REPORT No.: SZ24040355S01



# **TEST REPORT**

APPLICANT	MICRO COMPUTER (HK) TECH LIMITED
PRODUCT NAME	: V3 3-in-1 Tablet
MODEL NAME	<ul> <li>V3, V3-001, V3-002, V3-003, V3-004, V3-005, V3-006, V3-007, V3-008,</li> <li>V3-009, V3-010, V3-011, V3-012,</li> <li>V3-013, V3-014, V3- 015, V3-016, V3-017, V3-018, V3-019, V3-020, V3 SE</li> </ul>
BRAND NAME	: minisfourm
FCC ID	: 2A49R-V3
STANDARD(S)	: FCC 47 CFR Part 2(2.1093) IEC TR 63170:2018 IEEE 1528-2013 IEC/IEEE 62209-1528:2020
receipt date	: 2024-04-28
TEST DATE	: 2024-06-04 to 2024-06-20
ISSUE DATE	: 2024-08-07
Certification	Edited by: Xie Yiyun (Rapporteur)

Approved by: Gan Yueming (Supervisor)

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Annex D Plots of Maximum SAR&PD Test Results Annex E Conducted Power Annex F Test Position Consideration Annex G DASY Calibration Certificate

	Change History	
Version	Date	Reason for Change
1.0	2024-08-07	First edition



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## **1 SAR Results Summary**

The maximum results of Specific Absorption Rate (SAR) found during test as bellows:

		Highest SAR Summary
Frequency		Body
Band		(Separation 0mm)
		1g SAR (W/kg)
	2.4GHz WLAN	0.205
VVLAN	5GHz WLAN	0.335
2.4GHz Band	Bluetooth	0.086

		Reported SAR	APD	Scaled PD
Frequ	lency Band	Body	Body	4cm <sup>2</sup> psPD
		1g SAR (W/kg)	4cm <sup>2</sup> (mW/cm <sup>2</sup> )	(mW/cm <sup>2</sup> )
WLAN	6GHz WLAN	0.907	0.335	0.647

Highest Simultaneous Transmission	0 993 W/ka	Limit(W/kg): 1.6 W/kg
1g SAR (W/kg)	elecci tring	

Highest Simultaneous Transmission with Multiple transmitters	Total Exposure Ratio	Limit
SAR & Power Density	0.701	1.0

#### Note:

- This device is compliance with Specific Absorption Rate (SAR) for general population or uncontrolled exposure limits (1.6 W/kg for 1g SAR, 1.0 mW/cm<sup>2</sup> for iPD and APD in 4cm<sup>2</sup>) specified in FCC 47 CFR part 1 (1.1310) and IEEE C95.1-1991), and had been tested in accordance with the measurement methods and procedures specified in IEC/IEEE 62209-1528, IEEE 1528-2013, TCBC workshop notes, IEC TR 63170 and FCC KDB publications.
- 2. When the test result is a critical value, we will use the measurement uncertainty give the judgment result based on the 95% confidence intervals.



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## **2** Technical Information

**Note:** Provide by applicant.

### 2.1 Applicant and Manufacturer Information

Applicant:	MICRO COMPUTER (HK) TECH LIMITED
Applicant Address:	RM 18, 28/F, Shui On Centre, 6-8 Harbour Road, WaterfRont, Wan Chai, HK
Manufacturer:	MICRO COMPUTER (HK) TECH LIMITED
Manufacturer Address:	RM 18, 28/F, Shui On Centre, 6-8 Harbour Road, WaterfRont, Wan Chai, HK

### 2.2 Equipment under Test (EUT) Description

Product Name:	V3 3-in-1 Tablet
EUT NO.:	1#
Hardware Version:	HPPAC_V1.0
Software Version:	Windows pro 23H2
Operation Frequency:	WLAN 2.4GHz: 2412 MHz ~ 2472 MHz
	WLAN 5.2GHz: 5180 MHz ~ 5240 MHz
	WLAN 5.3GHz: 5260 MHz ~ 5320 MHz
	WLAN 5.5GHz: 5500 MHz ~ 5700 MHz
	WLAN 5.8GHz: 5745 MHz ~ 5825 MHz
	WLAN 6.2GHz (U-NII-5): 5925 MHz ~ 6425 MHz
	WLAN 6.7GHz (U-NII-6): 6425 MHz ~ 6525 MHz
	WLAN 6.5GHz (U-NII-7): 6525 MHz ~ 6875 MHz
	WLAN 7.0GHz (U-NII-8): 6875 MHz ~ 7125 MHz
	Bluetooth: 2402 MHz ~ 2480 MHz
Modulation Technology:	802.11b: DSSS
	802.11a/g/n-HT20/HT40/ac-VHT80/160: OFDM
	802.11ax-HEW20/40/80/160: OFDMA
	BR+EDR: GFSK(1Mbps), π/4-DQPSK(2Mbps), 8-DPSK(3Mbps)
	BLE: GFSK(1Mbps)
Antenna Type:	WLAN: FPC Antenna
	Bluetooth: FPC Antenna

Note:

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- There are twenty-two models (V3, V3-001, V3-002, V3-003, V3-004, V3-005, V3-006, V3-007, V3-008, V3-009, V3-010, V3-011, V3-012, V3-013, V3-014, V3- 015, V3-016, V3-017, V3-018, V3-019, V3-020 and V3 SE) in this report. They are different from the model names and the appearance colors.
- The output power test results of WLAN/Bluetooth refer to the module test report (Report No.: 200611-04. TR04, 200611-04. TR01, 200611-04. TR05 and 200611-04.TR38), which issued on November 03, 2020 and February 17, 2021 by Intel Corporation S.A.S WRF Lab.
- Declaration of Conformity: The output power test results of WLAN/Bluetooth in the report are provided by the applicant, and the test laboratory is not responsible for the accuracy of the information.
- 4. For more detailed description, please refer to specification or user manual supplied by the applicant and/or manufacturer.

Temperature:	18°C ~25°C
Humidity:	35%~75% RH

2.3 Environment of Test Sit
-----------------------------

Test Frequency:	WLAN 2.4GHz WLAN 5GHz WLAN 6GHz Bluetooth
Operation Mode:	
Power Level:	WLAN 2.4GHz, WLAN5GHz, WLAN 6GHz, Bluetooth

During SAR test, EUT is in Traffic Mode (Channel Allocated) at Normal Voltage Condition. A communication link is set up with a System Simulator (SS) by air link, and a call is established.

The EUT shall use its internal transmitter. The antenna(s), battery and accessories shall be those specified by the Factory. The EUT battery must be fully charged and checked periodically during the test to ascertain uniform power output. If a wireless link is used, the antenna connected to the output of the base station simulator shall be placed at least 50 cm away from the handset. The signal transmitted by the simulator to the antenna feeding point shall be lower than the output power level of the handset by at least 35 dB.





## **3** Specific Absorption Rate (SAR)

### **3.1 Introduction**

SAR is related to the rate at which energy is absorbed per unit mass in an object exposed to a radio field. The SAR distribution in a biological body is complicated and is usually carried out by experimental techniques or numerical modeling. The standard recommends limits for two tiers of groups, occupational or controlled and general population or uncontrolled, based on a person's awareness and ability to exercise control over his or her exposure. In general, occupational or controlled exposure limits are higher than the limits for general population or uncontrolled.

### 3.2 SAR Definition

The SAR definition is the time derivative (rate) of the incremental energy (dW) absorbed by (dissipated in) an incremental mass (dm) contained in a volume element (dv) of a given density ( $\rho$ ). The equation description is as below:

$$SAR = \frac{d}{dt} \left( \frac{dU}{dm} \right) = \frac{d}{dt} \left( \frac{dU}{\rho dv} \right)$$

SAR is expressed in units of Watts per kilogram (W/kg) SAR measurement can be either related to the temperature elevation in tissue by

$$SAR = C\left(\frac{\delta T}{\delta t}\right)$$

Where: C is the specific heat capacity,  $\delta T$  is the temperature rise and  $\delta t$  is the exposure duration, or related to the electrical field in the tissue by

$$SAR = \frac{\sigma \cdot E^2}{\rho}$$

Where:  $\sigma$  is the conductivity of the tissue,  $\rho$  is the mass density of the tissue and E is the RMS electrical field strength. However for evaluating SAR of low power transmitter, electrical field measurement is typically applied.



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## **4 RF Exposure Limits**

### 4.1 Uncontrolled Environment

Uncontrolled Environments are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure. The general population/uncontrolled exposure limits are applicable to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Members of the general public would come under this category when exposure is not employment-related; for example, in the case of a wireless transmitter that exposes persons in its vicinity.

Type Exposure	Uncontrolled Environment Limit
Spatial Peak SAR (1g cube tissue for head and trunk)	1.6 W/kg
Spatial Peak SAR (10g cube tissue for limbs)	4.0 W/kg
Spatial Peak SAR (1g cube tissue for whole body)	0.08 W/kg

Limits for General Po	pulation/Uncontrolled	l Ex	posure	(W/kg)

Frequency range (MHz)	Electric field strength (V/m)	Magnetic field strength (A/m)	Power density (mW/cm <sup>2</sup> )	Averaging time (minutes)
	(A) Limits for O	ccupational/Controlled Expo	sures	
0.3-3.0	614	1.63	*(100)	6
3.0-30	1842/	f 4.89/	f *(900/f2)	6
30-300	61.4	0.163	1.0	6
300-1500			f/300	6
1500-100,000			5	6
	(B) Limits for Gene	ral Population/Uncontrolled	Exposure	
0.3-1.34	614	1.63	*(100)	30
1.34-30	824/	f 2.19/	f *(180/f2)	30
30-300	27.5	5 0.073	0.2	30
300-1500			f/1500	30
1500-100,000			1.0	30

### Note:

- 1. Occupational/Uncontrolled Environments are defined as locations where there is exposure that may be incurred by people who are aware of the potential for exposure (i.e. as a result of employment or occupation).
- 2. Whole-Body SAR is averaged over the entire body, partial-body SAR is averaged over any 1gram of tissue defined as a tissue volume in the shape of a cube. SAR for hands, wrists, feet and ankles is averaged over any 10 grams of tissue defined as a tissue volume in the shape of a cube.

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### **4.2 Controlled Environment**

Controlled Environments are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation). In general, occupational/controlled exposure limits are applicable to situations in which persons are exposed as a consequence of their employment, who have been made fully aware of the potential for exposure and can exercise control over their exposure. This exposure category is also applicable when the exposure is of a transient nature due to incidental passage through a location where the exposure levels may be higher than the general population/uncontrolled limits, but the exposure by leaving the area or by some other appropriate means.



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## **5 Applied Reference Documents**

Leading reference documents for testing:

		Method			
Identity	Document Title	Determination			
		/Remark			
	Radio Frequency Radiation Exposure				
FCC 47 CFR Part 2(2.1093)	valuation: Portable Devices	No deviation			
IEC/IEEE 62209-1528:2020	Measurement procedure for the assessment of specific absorption rate of human exposure to radio frequency fields from hand-held and body-mounted wireless communication devices –Part 1528: Human models, instrumentation, and procedures (Frequency range of 4 MHz to 10 GHz)	No deviation			
IEC TR 63170:2018	Measurement procedure for the evaluation of power density related to human exposure to radio frequency fields from wireless communication devices operating between 6 GHz and 100 GHz	No deviation			
IEEE 1528-2013	IEEE Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques	No deviation			
KDB 447498 D01v06	General RF Exposure Guidance	No deviation			
KDB 248227 D01v02r02	SAR Measurement Procedures for 802.11 Transmitters	No deviation			
KDB 616217 D04 v01r01	SAR Evaluation Considerations for Laptop, Notebook, Notebook and Tablet Computers	No deviation			
KDB 865664 D01v01r04	SAR Measurement 100 MHz to 6 GHz	No deviation			
KDB 865664 D02v01r02	RF Exposure Reporting	No deviation			
KDB 941225 D06v02r01	SAR Evaluation Procedures For Portable Devices With Wireless Router Capabilities	No deviation			
TCBC workshop in April 2021	RF Exposure Policies and Procedures	No deviation			
<b>Note 1:</b> Additions to, deviation, or exclusions from the method shall be judged in the "method determination" column of add, deviate or exclude from the specific method shall be explained in the "Remark" of the above table.					





## 6 SAR Measurement System



### Fig.6.1 SPEAG DASY System Configurations

The DASY system for performance compliance tests is illustrated above graphically. This system consists of the following items:

- > A standard high precision 6-axis robot with controller, a teach pendant and software.
- > A data acquisition electronic (DAE) attached to the robot arm extension.
- > A dosimetric probe equipped with an optical surface detector system.
- The electro-optical converter (EOC) performs the conversion between optical and electrical signals.
- A measurement server performs the time critical tasks such as signal filtering, control of the robot operation and fast movement interrupts.
- > A probe alignment unit which improves the accuracy of the probe positioning.
- > A computer operating Windows XP.
- DASY software.
- Remove control with teach pendant and additional circuitry for robot safety such as warming lamps, etc.
- > The SAM twin phantom.
- > A device holder.



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- Tissue simulating liquid.
- > Dipole for evaluating the proper functioning of the system.

Component details are described in the following sub-sections.

### 6.1 E-Field Probe

The SAR measurement is conducted with the dosimetric probe (manufactured by SPEAG). The probe is specially designed and calibrated for use in liquid with high permittivity. The dosimetric probe has special calibration in liquid at different frequency. This probe has a built in optical surface detection system to prevent from collision with phantom.

### > E-Field Probe Specification

#### <EX3DV4 Probe>

Construction	Symmetrical design with triangular core	
	Built-in shielding against static charges	
	PEEK enclosure material (resistant to	
	organic solvents, e.g., DGBE)	
Frequency	10 MHz to 10 GHz; Linearity: $\pm$ 0.2 dB	100
Directivity	$\pm~$ 0.3 dB in HSL (rotation around probe	Ť
	axis)	
	$\pm$ 0.5 dB in tissue material (rotation normal	
	to probe axis)	
Dynamic Range	10 $\mu$ W/g to 100 mW/g; Linearity: $\pm$ 0.2 dB	
Dimensions	Overall length: 330 mm (Tip: 20 mm)	Ţ
	Tip diameter: 2.5 mm (Body: 12 mm)	
	Typical distance from probe tip to dipole	
	centers: 1 mm	Fig 6.2 Photo of EX3DV4

#### > E-Field Probe Calibration

Each probe needs to be calibrated according to a dosimetric assessment procedure with accuracy better than  $\pm 10\%$ . The spherical isotropy shall be evaluated and within  $\pm 0.25$  dB. The sensitivity parameters (Norm X, Norm Y and Norm Z), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe are tested. The calibration data can be referred to Annex E of this report.





### 6.2 Data Acquisition Electronics (DAE)

The Data acquisition electronics (DAE) consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast 16 bits AD-converter and a command decoder and control logic unit. Transmission to the measurement server is accomplished through an optical downlink for data and status information as well as an optical uplink for commands and the clock. The input impedance of the DAE is 200 MOhm; the inputs are symmetrical and floating. Common mode rejection is above 80 dB.



Fig 6.2 Photo of DAE

### 6.3 Robot

The SPEAG DASY system uses the high precision robots (DASY5: TX60XL) type from Stäubli SA (France). For the 6-axis controller system, the robot controller version (DASY5: CS8c) from Stäubliis used. The Stäublirobot series have many features that are important for our application:

- High precision (repeatability 0.02 mm)
- High reliability (industrial design)
- Low maintenance costs (virtually maintenance free due to direct drive gears; nobelt drives)
- Jerk-free straight movements
- Low ELF interference (motor control fields shielded via the closed metallic construction shields)



Fig. 6.3 Photo of Robot

### 6.4 Measurement Server

The measurement server is based on a PC/104 CPU board with CPU (DASY 5: 400MHz, Intel Celeron), chip-disk (DASY5: 128 MB), RAM (DASY5: 128 MB). The necessary circuits for communication with the DAE electronic box, as well as the 16 bits AD converter system for optical detection and digital I/O interface are contained on the DASY I/O board, which is directly connected to the PC/104 bus of the CPU board.

The measurement server performs all the real-time data evaluation for field measurements and surface detection, controls robot movements and handles safety operations.



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Fig. 6.4 Photo of Server for DASY5

### 6.5 Light Beam Unit

The light beam switch allows automatic "tooling" of the probe. During the process, the actual position of the probe tip with respect to the robot arm is measured, as well as the probe length and the horizontal probe offset. The software then corrects all movements, such that the robot coordinates are valid for the probe tip.

The repeatability of this process is better than 0.1 mm. If a position has been taught with an aligned probe, the same position will be reached with another aligned probe within 0.1 mm, even if the other probe has different dimensions. During probe rotations, the probe tip will keep its actual position.



Fig. 6.5 Photo of Light Beam

### 6.6 Phantom

#### <SAM Twin Phantom>

Shell	2 ± 0.2 mm (sagging: <1%)				
Thickness	Center ear point: 6 ± 0.2 mm				
Filling Volume	Approx. 25 liters				
Dimensions	Length: 1000 mm; Width: 500 mm;				
	Height: adjustable feet				
Measurement	Left Head, Right Head, Flat				
Areas	phantom				



Fig. 6.6 Photo of SAM Phantom

The bottom plate contains three pair of bolts for locking the device holder. The device holder positions are adjusted to the standard measurement positions in the three sections. A white cover is provided to tap the phantom during off-periods to prevent water evaporation and changes in the liquid parameters. On the phantom top, three reference markers are provided to identify the

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phantom position with respect to the robot.

### 6.7 Device Holder

### <Device Holder for SAM Twin Phantom>

The SAR in the phantom is approximately inversely proportional to the square of the distance between the source and the liquid surface. For a source at 5 mm distance, a positioning uncertainty of  $\pm 0.5$  mm would produce a SAR uncertainty of  $\pm 20$  %. Accurate device positioning is therefore crucial for accurate and repeatable measurements. The positions in which the devices must be measured are defined by the standards.

The DASY device holder is designed to cope with different positions given in the standard. It has two scales for the device rotation (with respect to the body axis) and the device inclination (with respect to the line between the ear reference points). The rotation center for both scales is the ear reference point (ERP).

Thus the device needs no repositioning when changing the angles.

The DASY device holder is constructed of low-low POM material having the following dielectric parameters: relative permittivity  $\varepsilon$  = 3 and loss tangent  $\delta$  = 0.02. The amount of dielectric material has been reduced in the closest vicinity of the device, since measurements have suggested that the influence of the clamp on the test results could thus be lowered.

### <Laptop Extension Kit>

The extension is lightweight and made of POM, acrylic glass and foam. It fits easily on the upper part of the mounting device in place of the phone positioned. The extension is fully compatible with the SAM Twin and ELI phantoms.



Fig 6.7 Device Holder



Fig 6.8 Laptop Extension Kit



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### 6.8 Data storage and Evaluation

### > Data Storage

The DASY software stores the assessed data from the data acquisition electronics as raw data (in microvolt readings from the probe sensors), together with all the necessary software parameters for the data evaluation (probe calibration data, liquid parameters and device frequency and modulation data) in measurement files. The post-processing software evaluates the desired unit and format for output each time the data is visualized or exported. This allows verifications of the complete software setup even after the measurement and allows correction of erroneous parameter settings. For example, if a measurement has been performed with an incorrect crest factor parameter in the device setup, the parameter can be corrected afterwards and the data can be reevaluated.

The measured data can be visualized or exported in different units or formats, depending on the selected probe type (e.g., [V/m], [mW/g]). Some of these units are not available in certain situations or give meaningless results, e.g., a SAR-output in a non-lose media, will always be zero. Raw data can also be exported to perform the evaluation with other software packages.

#### > Data Evaluation

The DASY post-processing software (SEMCAD) automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software:

Probe Parameters:	- Sensitivity	Norm <sub>i</sub> , a <sub>i0</sub> , a <sub>i1</sub> , a <sub>i2</sub>	
	- Conversion	ConvF <sub>i</sub>	
	- Diode compression point	dcpi	
Device Parameters:	- Frequency	f	
	- Crest	cf	
Media Parameters:	- Conductivity	σ	
	- Density	ρ	

These parameters must be set correctly in the software. They can be found in the component documents or they can be imported into the software from the configuration files issued for the DASY components. In the direct measuring mode of the multi-meter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the

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exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power.

The formula for each channel can be given as:

$$V_i = U_i + U_i^2 \cdot \frac{cf}{dcp_i}$$

With  $V_i$  = compensated signal of channel i, (i = x, y, z)

 $U_i$  = input signal of channel i, (i = x, y, z) cf = crest factor of exciting field (DASY parameter)

 $dcp^{i}$  = diode compression point (DASY parameter)

From the compensated input signals, the primary field data for each channel can be evaluated:

E- Field Probes: 
$$E_i = \sqrt{\frac{v_i}{Norm_i \cdot ConvF}}$$

H-Field Probes: 
$$H_i = \sqrt{V_i} \cdot \frac{a_{i0} + a_{i1}f + a_{i2}f^2}{f}$$

With  $V_i$  = compensated signal of channel i, (i = x, y, z)

Norm<sub>i</sub>= senor sensitivity of channel i, (i = x, y, z),  $\mu V/(V/m)^2$ 

ConvF = sensitivity enhancement in solution

a<sub>ii</sub> = sensor sensitivity factors for H-field probes

f = carrier frequency (GHz)

 $E_i$  = electric field strength of channel i in V/m

Hi = magnetic field strength of channel i in A/m

The RSS value of the field components gives the total field strength (Hermitian magnitude):

$$E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}$$

The primary field data are used to calculate the derived field units.

$$\mathsf{SAR} = E_{tot}^2 \cdot \frac{\sigma}{\rho \cdot 1000}$$

With

SAR = local specific absorption rate in mW/g Etot= total field strength in V/m

 $\sigma$  = conductivity in (mho/m) or (Siemens/m)

 $\rho$ = equipment tissue density in g/cm3

Note that the density is set to 1, to account for actual head tissue density rather than the density of the tissue simulating liquid.

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### REPORT No.: SZ24040355S01

## 6.9 Test Equipment List

			Serial No./	Calibration		
Manufacturer	Name of Equipment	Type/Model	SW Version	Last Cal.	Due Date	
SPEAG	2450MHz System Validation Kit	D2450V2	805	2021.12.17	2024.12.16	
SPEAG	5000MHz System Validation Kit	D5GHzV2	1176	2021.12.19	2024.12.18	
SPEAG	D6.5GHz System Validation Kit	D6.5GHzV2	1054	2021.11.01	2024.10.31	
SPEAG	5G Verification Source	10GHz	1019	2023.12.03	2026.12.02	
SPEAG	DOSIMETRIC ASSESSMENT SYSTEM Software	DASY52	52.10.4.1527	NCR	NCR	
SPEAG	DOSIMETRIC ASSESSMENT SYSTEM Software	cDASY6 SAR	16.0.0.116	NCR	NCR	
SPEAG	DOSIMETRIC ASSESSMENT SYSTEM Software	cDASY6 mmWave	V2.4.2.62	NCR	NCR	
SPEAG	Dosimetric E-Field Probe	EX3DV4	3823	2023.09.14	2024.09.13	
SPEAG	Dosimetric E-Field Probe	EX3DV4	7608	2024.03.21	2025.03.20	
SPEAG	EUmmWave Probe	EUmmMV4	9602	2024.03.12	2025.03.11	
SPEAG	Data Acquisition Electronics	DAE4	480	2023.09.19	2024.09.18	
SPEAG	ELI Phantom	QD OVA004Ax	N/A	NCR	NCR	
SPEAG	Phone Positioner	N/A	N/A	NCR	NCR	
Agilent	MAX Signal Analyzer	N9020A	MY52091436	2024.05.30	2025.05.29	
Agilent	Network Analyzer	E5071B	MY42404762	2024.01.25	2025.01.24	
SPEAG	Dielectric Assessment KIT	DAK-3.5	1279	2024.03.18	2025.03.17	
mini-circuits	Amplifier	ZHL-42W+	608501717	NCR	NCR	
mini-circuits	Amplifier	ZVE-8G+	754401735	NCR	NCR	
Agilent	Signal Generator	N5182B	MY53050509	2023.09.19	2024.09.18	
R&S	Power Senor	NRP8S	103215	2024.01.25	2025.01.24	
Agilent	Power Meter	E4416A	MY45102093	2023.09.19	2024.09.18	
R&S	Power Sensor	NRP8S	103240	2024.01.25	2025.01.24	
Anritsu	Power Meter	E4418B	GB43318055	2024.05.30	2025.05.29	
Agilent	Dual Directional Coupler	778D	50422	NA	NA	
MCL	Attenuation 1	351-218-010	N/A	NA	NA	
R&S	Spectrum Analyzer	N9030A	MY54170556	2023.10.07	2024.10.06	
KTJ	Thermo meter	TA298	N/A	2023.11.22	2024.11.21	
SPEAG	Tissue Simulating Liquids	HBBL600-	-10000V6 24H		4H	



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#### Note:

- 1. The calibration certificate of DASY can be referred to annex G of this report.
- 2. Referring to KDB 865664 D01v01r04, the dipole calibration interval can be extended to 3 years with justification. The dipoles are also not physically damaged, or repaired during the interval.
- 3. The Insertion Loss calibration of Dual Directional Coupler and Attenuator were characterized via the network analyzer and compensated during system check.
- 4. The dielectric probe kit was calibrated via the network analyzer, with the specified procedure (calibrated in pure water) and calibration kit (standard) short circuit, before the dielectric measurement. The specific procedure and calibration kit are provided by Speag.
- 5. In system check we need to monitor the level on the power meter, and adjust the power amplifier level to have precise power level to the dipole; the measured SAR will be normalized to 1W input power according to the ratio of 1W to the input power to the dipole. For system check, the calibration of the power amplifier is deemed not critically required for correct measurement; the power meter is critical and we do have calibration for it
- 6. Attenuator insertion loss is calibrated by the network Analyzer, which the calibration is valid, before system check.
- 7. N.C.R means No Calibration Requirement.



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## 7 Tissue Simulating Liquids

For the measurement of the field distribution inside the SAM phantom with DASY, the phantom must be filled with around 25 liters of homogeneous body tissue simulating liquid. For head SAR testing, the liquid height from the ear reference point (ERP) of the phantom to the liquid top surface is larger than 15 cm, which is shown in Fig. 7.1, for body SAR testing, the liquid height from the centre of the flat phantom to liquid top surface is larger than 15 cm, which is shown in Fig. 7.2.





Fig 7.1 Photo of Liquid Height for Head SAR

Fig 7.2 Photo of Liquid Height for Body SAR

The following table gives the recipes for tissue simulating liquids								
Frequency (MHz)	Water (%)	Sugar (%)	Cellulose (%)	Salt (%)	Preventol (%)	DGBE (%)	Conductivity (σ)	Permittivity (εr)
	Head							
750	41.1	57.0	0.2	1.4	0.2	0	0.89	41.9
835	40.3	57.9	0.2	1.4	0.2	0	0.90	41.5
1800,1900,2000	55.2	0	0	0.3	0	44.5	1.40	40.0
2450	55.0	0	0	0	0	45.0	1.80	39.2
2600	54.8	0	0	0.1	0	45.1	1.96	39.0

#### Simulating Liquid for 5GHz, Manufactured by SPEAG

Ingredients	(% by weight)
Water	64~78%
Mineral oil	11~18%
Emulsifiers	9~15%
Additives and Salt	2~3%



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0	,			
Target Frequency	He	ad	Во	dy
(MHz)	ε <b>r</b>	σ <b>(S/m)</b>	ε <b>r</b>	σ <b>(S/m)</b>
150	52.3	0.76	61.9	0.80
300	45.3	0.87	58.2	0.92
450	43.5	0.87	56.7	0.94
835	41.5	0.90	55.2	0.97
900	41.5	0.97	55.0	1.05
915	41.5	0.98	55.0	1.06
1450	40.5	1.20	54.0	1.30
1610	40.3	1.29	53.8	1.40
1800-2000	40.0	1.40	53.3	1.52
2450	39.2	1.80	52.7	1.95
3000	38.5	2.40	52.0	2.73
5800	35.3	5.27	48.2	6.00

The relative permittivity and conductivity of the tissue material should be within  $\pm 5\%$  of the values given in the table below recommended by the FCC OET 65supplement C and RSS 102 Issue 5.

(  $\varepsilon$  r = relative permittivity,  $\sigma$  = conductivity and  $\rho$  = 1000 kg/m<sup>3</sup>)

The dielectric parameters of liquids were verified prior to the SAR evaluation using a Speag Dielectric Probe Kit and an Agilent Network Analyzer.

The following table shows the measuring results for simulating liquid.

Frequency (MHz)	Tissue Type	Liquid Temp. (℃)	Conductivity (σ)	Conductivity Target (σ)	Delta (σ) (%)	Limit (%)	Date
2450	HSL	22.1	1.810	1.80	0.56	±5	2024.06.18
5250	HSL	22.1	4.720	4.71	0.21	±5	2024.06.18
5600	HSL	22.1	4.978	5.07	-1.81	±5	2024.06.19
5750	HSL	22.5	5.051	5.22	-3.24	±5	2024.06.20
6500	HSL	22.1	6.020	6.07	-0.82	±5	2024.06.04

### Table 1: Dielectric Performance of Tissue Simulating Liquid

Frequency (MHz)	Tissue Type	Liquid Temp. (℃)	Permittivity (εr)	Permittivity Target (εr)	Delta (εr) (%)	Limit (%)	Date
2450	HSL	22.1	39.440	39.20	0.61	±5	2024.06.18
5250	HSL	22.1	35.760	35.95	-0.53	±5	2024.06.18
5600	HSL	22.1	35.000	35.50	-1.41	±5	2024.06.19
5750	HSL	22.5	34.500	35.35	-2.40	±5	2024.06.20
6500	HSL	22.1	34.300	34.46	-0.46	±5	2024.06.04

Note:



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According to April 2019 TCB Workshop that FCC has permitted the use of single head-tissue simulating liquid specified in IEC 62209-1 for all SAR tests.

## 8 SAR System Verification

Each DASY system is equipped with one or more system validation kits. These units, together with the predefined measurement procedures within the DASY software, enable the user to conduct the system performance check and system validation. System validation kit includes a dipole, tripod holder to fix it underneath the flat phantom and a corresponding distance holder.

### System Validation

According to FCC KDB 865664 D02, SAR system verification is required to confirm measurement accuracy. The SAR systems (including SAR probes, system components and software versions) used for this device were validated against its performance specifications prior to the SAR measurements. Reference dipoles are used with the required tissue-equivalent media for system validation, according to the procedures outlined in FCC KDB 865664 D01 and IEEE 1528-2013. Since SAR probe calibrations are frequency dependent, each probe calibration point must be validated at a frequency within the valid frequency range of the probe calibration point, using the system that normally operates with the probe for routine SAR measurements and according to the required tissue-equivalent media. A tabulated summary of the system validation status, measurement frequencies, SAR probes, calibrated signal type(s) and tissue dielectric parameters has been included.

### > Purpose of System Performance check

The system performance check verifies that the system operates within its specifications. System and operator errors can be detected and corrected. It is recommended that the system performance check be performed prior to any usage of the system in order to guarantee reproducible results. The system performance check uses normal SAR measurements in a simplified setup with a well characterized source. This setup was selected to give a high sensitivity to all parameters that might fail or vary over time. The system check does not intend to replace the calibration of the components, but indicates situations where the system uncertainty is exceeded due to drift or failure.

### System Setup

In the simplified setup for system evaluation, the EUT is replaced by a calibrated dipole and the power source is replaced by a continuous wave that comes from a signal generator. The calibrated dipole must be placed beneath the flat phantom section of the SAM twin phantom with the correct distance holder. The distance holder should touch the phantom surface with a light pressure at the

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reference marking and be oriented parallel to the long side of the phantom. The equipment setup is shown below:





Fig 8.1 Photo of Dipole Setup

Fig 8.2 System Setup for System Evaluation

### > System Verification Results

Comparing to the original SAR value provided by SPEAG, the verification data should be within its specification of 10%. Below table shows the target SAR and measured SAR after normalized to 1W input power. The table as below indicates the system performance check can meet the variation criterion and the plots can be referred to Annex C of this report.

Dipole S/N	Probe S/N	DAE S/N
D2450V2-805	3823	480
D5GHzV2-1176-5250	3823	480
D5GHzV2-1176-5600	3823	480
D5GHzV2-1176-5750	3823	480
D6.5GHzV2-1054	7608	480

Frequency (MHz)	Tissuo	Conductivity	Permittivity (εr)	CW Signal Validation			
	Туре	(σ)		Sensitivity	Probe Linearity	Probe Isotropy	
750	HSL	0.851	42.43	PASS	PASS	PASS	
835	HSL	0.898	41.88	PASS	PASS	PASS	
1750	HSL	1.386	39.91	PASS	PASS	PASS	
1800	HSL	1.449	41.26	PASS	PASS	PASS	
1900	HSL	1.435	39.65	PASS	PASS	PASS	
2000	HSL	1.451	39.42	PASS	PASS	PASS	



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2300	HSL	1.764	38.99	PASS	PASS	PASS
2450	HSL	1.863	38.85	PASS	PASS	PASS
2600	HSL	1.973	38.58	PASS	PASS	PASS
5250	HSL	4.528	35.32	PASS	PASS	PASS
5600	HSL	4.905	34.89	PASS	PASS	PASS
5750	HSL	5.077	34.28	PASS	PASS	PASS
6500	HSL	6.07	34.46	PASS	PASS	PASS
•	•	•	•	•	•	•

Frequency	Tissuo	Conductivity	Pormittivity	Modulati	on Signal V	alidation
(MHz)	Туре	(σ)	(Er)	Mod. Type	Duty Factor	PAR
750	HSL	0.851	42.43	N/A	N/A	N/A
835	HSL	0.898	41.88	GMSK	PASS	N/A
1750	HSL	1.386	39.91	N/A	N/A	N/A
1800	HSL	1.449	41.26	N/A	N/A	N/A
1900	HSL	1.435	39.65	GMSK	PASS	N/A
2000	HSL	1.451	39.42	GMSK	PASS	N/A
2300	HSL	1.764	38.99	OFDM	PASS	PASS
2450	HSL	1.863	38.85	OFDM	PASS	PASS
2600	HSL	1.973	38.58	TDD	PASS	N/A
5250	HSL	4.528	35.32	OFDM	N/A	PASS
5600	HSL	4.905	34.89	OFDM	N/A	PASS
5750	HSL	5.077	34.28	OFDM	N/A	PASS
6500	HSL	6.07	34.46	OFDM	N/A	PASS

#### <Validation Results>

Date	Freq. (MHz)	Tissue Type	Input Power (mW)	Measured 1g SAR (W/kg)	Targeted 1g SAR (W/kg)	Normalized 1g SAR (W/kg)	Deviation (%)
2024.06.18	2450	HSL	250	12.71	52.30	50.84	-2.79
2024.06.18	5250	HSL	100	8.01	76.70	80.1	4.43
2024.06.19	5600	HSL	100	8.13	80.80	81.3	0.62
2024.06.20	5750	HSL	100	8.20	78.70	82	4.19
2024.06.04	6500	HSL	100	31.10	288.00	311	7.99



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Date	Freq. (MHz)	Tissue Type	Input Power (mW)	Measured 10g SAR (W/kg)	Targeted 10g SAR (W/kg)	Normalized 10g SAR (W/kg)	Deviation (%)
2024.06.18	2450	HSL	250	6.03	23.90	24.12	0.92
2024.06.18	5250	HSL	100	2.36	22.10	23.6	6.79
2024.06.19	5600	HSL	100	2.34	23.30	23.4	0.43
2024.06.20	5750	HSL	100	2.41	22.50	24.1	7.11
2024.06.04	6500	HSL	100	5.13	53.10	51.3	-3.39

Date	Freq. (MHz)	Tissue Type	Input Power (mW)	Measured 4cm <sup>2</sup> APD (W/m <sup>2</sup> )	Targeted 4cm <sup>2</sup> APD (W/m <sup>2</sup> )	Normalized 4cm <sup>2</sup> APD (W/m <sup>2</sup> )	Deviation (%)
2024.06.04	6500	HSL	100	139.00	1310.00	1390	6.11

Note: System checks the specific test data please see Annex C.



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### 8.1 PD System Verification Source

### General description

The EUT is replaced by a calibrated source, the same spatial resolution, measurement region and test separation used in the calibration was applied to system check. Through visual inspection into the measured power density distribution, both the spatially (shape) and numerically (level) have no noticeable difference. The measurement results should be within  $\pm 10\%$  of the calibrated targets.

Frequency [GHz]	Grid step	Grid extent X/Y [mm]	Measurement points
10	$0.25 \left(\frac{\lambda}{4}\right)$	120/120	$16 \times 16$
30	$0.25~(\frac{\bar{\lambda}}{4})$	60/60	$24 \times 24$
60	$0.25 \ (\frac{\hat{\lambda}}{4})$	32.5/32.5	$26 \times 26$
90	$0.25 \ (\frac{\dot{\lambda}}{4})$	30/30	36 imes 36



Fig 8.3 Photos of Verification Setup

### Validation Results

After system check testing, the results of power density will be compared with the reference value derived from the certificate report. The deviation of system check should be within  $\pm 10\%$ .

### <Validation Setup>

Frequency	6 EC Varification Source	Probe	DAE
(GHz)	6.5G vernication Source	S/N	S/N
10	10GHz-SN 1019	9602	480



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### <Validation Results>

Date	Frequency (GHz)	Test Distance (mm)	Measured 4cm² pStotavg (W/m²)	Targeted 4cm <sup>2</sup> pStotavg (W/m <sup>2</sup> )	Deviation (%)
2024.06.05	10	5.5	40.8	44.8	-8.9

Note: System checks the specific test data please see Annex C.

## 9 EUT Testing Position

This EUT was tested in two different positions. They are Bottom Face/Edge 1 of the EUT with phantom 0 mm gap, as illustrated below, please refer to Annex B for the test setup photos.

### 9.1 SAR Evaluation to the Mouth/Jaw Regions of the Phantom

Antennas located near the bottom of a phone may require SAR measurements around the mouth and jaw regions of the SAM head phantom. This typically applies to clam-shell style phones that are generally longer in the unfolded normal use positions or to certain older style long rectangular phones.

Under these circumstances, the following procedures apply, adopted from the FCC guidance on SAR handsets document FCC KDB Publication 648474 D04v01r03. The SAR required in these regions of SAM should be measured using a flat phantom. The phone should be positioned with a separation distance of 4 mm between the ear reference point (ERP) and the outer surface of the flat phantom shell. While maintaining this distance at the ERP location, the low (bottom) edge of the phone should be lowered from the phantom to establish the same separation distance between the peak SAR locations identified by the truncated partial SAR distribution measured with the SAM phantom. The distance from the peak SAR location to the phone is determined by the straight line passing perpendicularly through the phantom surface. When it is not feasible to maintain 4 mm separation at the ERP while also establishing the required separation at the peak SAR location, the top edge of the phone will be allowed to touch the phantom with a separation < 4 mm at the ERP. The phone should not be tilted to the left or right while placed in this inclined position to the flat phantom.

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### 9.2 Body-Supported Device Configurations

According to KDB 616217 section 4.3, SAR should be separately assessed with each surface and separation distance positioned against the flat phantom that correspond to the intended use as specified by the manufacturer. The antennas in tablets are typically located near the back (bottom) surface and/or along the edges of the devices; therefore, SAR evaluation is required for these configurations. Exposures from antennas through the front (top) surface of the display section of a full-size tablet, away from the edges, are generally limited to the user's hands. Exposures to hands for typical consumer transmitters used in tablets are not expected to exceed the extremity SAR limit; therefore, SAR evaluation for the front surface of tablet display screens are generally not necessary, except for tablets that are designed to require continuous operations with the hand(s) next to the antenna(s).

- > To position the device parallel to the phantom surface with either keypad up or down.
- > To adjust the device parallel to the flat phantom.
- > To adjust the distance between the device surface and the flat phantom to 0 mm.
- When each surface is measurement, the SAR Test Exclusion Threshold in KDB 447498 should be applied.



Fig.9.5 Illustration for Body Position



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### 9.3 Wireless Router (Hotspot) Configurations

Some battery-operated handsets have the capability to transmit and receive internet connectivity through simultaneous transmission of WIFI in conjunction with a separate licensed transmitter. The FCC has provided guidance in KDB Publication 941225 D06 where SAR test considerations for handsets (L x W  $\geq$ 

9 cm x 5 cm) are based on a composite test separation distance of 10 mm from the front, back and edges of the device with antennas 2.5 cm or closer to the edge of the device, determined from general mixed use conditions for this type of devices. Since the hotspot SAR results may overlap with the body-worn accessory SAR requirements, the more conservative configurations can be considered, thus excluding some body-worn accessory SAR tests.

When the user enables the personal wireless router functions for the handset, actual operations include simultaneous transmission of both the WIFI transmitter and another licensed transmitter. Both transmitters often do not transmit at the same transmitting frequency and thus cannot be evaluated for SAR under actual use conditions. Therefore, SAR must be evaluated for each frequency transmission and mode separately and summed with the WIFI transmitter according to KDB 648474 publication procedures. The "Portable Hotspot" feature on the handset was NOT activated, to ensure the SAR measurements were evaluated for a single transmission frequency RF signal.



#### Fig.9.6 Illustration for Hotspot Position

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## **10 Measurement Procedures**

The measurement procedures are as bellows:

### <Conducted power measurement>

- For WWAN power measurement, use base station simulator to configure EUT WWAN transition in conducted connection with RF cable, at maximum power in each supported wireless interface and frequency band.
- > Read the WWAN RF power level from the base station simulator.
- For WLAN/BT power measurement, use engineering software to configure EUT WLAN/BT continuously transmission, at maximum RF power in each supported wireless interface and frequency band.
- Connect EUT RF port through RF cable to the power meter or spectrum analyzer, and measure WLAN/BT output power.

#### <Conducted power measurement>

- Use base station simulator to configure EUT WWAN transmission in radiated connection, and engineering software to configure EUT WLAN/BT continuously transmission, at maximum RF power, in the highest power channel.
- > Place the EUT in positions as Annex B demonstrates.
- > Set scan area, grid size and other setting on the DASY software.
- > Measure SAR results for the highest power channel on each testing position.
- > Find out the largest SAR result on these testing positions of each band.
- Measure SAR results for other channels in worst SAR testing position if the Reported SAR or highest power channel is larger than 0.8 W/kg.

According to the test standard, the recommended procedure for assessing the peak spatial-average SAR value consists of the following steps:

- > Power reference measurement.
- Area scan.
- Zoom scan.
- > Power drift measurement.



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### **10.1 Spatial Peak SAR Evaluation**

The procedure for spatial peak SAR evaluation has been implemented according to the test standard. It can be conducted for 1g and 10g, as well as for user-specific masses. The DASY software includes all numerical procedures necessary to evaluate the spatial peak SAR value.

The base for the evaluation is a "cube" measurement. The measured volume must include the 1g and 10 g cubes with the highest averaged SAR values. For that purpose, the center of the measured volume is aligned to the interpolated peak SAR value of a previously performed area scan.

The entire evaluation of the spatial peak values is performed within the post-processing engine (SEMCAD). The system always gives the maximum values for 1g and 10g cubes. The algorithm to find the cube with highest averaged SAR is divided into the following stages:

- Extraction of the measured data (grid and values) from the Zoom Scan.
- Calculation of the SAR value at every measurement point based on all stored data (A/D values and measurement parameters).
- Generation of a high-resolution mesh within the measured volume.
- > Interpolation of all measured values form the measurement grid to the high-resolution grid
- Extrapolation of the entire 3-D field distribution to the phantom surface over the distance from sensor to surface
- > Calculation of the averaged SAR within masses of 1g and 10g.

### **10.2 Power Reference Measurement**

The Power Reference Measurement and Power Drift Measurement are for monitoring the power drift of the device under test in the batch process. The minimum distance of probe sensors to surface determines the closest measurement point to phantom surface. This distance cannot be smaller than the distance of sensor calibration points to probe tip as defined in the probe properties.

### 10.3 Area Scan Procedures

Area scans are defined prior to the measurement process being executed with a user defined variable spacing between each measurement point (integral) allowing low uncertainty measurements to be conducted. Scans defined for FCC applications utilize a10mm<sup>2</sup> step integral, with 1mm interpolation used to locate the peak SAR area used for zoom scan assessments.



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When an Area Scan has measured all reachable points, it computes the field maxima found in the scanned area, within a range of the global maximum. The range (in dB) is specified in the standards for compliance testing.

### **10.4 Zoom Scan Procedures**

Zoom Scans are used to assess the peak spatial SAR values within a cubic averaging volume containing 1 g and 10 g of simulated tissue. A density of 1000 kg/m<sup>3</sup> is used to represent the head and body tissue density and not the phantom liquid density, in order to be consistent with the definition of the liquid dielectric properties, i.e. the side length of the 1g cube is 10mm, with the side length of the 10 g cube 21,5mm. The zoom scan integer steps can be user defined so as to reduce uncertainty, but normal practice for typical test applications utilize a physical step of 5x5x7 (8mmx8mmx5mm) providing a volume of 32mm in the X & Y axis, and 30mm in the Z axis.

### **10.5 SAR Averaged Methods**

In DASY, the interpolation and extrapolation are both based on the modified Quadratic Sheppard's method. The interpolation scheme combines a least-square fitted function method and a weighted average method which are the two basic types of computational interpolation and approximation.

Extrapolation routines are used to obtain SAR values between the lowest measurement points and the inner phantom surface. The extrapolation distance is determined by the surface detection distance and the probe sensor offset. The uncertainty increases with the extrapolation distance. To keep the uncertainty within 1% for the 1g and 10g cubes, the extrapolation distance should not be larger than 5 mm.

### 10.6 Power Drift Monitoring

All SAR testing is under the EUT install full charged battery and transmit maximum output power. In DASY measurement software, the power reference measurement and power drift measurement procedures are used for monitoring the power drift of EUT during SAR test. Both these procedures measure the field at a specified reference position before and after the SAR testing. The software will calculate the field difference in dB. If the power drifts more than 5%, the SAR will be retested.



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## **11 Power Density Measurement Procedure**

### > Computation of the Electric Field Polarization Ellipse

For the numerical description of an arbitrarily oriented ellipse in three-dimensional space, five parameters are needed: the semi-major axis (a), the semi-minor axis (b), two angles describing the orientation of the normal vector of the ellipse ( $\phi$ ,  $\theta$ ), and one angle describing the tilt of the semi-major axis ( $\Psi$ ). For the two extreme cases, i.e. circular and linear polarizations, three parameters only (a,  $\phi$  and  $\theta$ ) are sufficient for the description of the incident field.





For the construction of the ellipse parameters from measured data, the problem can be reformulated as a nonlinear search problem. The semi-major and semi-minor axes of an elliptical field can be express as functions of the three angles ( $\phi$ ,  $\theta$  and  $\Psi$ ). The parameters can be uniquely determined towards minimizing the error based on least-squares for the given set of angles and the measured data. In this way, the numbers of three parameters is reduced from five to three, which means that least three sensors readings are necessary to gain sufficient information for the reconstruction of ellipse parameters. However, to suppress the noise and increase the reconstruction accuracy, it is desirable to have an over determined system of equations. The solution to use a probe consisting of two sensors angled by  $\gamma$  1 and  $\gamma$  2 toward the probe axis and to perform measurements at three angular positions of the probe, i.e. at  $\beta$  1,  $\beta$  2 and  $\beta$  3, results in over determination of two. If there is a need for more information or increased accuracy, more rotation angles can be added.

The reconstruction of ellipse parameters can be separated into linear and non-linear parts that are best solved by the givens algorithm combined with a downhill simplex algorithm. To minimize the mutual coupling, sensor angles are set with a 90° shift ( $\gamma 1 = \gamma 2 + 90°$ ), and, to simplify, the first rotation angle of the probe ( $\beta 1$ ) can be set to 0°.



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### > Total Field and Power Flux Density Reconstruction

Computation of the power density in general requires knowledge of the electric and magnetic field amplitudes and phases in the plane of incidence. Reconstruction of these quantities from pseudo-vector E-field measurements is feasible, as they are constrained by Maxi well,s equations. The SPEAG have developed a reconstruction approach based on the Gerchberg-Saxton algorithm, which benefits from the availability of the E-Field polarization ellipse information obtained with the EUmmWV2 probe. This reconstruction algorithm, together with the ability of the probe to measure extremely close to the source without perturbing the field, permits reconstruction of the E-field and H-field, as well as of the power density, on measurement planes located as near as  $\lambda$ /5 away.

#### > Power Flux Density Averaging

The average of the reconstructed power density is evaluated over a circular area in each measurement plane. The area of the circle is defined by the user; the default is 1cm2. The computed peak average value is displayed in the box at the top right. Note that the average is evaluated only for grid points where the averaging circle is completely filed with values; for points at the edge where the averaging circle is only partly filled with values, the average power density is set to zero. Two average power density values are computed.



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## **12 SAR Test Configuration**

### <WLAN 2.4GHz>

- 1. SAR is measured for 2.4 GHz 802.11b DSSS using either the fixed test position or, when applicable, the initial test position procedure. SAR test reduction is determined according to the following:
  - a. When the reported SAR of the highest measured maximum output power channel for the exposure configuration is  $\leq 0.8$  W/kg, no further SAR testing is required for 802.11b DSSS in that exposure configuration.
  - b. When the reported SAR is > 0.8 W/kg, SAR is required for that position using the next highest measured output power channel. When any reported SAR is > 1.2 W/kg, SAR is required for the third channel; i.e., all channels require testing.
- 2.4 GHz 802.11 g/n OFDM are additionally evaluated for SAR if the highest reported SAR for 802.11b, adjusted by the ratio of the OFDM to DSSS specified maximum output power, is > 1.2 W/kg. When SAR is required for OFDM modes in 2.4 GHz band, the Initial Test configuration Procedures should be followed.
- 3. For held-to-ear and hotspot operations, the initial test position procedures were applied. The test position with the highest extrapolated peak SAR will be used as the initial test position. When reported SAR for the initial test position is ≤ 0.4 W/kg, no additional testing for the remaining test positions was required. Otherwise, SAR is evaluated at the subsequent highest peak SAR positions until the reported SAR result is ≤ 0.8 W/kg or all test positions are measured.
- 4. Justification for test configurations for WLAN per KDB Publication 248227 D02DR02-41929 for 2.4 GHz WI-FI single transmission chain operations, the highest measured maximum output power channel for DSSS was selected for SAR measurement. SAR for OFDM modes (2.4 GHz802.11g/n) was not required due to the maximum allowed powers and the highest reported SAR.
- 5. A fixed level power reduction is applied for WiFi when handset operates "held to the body" condition or "held to the ear" condition, the power reduction triggered by audio receiver detection and call establish status.
- Per KDB 248227 D01v02r02, In the 2.4 GHz band, separate SAR procedures are applied to DSSS and OFDM configurations to simplify DSSS test requirements.SAR is not required for the following 2.4 GHz OFDM conditions:
  - a. When KDB Publication 447498 SAR test exclusion applies to the OFDM configuration.
  - b. When the highest reported SAR for DSSS is adjusted by the ratio of OFDM to DSSS specified maximum output power and the adjusted SAR is  $\leq$  1.2 W/kg.



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#### <WLAN 5GHz>

#### A) U-NII-1 and U-NII-2A Bands

For devices that operate in only one of the U-NII-1 and U-NII-2A bands, the normally required SAR procedures for OFDM configurations are applied. For devices that operate in both U-NII bands using the same transmitter and antenna(s), SAR test reduction is determined according to the following:

- When the same maximum output power is specified for both bands, begin SAR measurement in U- NII-2A band by applying the OFDM SAR requirements. If the highest reported SAR for a test configuration is ≤ 1.2 W/kg, SAR is not required for U-NII-1 band for that configuration (802.11 mode and exposure condition); otherwise, both bands are tested independently for SAR.
- 2. When different maximum output power is specified for the bands, begin SAR measurement in the band with higher specified maximum output power. The highest reported SAR for the tested configuration is adjusted by the ratio of lower to higher specified maximum output power for the two bands. When the adjusted SAR is ≤ 1.2 W/kg, SAR is not required for the band with lower maximum output power in that test configuration; otherwise, both bands are tested independently for SAR.
- 3. The two U-NII bands may be aggregated to support a 160 MHz channel on channel number 50.
- 4. Without additional testing, the maximum output power for this is limited to the lower of the maximum output power certified for the two bands. When SAR measurement is required for at least one of the bands and the highest reported SAR adjusted by the ratio of specified maximum output power of aggregated to standalone band is > 1.2 W/kg, SAR is required for the 160 MHz channel. This procedure does not apply to an aggregated band with maximum output higher than the standalone band(s); the aggregated band must be tested independently for SAR. SAR is not required when the 160 MHz channel is operating at a reduced maximum power and also qualifies for SAR test exclusion.

#### B) U-NII-2C and U-NII-3 Bands

The frequency range covered by these bands is 380 MHz (5.47 - 5.85 GHz), which requires a minimum of at least two SAR probe calibration frequency points to support SAR measurements. when Terminal Doppler Weather Radar (TDWR) restriction applies, all channels that operate at 5.60 - 5.65 GHz must be included to apply the SAR test reduction and measurement procedures. When the same transmitter and antenna(s) are used for U-NII-2C band and U-NII-3 band or 5.8 GHz band of §15.247, the bands may be aggregated to enable additional channels with 20, 40 or 80 MHz bandwidth to span across the band gap, as illustrated in Appendix B. The maximum output power for the additional band gap channels is limited to the lower of those certified for the bands. Unless band gap channels are permanently disabled, they must be considered for SAR testing. The frequency range covered by these bands is 380 MHz (5.47 - 5.85 GHz), which requires a minimum of at least two SAR probe calibration frequency points to support SAR measurements. To maintain SAR measurement accuracy and to facilitate test reduction, the channels in U-NII-2C band above 5.65 GHz may be grouped with the 5.8 GHz channels in U-NII-3 or §15.247 band to enable two

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SAR probe calibration frequency points to cover the bands, including the band gap channels. When band gap channels are supported and the bands are not aggregated for SAR testing, band gap channels must be considered independently in each band according to the normally required OFDM SAR measurement and probe calibration frequency points requirements.

### C) OFDM Transmission Mode SAR Test Configuration and Channel Selection Requirements

The initial test configuration for 5 GHz OFDM transmission modes is determined by the 802.11 configuration with the highest maximum output power specified for production units, including tune-up tolerance, in each standalone and aggregated frequency band. SAR for the initial test configuration is measured using the highest maximum output power channel determined by the default power measurement procedures. When multiple configurations in a frequency band have the same specified maximum output power, the initial test configuration is determined according to the following steps applied sequentially.

- 1. The largest channel bandwidth configuration is selected among the multiple configurations with the same specified maximum output power.
- 2. If multiple configurations have the same specified maximum output power and largest channel bandwidth, the lowest order modulation among the largest channel bandwidth configurations is selected.
- 3. If multiple configurations have the same specified maximum output power, largest channel band width and lowest order modulation, the lowest data rate configuration among these configurations is selected.
- 4. When multiple transmission modes (802.11a/g/n/ac) have the same specified maximum output power, largest channel bandwidth, lowest order modulation and lowest data rate, the lowest order 802.11 mode is selected; i.e., 802.11a is chosen over 802.11n then 802.11ac or 802.11g is chosen over 802.11n. After an initial test configuration is determined, if multiple test channels have the same measured maximum output power, the channel chosen for SAR measurement is determined according to the following. These channel selection procedures apply to both the initial test configuration and subsequent test configuration(s), with respect to the default power measurement procedures or additional power measurements required for further SAR test reduction. The same procedures also apply to subsequent highest output power channel(s) selection.
- 5. The channel closest to mid-band frequency is selected for SAR measurement.
- 6. For channels with equal separation from mid-band frequency; for example, high and low channels or two mid-band channels, the higher frequency (number) channel is selected for SAR measurement.



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#### D) SAR Test Requirements for OFDM configurations

When SAR measurement is required for 802.11 a/n/ac OFDM configurations, each standalone and frequency aggregated band is considered separately for SAR test reduction. When the sametransmitter and antenna(s) are used for U-NII-1 and U-NII-2A bands, additional SAR test reduction Vapplies. When band gap channels between U-NII-2C band and 5.8 GHz U-NII-3 or §15.247 bandare supported, the highest maximum output power transmission mode configuration and maximumoutput power channel across the bands must be used to determine SAR test reduction, accordingto the initial test configuration and subsequent test configuration requirements. In applying theinitial test configuration and subsequent test configuration procedures, the 802.11 transmissionconfiguration with the highest specified maximum output power and the channel within a testconfiguration with the highest measured maximum output power should be clearly distinguished toapply the procedures.



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## **13 Conducted Output Power**

Remark: The maximum output power and mode of WLAN/Bluetooth were recorded in annex E of this report. For the complete output power test results of WLAN/Bluetooth, please refer to the test report numbers 200611-04. TR04, 200611-04. TR01, 200611-04. TR05 and 200611-04. TR38.

## **14 Exposure Positions Consideration**

> EUT Antenna Locations

The antenna location was shown in annex B.

WIFI 1 (ChainB): TX/RX: WLAN 2.4GHz/5GHz/6GHz

WIFI 2 (Chain A): TX/RX: WLAN 2.4GHz/5GHz/6GHz, Bluetooth

### > Test Positions Consideration

- 1. The test position consideration was recorded in annex F.
- Per KDB 616217 D04v01r02, when the overall diagonal dimension of display is > 20 cm, the test distance is 0mm; the SAR Test Exclusion Threshold in KDB 447498 section 4.3.1 can be applied to determine SAR test exclusion for adjacent edge configurations.
- 3. Per KDB 616217 D04v01r02, SAR evaluation for the front surface of tablet display screens is generally not necessary.
- 4. Per KDB 616217 D04v01r02, additional testing for hotspot SAR is not required.
- 5. For WLAN bands, bottom face and edge 1 would be tested in this report.





## **15 SAR Test Results Summary**

### 15.1 Test Guidance

- 1. The reported SAR is the measured SAR value adjusted for maximum tune-up tolerance.
  - a. Tune-up scaling Factor = tune-up limit power (mW) / EUT RF power (mW), where tune-up limit is the maximum rated power among all production units.
  - b. For SAR testing of WLAN signal with non-100% duty cycle, the measured SAR is scaled-up by the duty cycle scaling factor which is equal to "1 / (duty cycle)".
  - c. For WLAN/Bluetooth: Reported SAR (W/kg) = Measured SAR(W/kg) \* Duty Cycle scaling factor \* Tune-up scaling factor.
- 2. Per KDB 447498 D01v06, for each exposure position, testing of other required channels within the operating mode of a frequency band is not required when the *reported* 1-g or 10-g SAR for the mid-band or highest output power channel is:
  - a. ≤ 0.8 W/kg or 2.0 W/kg, for 1-g or 10-g respectively, when the transmission band is ≤ 100 MHz.
  - b. ≤ 0.6 W/kg or 1.5 W/kg, for 1-g or 10-g respectively, when the transmission band is between 100 MHz and 200 MHz.
  - c.  $\leq$  0.4 W/kg or 1.0 W/kg, for 1-g or 10-g respectively, when the transmission band is  $\geq$  200 MHz.
- 3. Per KDB248227 D01v02r02, a Wi-Fi device must be configured to transmit continuously at the required data rate, channel bandwidth and signal modulation, using the highest transmission duty factor supported by the test mode tools for SAR measurement. The test frequencies established using test mode must correspond to the actual channel frequencies required for operations in the U.S. When 802.11 frame gaps are accounted for in the transmission, a maximum transmission duty factor of 92 - 96% is typically achievable in most test mode configurations. A minimum transmission duty factor of 85% is required to avoid certain hardware and device implementation issues related to wide range SAR scaling. In addition, a periodic transmission duty factor is required for current generation SAR systems to measure SAR correctly. Unless it is permitted by specific KDB procedures or continuous transmission is specifically restricted by the device, the reported SAR must be scaled to 100% transmission duty factor to determine compliance at the maximum tune-up tolerance limit. When a device is not capable of sustaining continuous transmission or the output can become nonlinear, and it is limited by hardware design and unable to transmit at higher than 85% duty factor, a periodic duty factor within 15% of the maximum duty factor the device is capable of transmitting should be used. The reported SAR must be scaled to the maximum transmission duty factor to determine compliance. Descriptions of the procedures applied to establish the specific duty factor used for SAR testing are required in SAR reports to support the test results.
- 4. According to TCBC workshop in April 2021, start with minimum of 5 test channels across full

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5925-7125 MHz band and adapt conducted power and SAR test reduction procedures of KDB 248227 v02r02.

### 15.2 Body SAR Data

### > WLAN 2.4GHz/5GHz/Bluetooth Body SAR

Plot No.	Band/Mode	Test Position	CH.	Ave. Power	Tune-up Limit	Tune-up Scaling	Meas. SAR <sub>1g</sub>	Reported SAR <sub>1g</sub>				
			WIEL2 (Ch	(dBm) ain A)	(dBm)	Factor	(W/kg)	(W/kg)				
1#	WI AN2 4GHz/802 11b	Bottom Face		21.05	22.00	1 245	0 165	0 205				
117	WLAN2 4GHz/802 11b	Edge 1	1	21.00	22.00	1.245	0.027	0.034				
	WIFL1 (Chain B)											
	WLAN2.4GHz/802.11b	Bottom Face	7	21.12	22.00	1.225	0.033	0.040				
	WLAN2.4GHz/802.11b	Edge 1	7	21.12	22.00	1.225	0.022	0.027				
			MIMO	)								
	WLAN2.4GHz/802.11n20	Bottom Face	7	22.96	24.00	1.271	0.027	0.034				
	WLAN2.4GHz/802.11n20	Edge 1	7	22.96	24.00	1.271	0.017	0.022				
			WIFI 2 (Ch	ain A)								
2#	WLAN5.2GHz/802.11n40	Bottom Face	46	21.04	22.00	1.247	0.265	0.335				
	WLAN5.2GHz/802.11n40	Edge 1	46	21.04	22.00	1.247	0.086	0.109				
	WIFI 1 (Chain B)											
	WLAN5.2GHz/802.11n40	Bottom Face	46	21.03	22.00	1.250	0.112	0.142				
	WLAN5.2GHz/802.11n40	Edge 1	46	21.03	22.00	1.250	0.083	0.105				
			MIMC	)								
	WLAN5.2GHz/802.11n40	Bottom Face	46	23.41	24.50	1.285	0.234	0.304				
	WLAN5.2GHz/802.11n40	Edge 1	46	23.41	24.50	1.285	0.066	0.086				
			WIFI 2 (Ch	ain A)								
	WLAN5.3GHz/802.11ax40	Bottom Face	54	21.09	22.00	1.233	0.117	0.146				
	WLAN5.3GHz/802.11ax40	Edge 1	54	21.09	22.00	1.233	0.061	0.076				
			WIFI 1 (Cha	ain B)	1							
	WLAN5.3GHz/802.11n40	Bottom Face	54	21.2	22.00	1.202	0.086	0.105				
	WLAN5.3GHz/802.11n40	Edge 1	54	21.2	22.00	1.202	0.037	0.045				
			MIMC	)	1							
3#	WLAN5.3GHz/802.11ax20	Bottom Face	56	22.1	22.50	1.096	0.157	0.173				
	WLAN5.3GHz/802.11ax20	Edge 1	56	22.1	22.50	1.096	0.083	0.092				
			WIFI 2 (Ch	ain A)	I							
4#	WLAN5.5GHz/802.11n40	Bottom Face	118	21.02	22.00	1.253	0.138	0.175				
	WLAN5.5GHz/802.11n40	Edge 1	118	21.02	22.00	1.253	0.076	0.096				



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WIFI 1 (Chain B)												
	WLAN5.5GHz/802.11n40	Bottom Face	118	21.10	22.00	1.230	0.038	0.047				
	WLAN5.5GHz/802.11n40	Edge 1	118	21.10	22.00	1.230	0.034	0.042				
	MIMO											
	WLAN5.5GHz/802.11n40         Bottom Face         118         23.86         24.50         1.159         0.092         0.103											
	WLAN5.5GHz/802.11n40	Edge 1	118	23.86	24.50	1.159	0.085	0.100				
	WIFI 2 (Chain A)											
5#	WLAN5.8GHz/802.11n40	Bottom Face	151	21.05	22.00	1.245	0.241	0.304				
	WLAN5.8GHz/802.11n40	Edge 1	151	21.05	22.00	1.245	0.077	0.097				
			WIFI 1 (Ch	ain B)								
	WLAN5.8GHz/802.11n20	Bottom Face	165	21.05	22.00	1.245	0.100	0.126				
	WLAN5.8GHz/802.11n20	Edge 1	165	21.05	22.00	1.245	0.090	0.113				
			MIMC	)								
	WLAN5.8GHz/802.11n40	Bottom Face	151	24.10	25.00	1.230	0.121	0.151				
	WLAN5.8GHz/802.11n40	Edge 1	151	24.10	25.00	1.230	0.075	0.093				
			WIFI 2 (Ch	ain A)								
6#	Bluetooth/DH5	Bottom Face	78	11.04	12	1.247	0.063	0.086				
	Bluetooth/DH5	Edge 1	78	11.04	12	1.247	0.020	0.027				

#### Note:

1. Per KDB 447498 D01v06, for each exposure position, if the highest output channel Reported SAR ≤0.8W/kg, other channels SAR testing is not necessary.

- 2. Additional WLAN SAR testing was performed for simultaneous transmission analysis.
- 3. Per KDB 865664 D01v01r04, for each frequency band, repeated SAR measurement is required when the measured SAR is ≥0.8W/kg.
- 4. Per KDB248227 D01v02r02, OFDM SAR is not required when the highest reported SAR for DSSS is adjusted by the ratio of OFDM to DSSS specified maximum output power and the adjusted SAR is  $\leq$  1.2 W/kg.
- 5. According to KDB 865664 D02v01r02, SAR plot is required for the highest measured SAR in each exposure configuration, wireless mode and frequency band combination.
- The WLAN 2.4GHz Reported 1g SAR (W/kg) should be scaled with the duty cycle scaling factor 1.000 for 802.11b, 1.000 for WLAN 2.4GHz 802.11n20, 1.011 for WLAN 5GHz 802.11n20, 1.012 for WLAN 5GHz 802.11n40, 1.012 for WLAN 5GHz 802.11ax40 and 1.006 for WLAN 5GHz 802.11ax20.
- 7. According to 2016 Oct. TCB workshop for Bluetooth SAR consideration and the theoretical dut y cycle is 83.3%, therefore the actual duty cycle will be scaled up to the theoretical value of Bluetooth reported SAR calculation. The duty cycle of Bluetooth is 76.27%, therefore the duty cycle scaling factor 1.092 should be used to calculating the reported SAR.



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### REPORT No.: SZ24040355S01

### > WLAN 6GHz Body SAR

Plot No.	Band	Mode	Test Position	CH.	Ave. Power (dBm) 2 (Chain A)	Tune-up Limit (dBm)	Tune-up Scaling Factor	Meas. SAR1g (W/kg)	Reported SAR1g (W/kg)	Meas. 4cm <sup>2</sup> APD (W/m <sup>2</sup> )
	U-NII-5	802.11ax160	Bottom Face	79	13.89	15.00	1.291	0.161	0.210	0.569
	U-NII-5	802.11ax160	Edge 1	79	13.89	15.00	1.291	0.150	0.196	1.170
				WIFI	1 (Chain B)	)				
7#	U-NII-5	802.11ax160	Bottom Face	15	13.72	14.50	1.197	0.579	0.701	0.950
	U-NII-5	802.11ax160	Edge 1	15	13.72	14.50	1.197	0.265	0.321	1.260
					MIMO					
	U-NII-5	802.11ax160	Bottom Face	79	13.29	14.00	1.178	0.506	0.602	1.000
	U-NII-5	802.11ax160	Edge 1	79	13.29	14.00	1.178	0.181	0.215	0.957
				WIFI	2 (Chain A)	)				
	U-NII-6	802.11ax160	Bottom Face	111	13.48	14.50	1.265	0.259	0.331	1.050
	U-NII-6	802.11ax160	Edge 1	111	13.48	14.50	1.265	0.191	0.244	1.320
				WIFI	1 (Chain B)	)				
8#	U-NII-6	802.11ax160	Bottom Face	111	13.08	14.00	1.236	0.574	0.718	3.350
	U-NII-6	802.11ax160	Edge 1	111	13.08	14.00	1.236	0.346	0.433	2.170
					MIMO					
	U-NII-6	802.11ax160	Bottom Face	111	13.50	14.50	1.259	0.468	0.596	1.620
	U-NII-6	802.11ax160	Edge 1	111	13.50	14.50	1.259	0.192	0.244	1.320
				WIFI	2 (Chain A)	)		ſ	1	
	U-NII-7	802.11ax160	Bottom Face	143	13.25	14.00	1.189	0.256	0.308	0.931
	U-NII-7	802.11ax160	Edge 1	143	13.25	14.00	1.189	0.157	0.189	1.200
				WIFI	1 (Chain B)	)		r	1	
9#	U-NII-7	802.11ax160	Bottom Face	143	13.1	14.00	1.230	0.669	0.833	2.530
	U-NII-7	802.11ax160	Edge 1	143	13.1	14.00	1.230	0.323	0.402	2.050
			ſ		МІМО					
	U-NII-7	802.11ax160	Bottom Face	143	13.50	14.50	1.259	0.314	0.400	0.947
	U-NII-7	802.11ax160	Edge 1	143	13.50	14.50	1.259	0.184	0.234	1.270
			Γ	WIFI	2 (Chain A)	)		Γ	Γ	
	U-NII-8	802.11ax160	Bottom Face	207	13.79	14.50	1.178	0.440	0.524	1.830
	U-NII-8	802.11ax160	Edge 1	207	13.79	14.50	1.178	0.315	0.375	2.290
	<b></b>		l	WIFI	1 (Chain B)	)	l	[		<b></b>
10#	U-NII-8	802.11ax160	Bottom Face	207	12.34	13.50	1.306	0.686	0.907	2.870
	U-NII-8	802.11ax160	Edge 1	207	12.34	13.50	1.306	0.386	0.510	2.220



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MIMO										
U-NII-8	802.11ax160	Bottom Face	207	13.32	14.00	1.169	0.286	0.338	0.966	
U-NII-8	802.11ax160	Edge 1	207	13.32	14.00	1.169	0.137	0.162	0.914	

**Note:** The WLAN 6GHz 802.11ax-HEW160 Reported 1g SAR (W/kg) should be scaled with the duty cycle scaling factor 1.012 for SISO, 1.011 for MIMO.



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### **15.3 PD Test Results**

### > General Note

- 1. The reported PD is the measured Total PD value adjusted for maximum tune-up tolerance.
  - a. Tune-up scaling Factor = tune-up limit power (mW) / EUT RF power (mW), where tune-up limit is the maximum rated power among all production units.
  - b. For PD testing of WLAN signal with non-100% duty cycle, the measured PD is scaled-up by the duty cycle scaling factor which is equal to "1 / (duty cycle)".
  - c. For WLAN: Reported PD(W/m<sup>2</sup>)= Measured Total PD(W/m<sup>2</sup>)\* Duty Cycle scaling factor \* Tune-up scaling factor.
- 2. According to the equipment user manual that the most conservative test distance of 2mm was applied to PD measurement and the REC (field reconstruction) component of the uncertainty budget for a given E-field is valid only for  $d \ge \lambda$  /5mm.
- According to TCBC workshop in April 2021 that in addition to tune-up tolerance scaling, adjust measured results per amount that measurement uncertainty exceeds 30% (e.g. per methods of IEC 62479:2010). Total expanded uncertainty of 2.68dB which was converted to 85% was used to determining the psPD measurement scaling factor.
- 4. The duty cycle scaling factor of 1.000 should be calculated the final power density.
- 5. According to TCBC workshop in October 2018 that 4cm<sup>2</sup> averaging area may now be considered.
- 6. RF exposure compliance with PD is demonstrated for various radio configurations using below equation:

Final PD=Mea. psPD<sub>tot+</sub> \* tune-up factor \* duty cycle factor \* Uncertainty Factor

Where Uncertainty factor = 1 + (actual expanded uncertainty - 30%)

- 7. The final psPD should be scaled to the uncertainty factor of 1.55.
- 8. The measurement procedure consists of measuring the PDinc at two different distances: d=2mm (compliance distance) and d= λ /5. The same grid extents and grid steps should be used for both measurements. The grid extents should be large enough to fully capture the transmitted energy. The grid step should be fine enough to demonstrate that the integrated Power Density iPDn varies by less than 1 dB between the d=2mm and d= λ /5 measurements. We recommend using as first approximation a grid step Lgrid that is a function of the distance to the transmitting structure and not larger than:

$$I_{grid} = \begin{cases} 1.25d & \text{for } d < \lambda/5\\ \lambda/4 & \text{for } d \ge \lambda/5 \end{cases}$$

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#### > PD Test Results

		Exposure	Gan			Grin Sten	iPDn	iPDn	Total
Band	Mode	Desition	(mm)	Ant.	Ch.		(\\//m2)	Ratio	psPDtot+
		Position	(mm)	(11111)		(^)	(vv/m-)	(<1dB)	(W/m <sup>2</sup> )
U-NII-5	802.11ax160	Bottom Face	2	WIFI 2	79	0.0625	1.99	0 725	2.720
U-NII-5	802.11ax160	Bottom Face	9.56	WIFI 2	79	0.0625	1.68	0.735	2.189
U-NII-5	802.11ax160	Bottom Face	2	WIFI 1	15	0.0625	2.36	0.607	2.420
U-NII-5	802.11ax160	Bottom Face	9.25	WIFI 1	15	0.0625	2.01	0.097	1.980
U-NII-5	802.11ax160	Bottom Face	2	MIMO	79	0.0625	3.27	0.658	3.380
U-NII-5	802.11ax160	Bottom Face	9.06	MIMO	79	0.0625	2.81	0.000	2.970
U-NII-6	802.11ax160	Bottom Face	2	WIFI 2	111	0.0625	2.01	0.905	2.100
U-NII-6	802.11ax160	Bottom Face	9.12	WIFI 2	111	0.0625	1.67	0.805	1.670
U-NII-6	802.11ax160	Bottom Face	2	WIFI 1	111	0.0625	2.59	0 700	2.720
U-NII-6	802.11ax160	Bottom Face	9.31	WIFI 1	111	0.0625	2.16	0.700	2.165
U-NII-6	802.11ax160	Bottom Face	2	MIMO	111	0.0625	3.01	0 727	3.280
U-NII-6	802.11ax160	Bottom Face	8.94	MIMO	111	0.0625	2.54	0.737	2.842

Diet			Evenentre		Ave.	Tune-up	Tune-up	psPDtot+	over 4cm <sup>2</sup>		
Piol	Band	Mode	Exposure	Ch.	Power	Limit	Scaling	(W/	′m²)		
INO.			Position		(dBm)	(dBm)	Factor	Mea.	Scaled		
			WIF	I 2 (Chain )	A)						
	U-NII-5	802.11ax160	Bottom Face	79	13.89	15.00	1.291	2.720	5.509		
	U-NII-5	802.11ax160	Edge 1	79	13.89	15.00	1.291	0.960	1.944		
	U-NII-5	802.11ax160	Bottom Face	15	13.87	15.00	1.297	0.620	1.262		
			WIF	I 1 (Chain	B)						
	U-NII-5	802.11ax160	Bottom Face	15	13.72	14.50	1.197	2.420	4.543		
	U-NII-5	802.11ax160	Edge 1	15	13.72	14.50	1.197	0.762	1.430		
	U-NII-5	802.11ax160	Bottom Face	79	13.35	14.00	1.161	3.020	5.502		
				MIMO							
11#	U-NII-5	802.11ax160	Bottom Face	79	13.29	14.00	1.178	3.380	6.237		
	U-NII-5	802.11ax160	Edge 1	79	13.29	14.00	1.178	0.762	1.406		
	U-NII-5	802.11ax160	Bottom Face	15	13.23	14.00	1.194	1.160	2.170		
			WIF	I 2 (Chain	A)						
	U-NII-6	802.11ax160	Bottom Face	111	13.48	14.50	1.265	2.100	4.166		
	U-NII-6	802.11ax160	Edge 1	111	13.48	14.50	1.265	0.701	1.391		
	WIFI 1 (Chain B)										



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	U-NII-6	802.11ax160	Bottom Face	111	13.08	14.00	1.236	2.720	5.273
	U-NII-6	802.11ax160	Edge 1	111	13.08	14.00	1.236	0.116	0.225
			·	MIMO					
12#	U-NII-6	802.11ax160	Bottom Face	111	13.50	14.50	1.259	3.280	6.471
	U-NII-6	802.11ax160	Edge 1	111	13.50	14.50	1.259	0.123	0.243
WIFI 2 (Chain A)									
	U-NII-7	802.11ax160	Bottom Face	143	13.25	14.00	1.189	1.360	2.535
	U-NII-7	802.11ax160	Edge 1	143	13.25	14.00	1.189	1.720	3.207
			WIF	I 1 (Chain	B)				
	U-NII-7	802.11ax160	Bottom Face	143	13.1	14.00	1.230	2.560	4.940
	U-NII-7	802.11ax160	Edge 1	143	13.1	14.00	1.230	1.600	3.088
				MIMO					
13#	U-NII-7	802.11ax160	Bottom Face	143	13.50	14.50	1.259	2.900	5.721
	U-NII-7	802.11ax160	Edge 1	143	13.50	14.50	1.259	0.461	0.909
			WIF	I 2 (Chain	A)				
	U-NII-8	802.11ax160	Bottom Face	207	13.79	14.50	1.178	2.680	4.950
	U-NII-8	802.11ax160	Edge 1	207	13.79	14.50	1.178	0.827	1.528
			WIF	I 1 (Chain	В)				
	U-NII-8	802.11ax160	Bottom Face	207	12.34	13.50	1.306	2.720	5.573
	U-NII-8	802.11ax160	Edge 1	207	12.34	13.50	1.306	0.671	1.375
				MIMO					
14#	U-NII-8	802.11ax160	Bottom Face	207	13.32	14.00	1.169	3.300	6.048
	U-NII-8	802.11ax160	Edge 1	207	13.32	14.00	1,169	0.594	1.089

**Note:** The WLAN 6GHz 802.11ax-HEW160 Reported 1g SAR (W/kg) should be scaled with the duty cycle scaling factor 1.012 for SISO, 1.011 for MIMO.



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## **16 Simultaneous Transmission Analysis**

### **16.1 Simultaneous Transmission Consideration**

		Exposure Position
NO.	Simultaneous Transmission Consideration	Body
1	WLAN 6GHz (SISO/MIMO) + Bluetooth	Yes

#### Note:

- 1. Simultaneous Transmission SAR evaluation is not required for BT and WLAN, because the software mechanism have been incorporated to guarantee that the WLAN and Bluetooth transmitters would not simultaneously operate at the same time.
- 2. Per KDB 447498D01v06, simultaneous transmission SAR evaluation procedures is as followed:

Step 1: If sum of 1 g SAR <1.6 W/kg, Simultaneous SAR measurement is not required. Step 2: If sum of 1 g SAR >1.6 W/kg, ratio of SAR to peak separation distance for pair of transmitters calculated.

Step 3: If the ratio of SAR to peak separation distance is  $\leq 0.04$ , Simultaneous SAR measurement is not required.

Step 4: If the ratio of SAR to peak separation distance is >0.04, Simultaneous SAR measurement is required and simultaneous transmission SAR value is calculated.

(The ratio is determined by:  $(SAR_1 + SAR_2) \wedge 1.5/Ri \le 0.04$ ,

R<sub>i</sub> is the separation distance between the peak SAR locations for the antenna pair in mm.







### **16.2 Total Exposure Radio Analysis**

The fields generated by the antennas can be correlated or uncorrelated. At different frequencies, fields are always uncorrelated, and the aggregate power density contributions can be summed according to spatially averaged values of corresponding sources at any point in space, r, to determine the total exposure ratio (TER). Assuming I sources, the TER at each point in space is equal to

$$\text{TER}^{\text{uncorr}}(r) = \sum_{i=1}^{I} \text{ER}_{i} = \sum_{i=1}^{I} \frac{S_{\text{av},i}(r,f_{i})}{S_{\text{lim}}(f_{i})}$$

Where S<sub>av</sub>, i is the power density for the source I operating at a frequency fi and Slim is the power density limit as specified by the relevant standard.

Exposure from transmitters operating above and below 6GHz, where 6GHz denotes the transmission frequency where the basic restrictions change from being defined in terms of SAR to being defined in terms of power density, therefore uncorrelated and the TER is determined as

$$\text{TER}^{\text{uncorr}}(\mathbf{r}) = \sum_{i=1}^{I} \text{ER}_{i} = \sum_{i=1}^{I} \frac{S_{\text{av},i}(\mathbf{r}, \mathbf{f}_{i})}{S_{\text{lim}}(\mathbf{f}_{i})}$$

According to the FCC guidance in TCBC workshop and IEC TR 63170, the total exposure ratio calculated by taking ratio of maximum reported SAR divided by SAR limit and adding it to maximum measured power density by its limit. Numerical sum of the ratios should be less 1. Therefore the simultaneous transmission should be follows:

$$TER = \sum_{n=1}^{N} \frac{SAR_n}{SAR_{n,limit}} + \sum_{n=1}^{N} \frac{S_{m,avg}}{S_{m,limit}} < 1$$

For transmitters operating above 6000 MHz, it is necessary to perform an assessment against the PD (basic restriction up to 10 GHz and reference levels beyond). The exposure ratio for the -th transmitter is given by:

$$max\left[\frac{SAR_m}{SAR_{limit}}, \frac{APD_m}{APD_{limit}}\right]$$

5925 MHz 
$$< f_m \le 10 \; GHz$$

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#### Where:

- *SARm* is the SAR value for the *n*-th transmitter/test frequency.
- *SARlimit* is the basic restriction limit that is applicable to the *n*-th transmitter/test frequency.
- $APD_m$  is the APD value for the *m*-th transmitter/test frequency.
- *APDlimit* is the basic restriction limit that is applicable for the *m*-th transmitter/test frequency.

### **16.3 Simultaneous Transmission Analysis**

#### > SAR Simultaneous Transmission Evaluation

	1	2	1+2
Exposure	Max. Reported SAR (W/kg)	Max. Reported SAR (W/kg)	1g SAR
1 Osition	Wi-Fi 6E	Bluetooth (Chain A)	(W/kg)
Body	0.907	0.086	0.993

#### > Total Exposure Ratio

Exposure Position		Max. Power Density (mW/cm2)	Max. Reported SAR (W/kg)	Total Exposure
		Wi-Fi 6E	Bluetooth(Chain A)	Ralio
Body	Reported Exposure	0.647	0.086	0.701
	Ratio to Limit	1.0	1.6	

Note: The simultaneous transmission analysis of PD results is based on the final PD value.



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## **17 Measurement Uncertainty**

The component of uncertainly may generally be categorized according to the methods used to evaluate them. The evaluation of uncertainly by the statistical analysis of a series of observations is termed a Type A evaluation of uncertainty. The evaluation of uncertainty by means other than the statistical analysis of a series of observation is termed a Type B evaluation of uncertainty. Each component of uncertainty, however evaluated, is represented by an estimated standard deviation, termed standard uncertainty, which is determined by the positive square root of the estimated variance.

A Type A evaluation of standard uncertainty may be based on any valid statistical method for treating data. This includes calculating the standard deviation of the mean of a series of independent observations; using the method of least squares to fit a curve to the data in order to estimate the parameter of the curve and their standard deviations; or carrying out an analysis of variance in order to identify and quantify random effects in certain kinds of measurement.

A Type B evaluation of standard uncertainty is typically based on scientific judgment using all of the relevant information available. These may include previous measurement data, experience, and knowledge of the behavior and properties of relevant materials and instruments, manufacture's specification, data provided in calibration reports and uncertainties assigned to reference data taken from handbooks. Broadly speaking, the uncertainty is either obtained from an outdoor source or obtained from an assumed distribution, such as the normal distribution, rectangular or triangular distributions indicated in below Table.

Uncertainty Distributions	Normal	Rectangular	Triangular	U-Shape
Multi-plying Factor	1/k(b)	1/√3	1/√6	1/√2

### Standard Uncertainty for Assumed Distribution

The combined standard uncertainty of the measurement result represents the estimated standard deviation of the result. It is obtained by combining the individual standard uncertainties of both Type A and Type B evaluation using the usual "root-sum-squares" (RSS) methods of combining standard deviations by taking the positive square root of the estimated variances.

Expanded uncertainty is a measure of uncertainty that defines an interval about the measurement result within which the measured value is confidently believed to lie. It is obtained by multiplying the combined standard uncertainty by a coverage factor. Typically, the coverage factor ranges from 2 to 3. Using a coverage factor allows the true value of a measured quantity to be specified with a defined probability within the specified uncertainty range. For purpose of this document, a coverage



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factor two is used, which corresponds to confidence interval of about 95 %. The DASY uncertainty Budget is shown in the following tables.

	DASY6/8 Uncertainty Budget												
(Frequency Range: 300MHz ~ 3GHz)													
Symbol	Error Description	Uncert. Value (±%)	Prob.	Div.	Ci	Ci	Standard Uncertainty (1g) (土%)	Standard Uncertainty (10g) (±%)					
Measurement System Erros													
CF	Probe calibration	12.0	N	2	1	1	6.0	6.0					
CFdrift	Probe calibration Drift	1.7	R	$\sqrt{3}$	1	1	1.0	1.0					
LIN	Probe Linearity	4.7	R	$\sqrt{3}$	1	1	2.7	2.7					
BBS	Broadband Signal	3.0	R	$\sqrt{3}$	1	1	1.7	1.7					
ISO	Probe Isotropy	7.6	R	$\sqrt{3}$	1	1	4.4	4.4					
DAE	Other Probe+Electronic	0.7	N	1	1	1	0.7	0.7					
AMB	RF Ambient	1.8	N	1	1	1	1.8	1.8					
<b>▲</b> sys	Probe positioning	0.006mm	N	1	0.14	0.14	0.1	0.1					
DAT	Data Processing	1.2	N	1	1	1	1.2	1.2					
Phantom and Device Errors													
LIQ(σ)	Conductivity (meas.) DAK	2.5	N	1	0.78	0.71	2.0	1.8					
LIQ(T <sub>σ</sub> )	Conductivity (temp.) BB	3.3	R	$\sqrt{3}$	0.78	0.71	1.5	1.4					
EPS	Phantom Permittivity	14.0	R	$\sqrt{3}$	0	0	0	0					
DIS	Distance DUT - TSL	2.0	N	1	2	2	4.0	4.0					
Dxyz	Device Positioning	1.0	N	1	1	1	1.0	1.0					
н	Device Holder	3.6	N	1	1	1	3.6	3.6					
MOD	DUT Modulation <sup>m</sup>	2.4	R	$\sqrt{3}$	1	1	1.4	1.4					
TAS	Time-average SAR	1.7	R	$\sqrt{3}$	1	1	1.0	1.0					
RFdrift	DUT Drift	2.5	N	1	1	1	2.5	2.5					
VAL	Val Antenna Unc. <sup>val</sup>	0.0	N	1	1	1	0.0	0.0					
RFin	Unc. Input Power <sup>val</sup>	0.0	N	1	1	1	0.0	0.0					
		Correc	tion to the	SAR Re	esults								
C(ε,σ)	Deviation to Target	1.9	N	1	1	0.84	1.9	1.6					
C(R)	SAR Scaling <sup>p</sup>	0.0	R	$\sqrt{3}$	1	1	0.0	0.0					
u( <b>▲</b> SAR)	Comb	oined Standa	ard Uncer	tainty			10.9	10.9					
U	Expa	nded Standa	ard Uncer	tainty			21.9	21.8					



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DASY6/8 Uncertainty Budget								
(Frequency Range: 3GHz ~ 6GHz)								
Symbol	Error Description	Uncert. Value (±%)	Prob.	Div.	Ci	Ci	Standard Uncertainty (1g) (±%)	Standard Uncertainty (10g) (±%)
Measurement System Erros								
CF	Probe calibration	13.1	Ν	2	1	1	6.55	6.55
CFdrift	Probe calibration Drift	1.7	R	$\sqrt{3}$	1	1	1.0	1.0
LIN	Probe Linearity	4.7	R	$\sqrt{3}$	1	1	2.7	2.7
BBS	Broadband Signal	2.6	R	$\sqrt{3}$	1	1	1.5	1.5
ISO	Probe Isotropy	7.6	R	$\sqrt{3}$	1	1	4.4	4.4
DAE	Other Probe+Electronic	1.2	Ν	1	1	1	1.2	1.2
AMB	RF Ambient	1.8	Ν	1	1	1	1.8	1.8
<b>▲</b> sys	Probe positioning	0.005mm	Ν	1	0.29	0.29	0.15	0.15
DAT	Data Processing	2.3	Ν	1	1	1	2.3	2.3
Phantom and Device Errors								
LIQ(σ)	Conductivity (meas.) DAK	2.5	N	1	0.78	0.71	2.0	1.8
LIQ(T <sub>σ</sub> )	Conductivity (temp.) BB	3.4	R	$\sqrt{3}$	0.78	0.71	1.5	1.4
EPS	Phantom Permittivity	14.0	R	$\sqrt{3}$	0.25	0.25	2.0	2.0
DIS	Distance DUT - TSL	2.0	Ν	1	2	2	4.0	4.0
Dxyz	Device Positioning	1.0	N	1	1	1	1.0	1.0
н	Device Holder	3.6	N	1	1	1	3.6	3.6
MOD	DUT Modulation <sup>m</sup>	2.4	R	$\sqrt{3}$	1	1	1.4	1.4
TAS	Time-average SAR	1.7	R	$\sqrt{3}$	1	1	1.0	1.0
RFdrift	DUT Drift	2.5	Ν	1	1	1	2.5	2.5
VAL	Val Antenna Unc. <sup>val</sup>	0.0	Ν	1	1	1	0.0	0.0
RFin	Unc. Input Power <sup>val</sup>	0.0	Ν	1	1	1	0.0	0.0
	Correction to the SAR Results							
C(ε,σ)	Deviation to Target	1.9	Ν	1	1	0.84	1.9	1.6
C(R)	SAR Scaling <sup>p</sup>	0.0	R	$\sqrt{3}$	1	1	0.0	0.0
u( <b>▲</b> SAR)	Comb	pined Standa	ard Uncer	tainty			11.6	11.5
U	Expanded Standard Uncertainty23.323.0						23.0	



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DASY6/8 Uncertainty Budget								
(Frequency Range: 6GHz ~ 10GHz)								
Symbol	Error Description	Uncert. Value (±%)	Prob.	Div.	Ci	Ci	Standard Uncertainty (1g) (±%)	Standard Uncertainty (10g) (±%)
Measurement System Erros								
CF	Probe calibration	18.6	Ν	2	1	1	9.3	9.3
CFdrift	Probe calibration Drift	1.7	R	$\sqrt{3}$	1	1	1.0	1.0
LIN	Probe Linearity	4.7	R	$\sqrt{3}$	1	1	2.7	2.7
BBS	Broadband Signal	2.8	R	$\sqrt{3}$	1	1	1.6	1.6
ISO	Probe Isotropy	7.6	R	$\sqrt{3}$	1	1	4.4	4.4
DAE	Other Probe+Electronic	1.2	N	1	1	1	2.4	2.4
AMB	RF Ambient	1.8	N	1	1	1	1.8	1.8
<b>▲</b> sys	Probe positioning	0.005mm	N	1	0.50	0.50	0.25	0.25
DAT	Data Processing	3.5	Ν	1	1	1	3.5	3.5
Phantom and Device Errors								
LIQ(σ)	Conductivity (meas.) DAK	2.5	N	1	0.78	0.71	2.0	1.8
LIQ(T <sub>σ</sub> )	Conductivity (temp.) BB	2.4	R	$\sqrt{3}$	0.78	0.71	1.1	1.0
EPS	Phantom Permittivity	14.0	R	$\sqrt{3}$	0.5	0.5	4.0	4.0
DIS	Distance DUT - TSL	2.0	N	1	2	2	4.0	4.0
Dxyz	Device Positioning	1.0	N	1	1	1	1.0	1.0
н	Device Holder	3.6	N	1	1	1	3.6	3.6
MOD	DUT Modulation <sup>m</sup>	2.4	R	$\sqrt{3}$	1	1	1.4	1.4
TAS	Time-average SAR	1.7	R	$\sqrt{3}$	1	1	1.0	1.0
RFdrift	DUT Drift	2.5	N	1	1	1	2.5	2.5
VAL	Val Antenna Unc. <sup>val</sup>	0.0	N	1	1	1	0.0	0.0
RFin	Unc. Input Power <sup>val</sup>	0.0	N	1	1	1	0.0	0.0
	Correction to the SAR Results							
C(ε,σ)	Deviation to Target	1.9	Ν	1	1	0.84	1.9	1.6
C(R)	SAR Scaling <sup>p</sup>	0.0	R	$\sqrt{3}$	1	1	0.0	0.0
u( <b>▲</b> SAR)	Comb	pined Standa	ard Uncer	tainty			14.2	13.9
U	Expanded Standard Uncertainty 28.4 27.9							



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	DASY6/8 Uncertainty Budget for psSAR / psAPD Assessment							
	(Frequency Range: 6GHz ~ 10GHz)							
Symbol	Error Description	Uncert. Value (±%)	Prob.	Div.	Ci	Ci	Standard Uncertainty (1g) (±%)	Standard Uncertainty (10g) (±%)
psSAR	Module SAR V16.0 (Table 6.3.3)	14.2/13.9	N	1	1	1	14.2	13.9
PDC	Power Density Conversion	13.5	R	$\sqrt{3}$	1	1	7.8	7.8
u( <b>▲</b> SAR)	I(▲SAR) Combined Standard Uncertainty 16.2 15.9					15.9		
				tuin dP			32.4	31.9
U	Expanded Standard Uncertainty in dB						$\pm$ 1.2dB	$\pm$ 1.2dB

Error Description	Uncertainty (±dB)	Probability Distribution	Divisor	ci	Standard Uncertainty (±dB)	ν <sub>i</sub> <b>or</b> ν <sub>eff</sub>		
Uncertai	Uncertainty terms dependent on the measurement system							
Probe calibration	0.49	N	1	1	0.49	8		
Probe correction	0	R	1.732	1	0	8		
Frequency response	0.20	R	1.732	1	0.12	8		
Sensor cross coupling	0	R	1.732	1	0	8		
Isotropy	0.50	R	1.732	1	0.29	8		
Linearity	0.20	R	1.732	1	0.12	$\infty$		
Probe scattering	0	R	1.732	1	0	8		
Probe positioning offset	0.30	R	1.732	1	0.17	8		
Probe positioning repeatability	0.04	R	1.732	1	0.02	8		
Sensor mechanical offset	0	R	1.732	1	0	8		
Probe spatial resolution	0	R	1.732	1	0	8		
Field impedance dependance	0	R	1.732	1	0	8		
Amplitude and phase drift	0	R	1.732	1	0	8		
Amplitude and phase noise	0.04	R	1.732	1	0.02	8		
Measurement area truncation	0	R	1.732	1	0	8		
Data acquisition	0.03	R	1.732	1	0.03	8		
Sampling	0	R	1.732	1	0	8		
Field reconstruction	2.0	R	1.732	1	1.15	8		
Forward transformation	0	R	1.732	1	0	8		
Power density scaling	-	R	1.732	1	-	8		
Spatial averaging	0.10	R	1.732	1	0.06	8		
System Detection Limits	0.04	R	1.732	1	0.02	8		
Uncertainty te	erms dependen	t on the DUT a	and enviro	nmental f	actors			
Probe coupling with DUT	0	R	1.732	1	0	8		



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Modulation response	0.40	R	1.732	1	0.23	œ
Integration time	0	R	1.732	1	0	œ
Response time	0	R	1.732	1	0	8
Device holder influence	0.10	R	1.732	1	0.06	8
DUT alignment	0	R	1.732	1	0	8
RF ambient	0.04	R	1.732	1	0.02	8
Ambient reflections	0.04	R	1.732	1	0.02	8
Immunity / secondary reception	0	R	1.732	1	0	8
Drift of the DUT	-	R	1.732	1	-	8
Combined standard uncertainty 1.34 dB						8
Cov		K=2	NI/A			
Expanded standard uncertainty 2.68 dB						

PD Uncertainty Budget for Frequency Range 6 – 10GHz



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## **18 Measurement Conclusion**

The SAR evaluation indicates that the EUT complies with the RF radiation exposure limits of FCC, with respect to all parameters subject to this test. These measurements were taken to simulate the RF effects of RF exposure under worst-case conditions. Precise laboratory measures were taken to assure repeatability of the tests. The results and statements relate only to the item(s) tested. Please note that the absorption and distribution of electromagnetic energy in the body are very complex phenomena that depend on the mass, shape, and size of the body, the orientation of the body with respect to the field vectors, and the electrical properties of both the body and the environment. Other variables that may play a substantial role in possible biological effects are those that characterize the environment (e.g. ambient temperature, air velocity, relative humidity, and body insulation) and those that characterize the individual (e.g. age, gender, activity level, debilitation, or disease). Because various factors may interact with one another to vary the specific biological outcome of an exposure to electromagnetic fields, any protection guide should consider maximal amplification of biological effects as a result of field-body interactions, environmental conditions, and physiological variables.



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## **Annex A General Information**

### 1. Identification of the Responsible Testing Laboratory

Laboratory Name:	Shenzhen Morlab Communications Technology Co., Ltd.			
Laboratory Address:	FL.1-3, Building A, FeiYang Science Park, No.8			
	LongChang Road, Block 67, BaoAn District, ShenZhen,			
	GuangDong Province, P. R. China			
Telephone:	+86 755 36698555			
Facsimile:	+86 755 36698525			

#### 2. Identification of the Responsible Testing Location

Name:	Shenzhen Morlab Communications Technology Co., Ltd.
Address:	FL.1-3, Building A, FeiYang Science Park, No.8
	LongChang Road, Block 67, BaoAn District, ShenZhen,
	GuangDong Province, P. R. China

#### 3. Facilities and Accreditations

The FCC designation number is CN1192, the test firm registration number is 226174.

#### Note:

The main report is end here and the other Annex (B,C,D,E,F,G) will be submitted separately.

#### \*\*\*\*\*\* END OF MAIN REPORT \*\*\*\*\*\*



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