MHz Body liquid (Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 835 MHz
Probe: ET3DV6 - SN1604; ConvF(6.40,6.40,6.40); Crest factor: 8.0; 835 (Body) MHz: σ = 0.98 mho/m ε_r = 55.5 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 1.24 mW/g, SAR (10g): 0.750 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: -0.02 dB



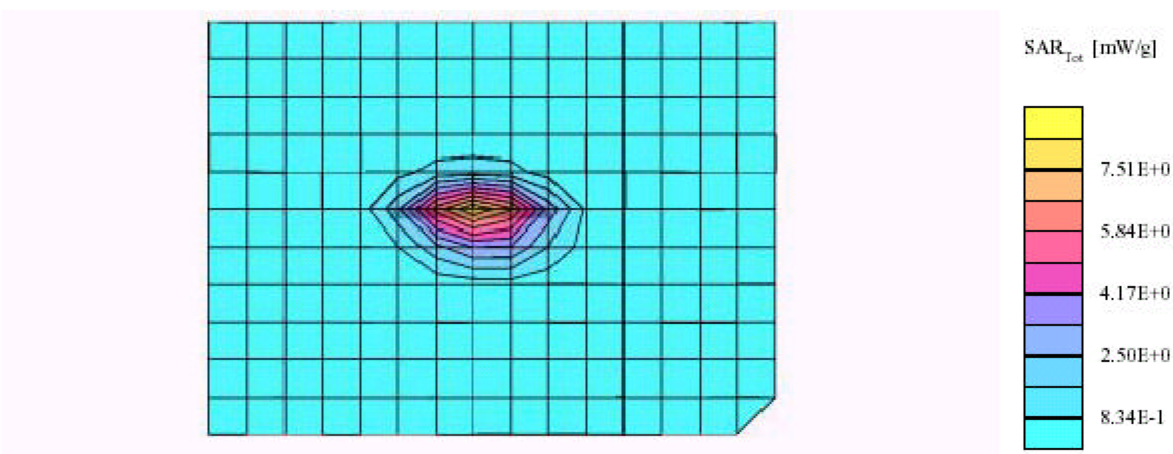
System Validation 835 MHz Head liquid (Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 835 MHz
Probe: ET3DV6 - SN1604; ConvF(6.50,6.50,6.50); Crest factor: 8.0; 835 (Head) MHz: σ = 0.91 mho/m ε_r = 43.1 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 1.27 mW/g, SAR (10g): 0.753 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.01 dB



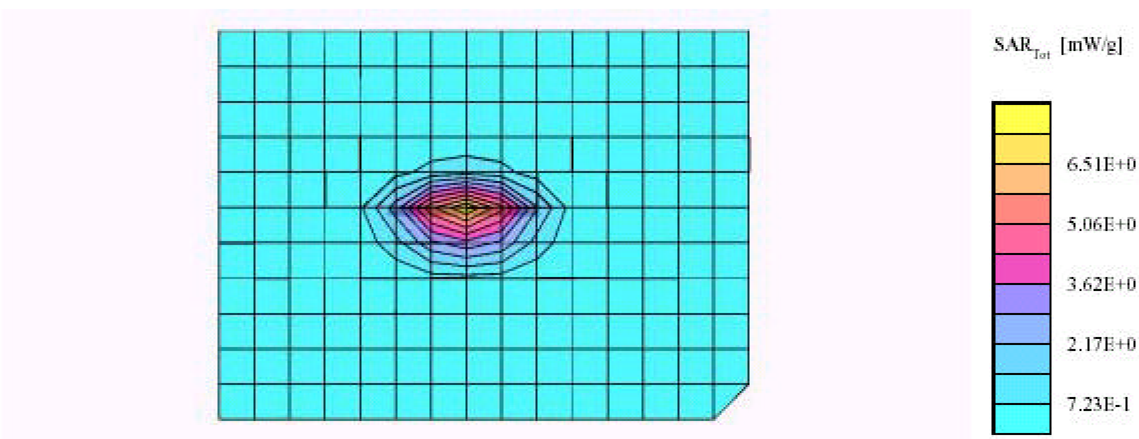
System Validation 1900 MHz (Body Liquid, Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/03)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 1900 MHz
Probe: ET3DV6 - SN1604; ConvF(4.90,4.90,4.90); Crest factor: 8.0; Body 1900 MHz: σ = 1.52 mho/m ε_r = 52.9 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 4.06 mW/g, SAR (10g): 2.20 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: -0.02 dB



System Validation 1900 MHz (Head Liquid, Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/2003)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 1900 MHz
Probe: ET3DV6 - SN1604; ConvF(5.50,5.50,5.50); Crest factor: 8.0; Head 1900 MHz: σ = 1.37 mho/m ε_r = 40.4 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 3.94 mW/g, SAR (10g): 2.07 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: -0.00 dB



8 - SAR TEST RESULTS

This page summarizes the results of the performed dosimetric evaluation. The plots with the corresponding SAR distributions, which reveal information about the location of the maximum SAR with respect to the device could be found in the following pages.

The output power was measured prior to testing and a fresh battery charge was ensured before each test. The modulation characteristics of the EUT is GSM, therefore, a crest factor of 8 was used during the test.

8.1 SAR Body and Head Worst-Case Test Data

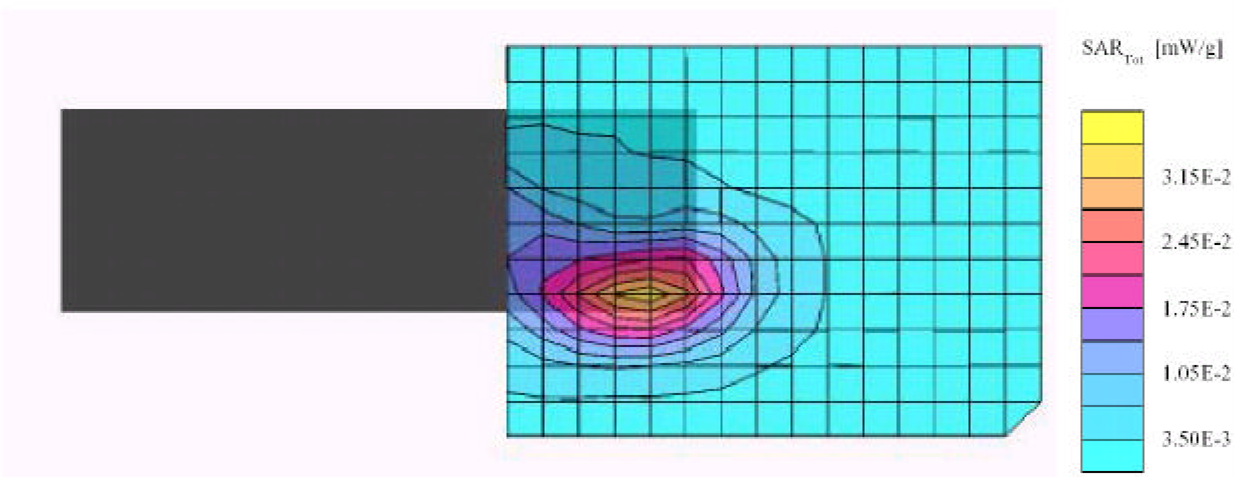
Ambient Temperature (ºC): 23.0
Relative Humidity (%): 49.3

Position	Frequency (MHz)	Output Power (dBm)	Test Type	Antenna position	Liquid	Phantom	Notes / Accessories	Measured (mW/g)	Limit (mW/g)	Plot #
Right Side Touching	837	23.83	Body worn	Retracted	Body	Flat	None	0.0312	1.6	1
Left Side Touching	837	23.83						0.0251		2
Top Touching	837	23.83						0.0259		3
Back Touching	837	23.83						0.245		4
Right Side Touching	1880	28.00	Body worn	Retracted	Body	Flat	None	0.133	1.6	5
Left Side Touching	1880	28.00						0.0169		6
Top Touching	1880	28.00						0.152		7
Back Touching	1880	28.00						0.218		8

8.2 Plots of Test Result

The plots of test result were attached as reference.

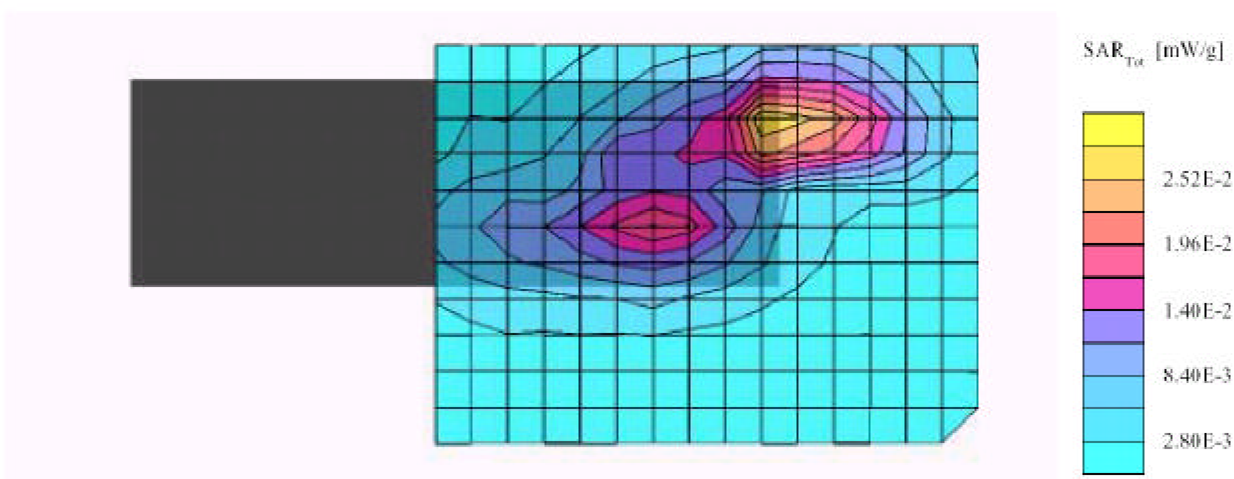
Verifone, Omni3600G (Right Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 837 MHz
Probe: ET3DV6 - SN1604; ConvF(6.40,6.40,6.40); Crest factor: 8.0; Body 835 MHz: $\sigma = 0.98$ mho/m $\varepsilon_r = 55.5$ $\rho = 1.00$ g/cm³
Cube 5x5x7: SAR (1g): 0.0312 mW/g, SAR (10g): 0.0187 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: -0.01 dB



Plot #1

Verifone, Omni3600G (Left Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)

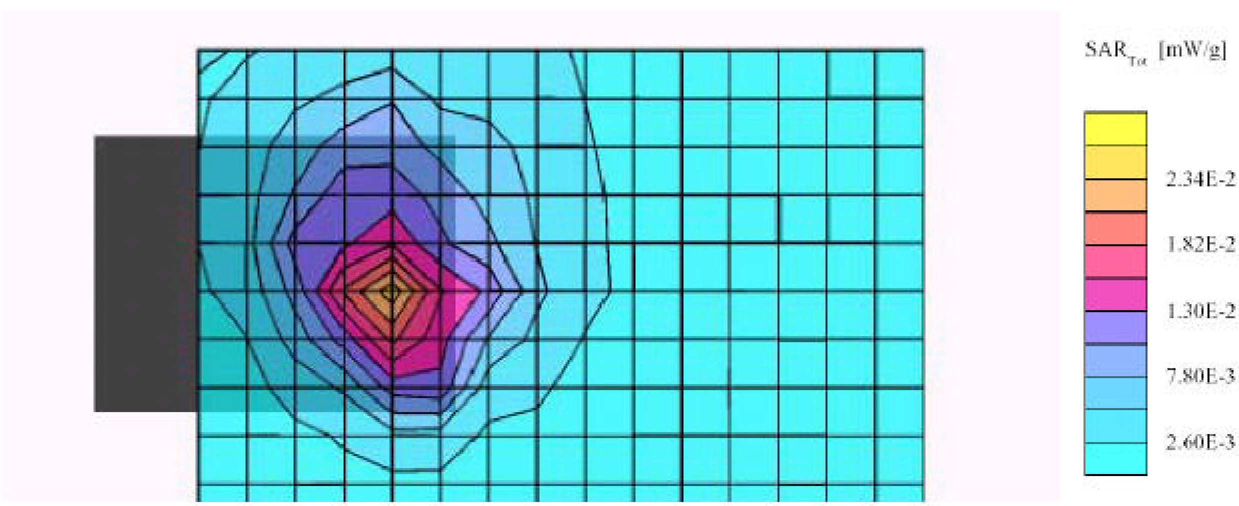
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 837 MHz
Probe: ET3DV6 - SN1604; ConvF(6.40,6.40,6.40); Crest factor: 8.0; Body 835 MHz: σ = 0.98 mho/m ε_r = 55.5 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 0.0251 mW/g, SAR (10g): 0.0152 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: -0.01 dB



Plot #2

Verifone, Omni3600G (Top Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 837 MHz
Probe: ET3DV6 - SN1604; ConvF(6.40,6.40,6.40); Crest factor: 8.0; Body 835 MHz: $\sigma = 0.98$ mho/m $\varepsilon_r = 55.5$ $\rho = 1.00$ g/cm³
Cube 5x5x7: SAR (1g): 0.0259 mW/g, SAR (10g): 0.0152 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.02 dB



Plot #3

Verifone, Omni3600G (Back Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)

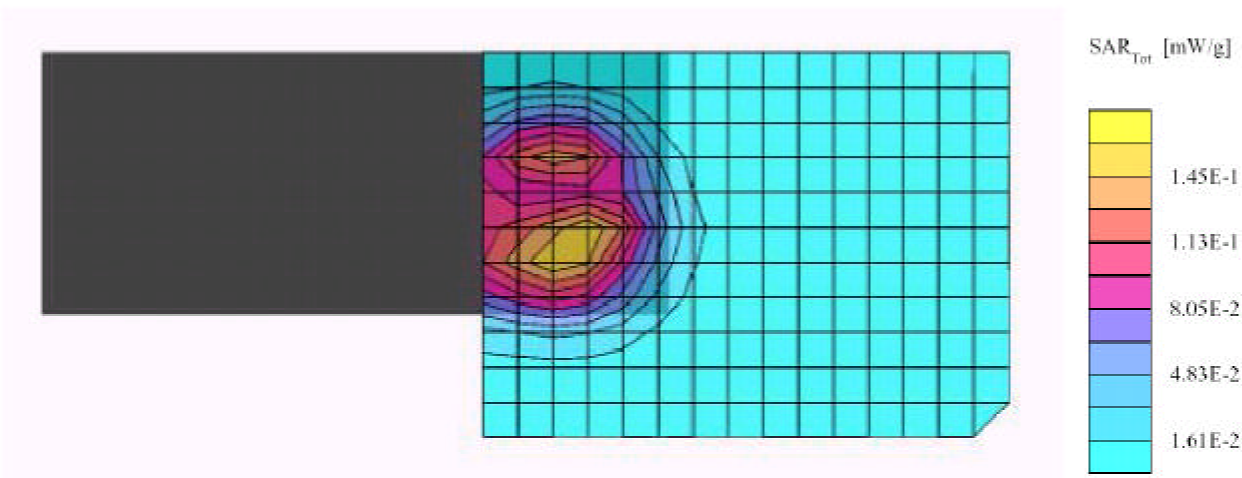
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 837 MHz

Probe: ET3DV6 - SN1604; ConvF(6.40,6.40,6.40); Crest factor: 8.0; Body 835 MHz: σ = 0.98 mho/m ε_r = 55.5 ρ = 1.00 g/cm³

Cube 5x5x7: SAR (1g): 0.245 mW/g, SAR (10g): 0.134 mW/g, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.05 dB



Plot #4

Verifone, Omni3600G (Right Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/03)

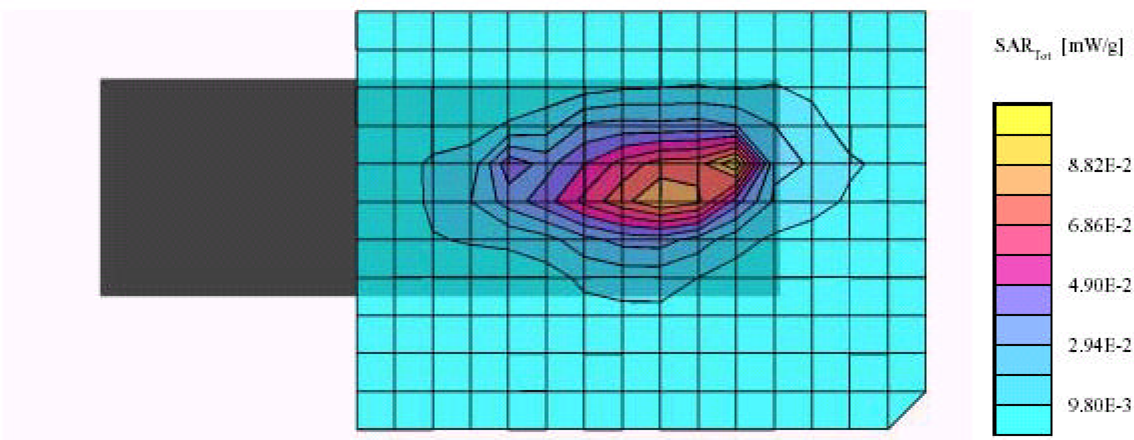
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 1880 MHz

Probe: ET3DV6 - SN1604; ConvF(4.90,4.90,4.90); Crest factor: 8.0; Body 1900 MHz: σ = 1.52 mho/m ε_r = 52.9 ρ = 1.00 g/cm³

Cube 5x5x7: SAR (1g): 0.133 mW/g, SAR (10g): 0.0705 mW/g, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

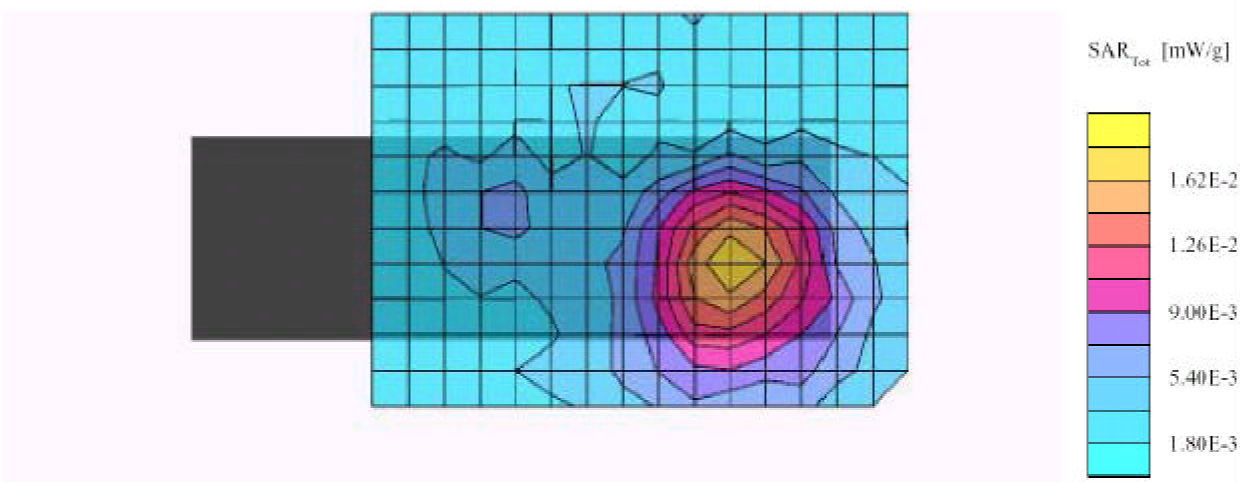
Powerdrift: -0.03 dB



Plot #5

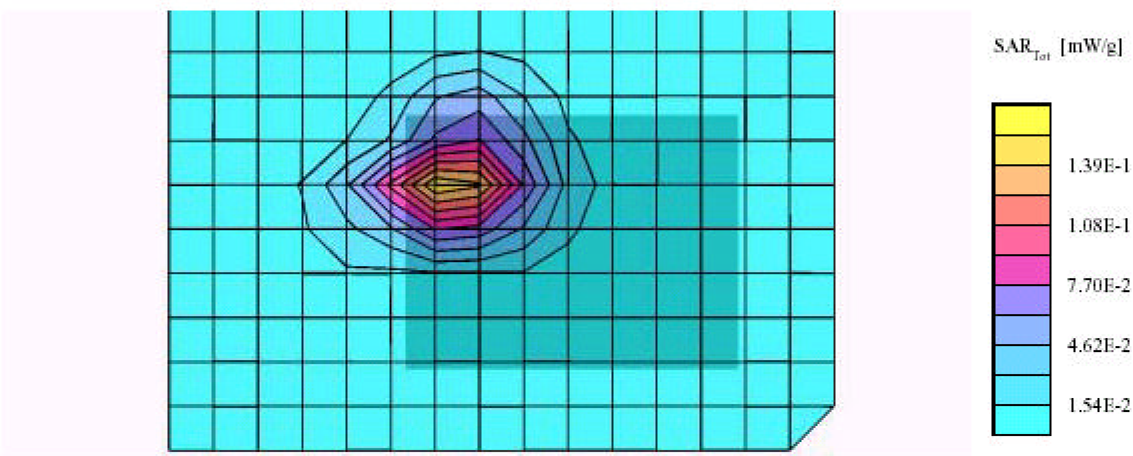
Verifone, Omni3600G (Left Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/03)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 1880 MHz
Probe: ET3DV6 - SN1604; ConvF(4.90,4.90,4.90); Crest factor: 8.0; Body 1900 MHz: σ = 1.52 mho/m ε_r = 52.9 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 0.0169 mW/g, SAR (10g): 0.0115 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.01 dB



Plot #6

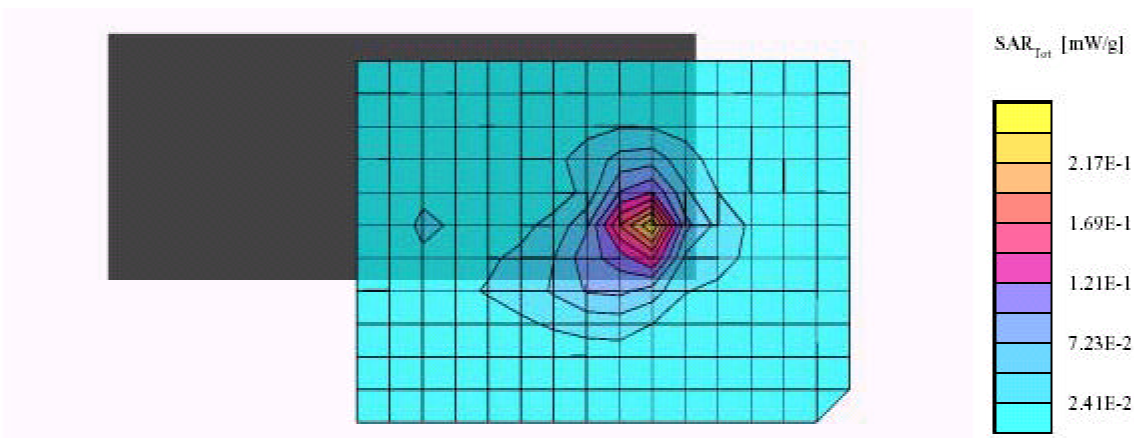
Verifone, Omni3600G (Top Side of the DUT faced toward and in touch with flat phantom,
Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/03)
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 1880 MHz
Probe: ET3DV6 - SN1604; ConvF(4.90,4.90,4.90); Crest factor: 8.0; Body 1900 MHz: σ = 1.52 mho/m ε_r = 52.9 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 0.152 mW/g, SAR (10g): 0.0893 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.05 dB



Plot #7

Verifone, Omni3600G (Back Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/03)

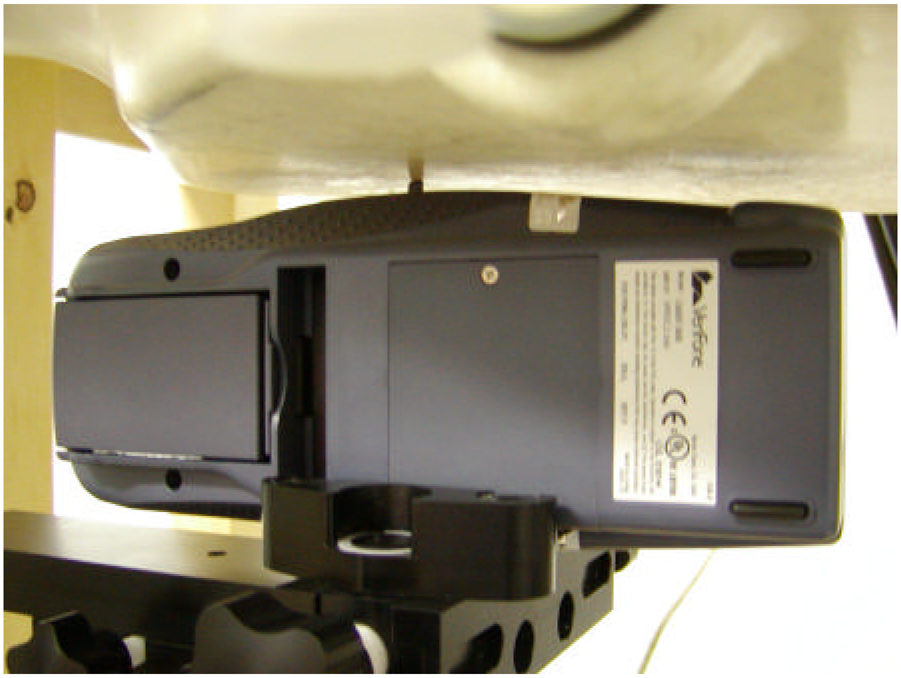
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 1880 MHz
Probe: ET3DV6 - SN1604; ConvF(4.90,4.90,4.90); Crest factor: 8.0; Body 1900 MHz: σ = 1.52 mho/m ε_r = 52.9 ρ = 1.00 g/cm³
Cube 5x5x7: SAR (1g): 0.218 mW/g, SAR (10g): 0.112 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.00 dB



Plot #8

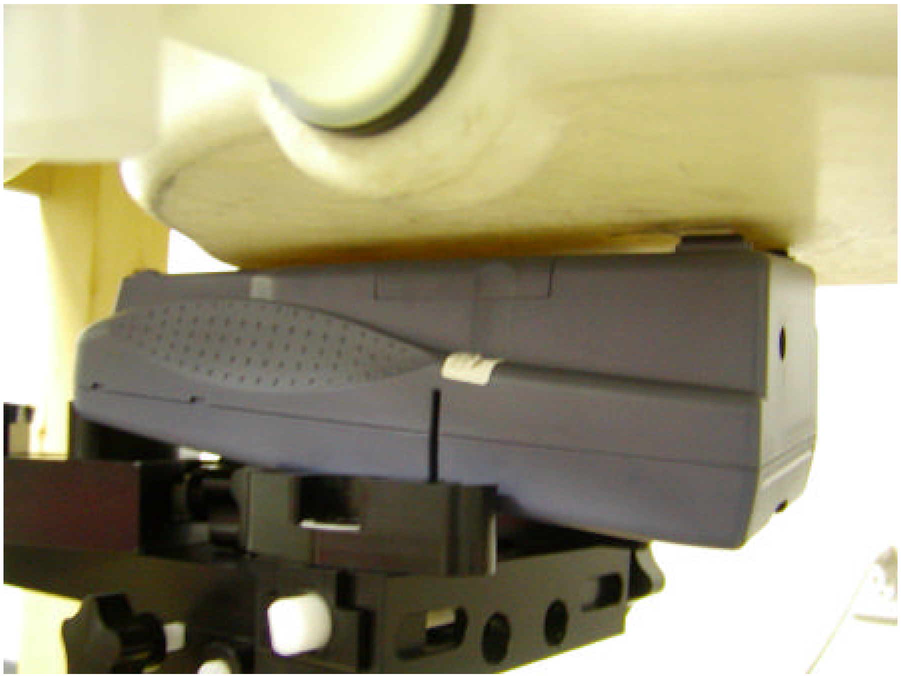
EXHIBIT A - SAR SETUP PHOTOGRAPHS

Right Side Touching with Phantom



Left Side Touching with Phantom

Back Side Touching with Phantom



Top Side Touching with Phantom

EXHIBIT B – EUT PHOTOGRAPHS

Chassis - Top View

Chassis - Back View

Chassis – Right Side View

Chassis – Cover off View

EUT – Inside Explode View

EUT – Antenna and Modem View

EUT – Antenna and Modem View 2

EUT – AnyData Modem and Antenna View

EUT – AnyData Modem Close Up View

EUT – SN7 Close Up View

EXHIBIT C – Z-Axis

Verifone, Omni3600G (Back Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 7/11/03)

SAM Phantom: Section; Position: ; Frequency: 837 MHz

Probe: ET3DV6 - SN1604; ConvF(6.40,6.40,6.40); Crest factor: 8.0; Body 835 MHz: σ = 0.98 mho/m ε_r = 55.5 ρ = 1.00 g/cm³

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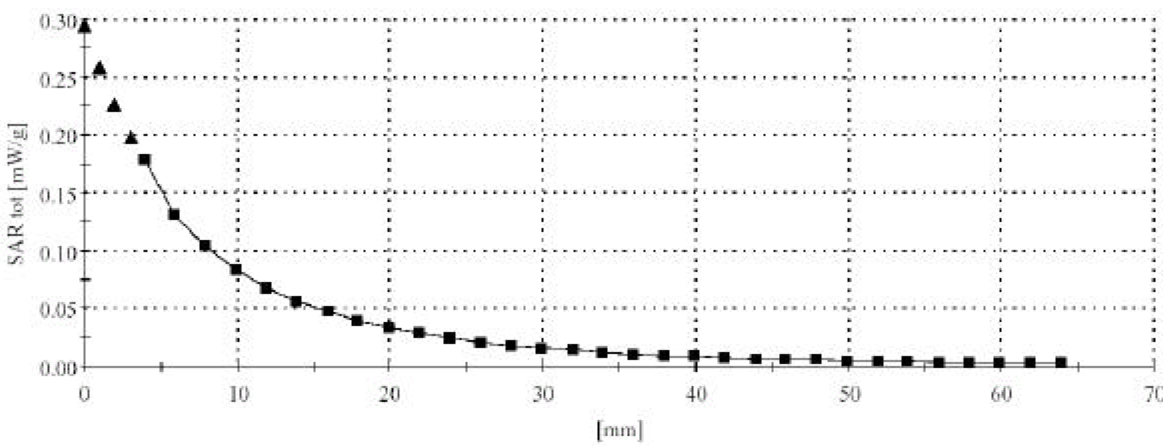
Z-Axis: Dx = 0.0, Dy = 0.0, Dz = 2.0



Verifone, Omni3600G (Back Side of the DUT faced toward and in touch with flat phantom, Ambient Temp = 22 Deg C, Liquid Temp = 22 Deg C, 7/14/03)

SAM Phantom: Section; Position: ; Frequency: 1880 MHz

Probe: ET3DV6 - SN1604; ConvF(4.90,4.90,4.90); Crest factor: 8.0; Body 1900 MHz: σ = 1.52 mho/m ε_r = 52.9 ρ = 1.00 g/cm³

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Z-Axis: Dx = 0.0, Dy = 0.0, Dz = 2.0