

SAR EVALUATION REPORT

For

Kirisun Electronics (Shenzhen) Co., Ltd.

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Chinese Town, Nanshan Dist.
Shenzhen, 518053, China

FCC ID: Q5EPT320802

2003-06-26

This Report Concerns: ☒ Original Report	Equipment Type: FM Handheld Transceiver
Test Engineer: Eric Hong	
Report No.: R0304284S	
Test Date: 2003-06-21	
Reviewed By: Ling Zhang	
Prepared By:	Bay Area Compliance Laboratory Corporation 230 Commercial Street Sunnyvale, CA 94085 Tel: (408) 732-9162 Fax: (408) 732 9164

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SUMMARY

The US Federal Communications Commission has released the report and order “Guidelines for Evaluating the Environmental Effects of RF Radiation”, ET Docket No. 93-62 in August 1996 [1].

The order requires routine SAR evaluation prior to equipment authorization of portable transmitter devices, including portable telephones. For consumer products, the applicable limit is 1.6 mW/g as recommended by the ANSI/IEEE standard C95.1-1992 [6] for an uncontrolled environment (Paragraph 65). According to the Supplement C of OET Bulletin 65 “Evaluating Compliance with FCC Guide-lines for Human Exposure to Radio frequency Electromagnetic Fields”, released on Jun 29, 2001 by the FCC, the device should be evaluated at maximum output power (radiated from the antenna) under “worst-case” conditions for normal or intended use, incorporating normal antenna operating positions, device peak performance frequencies and positions for maximum RF energy coupling.

This report describes the methodology and results of experiments performed on wireless data terminal. The objective was to determine if there is RF radiation and if radiation is found, what is the extent of radiation with respect to safety limits. SAR (Specific Absorption Rate) is the measure of RF exposure determined by the amount of RF energy absorbed by human body (or its parts) – to determine how the RF energy couples to the body or head which is a primary health concern for body worn devices. The limit below which the exposure to RF is considered safe by regulatory bodies in North America is 1.6 mW/g average over 1 gram of tissue mass.

The test configurations were laid out on a specially designed test fixture to ensure the reproducibility of measurements. Each configuration was scanned for SAR. Analysis of each scan was carried out to characterize the above effects in the device.

The investigation was limited to the worst-case scenario from the device usage point of view. For the clarity of data analysis, and clarity of presentation, only one tissue simulation was used for the head and body simulation. This means that if SAR was found at the headset position, the magnitude of SAR would be overestimated comparing to SAR to a headset placed in the ear region.

There was no SAR of any concern measured on the device for any of the investigated configurations, please see following table for testing result summary:

Ambient Temperature (°C): 23.0

Relative Humidity (%): 51.1

Worst case SAR reading

EUT position	Frequency (MHz)	Conducted Power (W)	Test Type	Antenna Type	Liquid	Phantom	Notes / Accessories	Measured (mW/g)		Limit (mW/g)	Plot #
								100% duty cycle	50% duty cycle		
back in touch with phantom	450	3.83	Body worn	Built-in	body	flat	headset	8.43	4.215	8	1
back in touch with phantom	460	4.14	Body worn	Built-in	body	flat	headset	9.78	4.89	8	2
back in touch with phantom	470	4.14	Body worn	Built-in	body	flat	headset	9.54	4.77	8	3
2.5 cm head separation to phantom	450	3.83	Face-held	Built-in	head	flat	none	8.21	4.11	8	4
2.5 cm head separation to phantom	460	4.14	Face-held	Built-in	head	flat	none	8.52	4.26	8	5
2.5 cm head separation to phantom	470	4.14	Face-held	Built-in	head	flat	none	6.56	3.28	8	6

1 - REFERENCE

- [1] Federal Communications Commission, \Report and order: Guidelines for evaluating the environmental effects of radiofrequency radiation", Tech. Rep. FCC 96-326, FCC, Washington, D.C. 20554, 1996.
- [2] David L. Means Kwok Chan, Robert F. Cleveland, \Evaluating compliance with FCC guidelines for human exposure to radiofrequency electromagnetic fields", Tech. Rep., Federal Communication Commission, Office of Engineering & Technology, Washington, DC, 1997.
- [3] Thomas Schmid, Oliver Egger, and Niels Kuster, \Automated E-field scanning system for dosimetric assessments", IEEE Transactions on Microwave Theory and Techniques, vol. 44, pp. 105{113, Jan. 1996.
- [4] Niels Kuster, Ralph Kastle, and Thomas Schmid, \Dosimetric evaluation of mobile communications equipment with known precision", IEICE Transactions on Communications, vol. E80-B, no. 5, pp. 645{652, May 1997.
- [5] CENELEC, \Considerations for evaluating of human exposure to electromagnetic fields (EMFs) from mobile telecommunication equipment (MTE) in the frequency range 30MHz - 6GHz", Tech. Rep., CENELEC, European Committee for Electrotechnical Standardization, Brussels, 1997.
- [6] ANSI, ANSI/IEEE C95.1-1992: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz, The Institute of Electrical and Electronics Engineers, Inc., New York, NY 10017, 1992.
- [7] Katja Pokovic, Thomas Schmid, and Niels Kuster, \Robust setup for precise calibration of E-field probes in tissue simulating liquids at mobile communications frequencies", in ICECOM _ 97, Dubrovnik, October 15{17, 1997, pp. 120-24.
- [8] Katja Pokovic, Thomas Schmid, and Niels Kuster, \E-field probe with improved isotropy in brain simulating liquids", in Proceedings of the ELMAR, Zadar, Croatia, 23{25 June, 1996, pp. 172-175.
- [9] Volker Hombach, Klaus Meier, Michael Burkhardt, Eberhard Kuhn, and Niels Kuster, \The dependence of EM energy absorption upon human head modeling at 900 MHz", IEEE Transactions on Microwave Theory and Techniques, vol. 44, no. 10, pp. 1865-1873, Oct. 1996.
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- [12] W. H. Press, S. A. Teukolsky, W. T. Vetterling, and B. P. Flannery, Numerical Recipes in C, The Art of Scientific Computing, Second Edition, Cambridge University Press, 1992. Dosimetric Evaluation of Sample device, month 1998 9
- [13] NIS81 NAMAS, \The treatment of uncertainty in EMC measurement", Tech. Rep., NAMAS Executive, National Physical Laboratory, Teddington, Middlesex, England, 1994.
- [14] Barry N. Taylor and Christ E. Kuyatt, \Guidelines for evaluating and expressing the uncertainty of NIST measurement results", Tech. Rep., National Institute of Standards and Technology, 1994. Dosimetric Evaluation of Sample device, month 1998 10

2 - TESTING EQUIPMENT

2.1 Equipment List & Calibration Info

Type / Model	Cal. Date	S/N:
DASY3 Professional Dosimetric System	N/A	N/A
Robot RX60L	N/A	F00/5H31A1/A/01
Robot Controller	N/A	F01/5J72A1/A/01
Dell Computer Optiplex GX110	N/A	N/A
Pentium III, Windows NT	N/A	N/A
SPEAG EDC3	N/A	N/A
SPEAG DAE3	6/02	456
SPEAG E-Field Probe ET3DV6	9/7/02	1604
SPEAG Dummy Probe	N/A	N/A
SPEAG Generic Twin Phantom	N/A	N/A
SPEAG Light Alignment Sensor	N/A	278
Apprel Validation Dipole D-1800-S-2	11/6/01	BCL-049
SPEAG Validation Dipole D900V2	9/3/02	122
Brain Equivalent Matter (800MHz)	Daily	N/A
Brain Equivalent Matter (1900MHz)	Daily	N/A
Brain Equivalent Matter (2450MHz)	Daily	N/A
Muscle Equivalent Matter (800MHz)	Daily	N/A
Muscle Equivalent Matter (1900MHz)	Daily	N/A
Muscle Equivalent Matter (2450MHz)	Daily	N/A
Robot Table	N/A	N/A
Phone Holder	N/A	N/A
Phantom Cover	N/A	N/A
HP Spectrum Analyzer HP8593GM	6/20/02	3009A00791
Microwave Amp. 8349B	N/A	2644A02662
Power Meter HP436A	4/2/02	2709A29209
Power Sensor HP8482A	4/2/02	2349A08568
Signal Generator RS SMIQ O3	2/10/02	1084800403
Network Analyzer HP-8753ES	7/30/02	820079
Dielectric Probe Kit HP85070A	N/A	N/A
Apprel Validation Dipole D-2450-S-1	10/1/02	BCL-141
Dipole Antenna AD-100 (450MHz)	5/7/02	02220

2.2 Equipment Calibration Certificate

Please see the attached file.

**Calibration Laboratory of
Schmid & Partner
Engineering AG**
Zeughausstrasse 43, 8004 Zurich, Switzerland

Client Bay Area Compliance Lab.

CALIBRATION CERTIFICATE

Object(s) D450V2 - SN:1010

Calibration procedure(s) QA CAL-15.v1
Calibration procedure for dipole validation kits below 800 MHz

Calibration date: January 24, 2003

Condition of the calibrated item In Tolerance (according to the specific calibration document)

This calibration statement documents traceability of M&TE used in the calibration procedures and conformity of the procedures with the ISO/IEC 17025 international standard.

All calibrations have been conducted in the closed laboratory facility: environment temperature 22 +/- 2 degrees Celsius and humidity < 75%.

Calibration Equipment used (M&TE critical for calibration)

Model Type	ID #	Cal Date	Scheduled Calibration
RF generator HP 8684C	US3642U01700	4-Aug-99 (in house check Aug-02)	In house check: Aug-05
Power sensor E4412A	MY41495277	8-Mar-02	Mar-03
Power sensor HP 8481A	MY41092180	18-Sep-02	Sep-03
Power meter EPM E4419B	GB41293874	13-Sep-02	Sep-03
Network Analyzer HP 8753E	US38432426	3-May-00	In house check: May 03
Fluke Process Calibrator Type 702	SN: 6295803	3-Sep-01	Sep-03

	Name	Function	Signature
Calibrated by:	Katja Pokovic	Laboratory Director	
Approved by:	Niels Kuster	Quality Manager	

Date issued: January 24, 2003

This calibration certificate is issued as an intermediate solution until the accreditation process (based on ISO/IEC 17025 International Standard) for Calibration Laboratory of Schmid & Partner Engineering AG is completed.

Schmid & Partner Engineering AG

Zeughausstrasse 43, 8004 Zurich, Switzerland, Phone +41 1 245 97 00, Fax +41 1 245 97 79

DASY

Dipole Validation Kit

Type: D450V2

Serial: 1010

Manufactured: November 18, 2002
Calibrated: January 24, 2003

1. Measurement Conditions

The measurements were performed in the 6mm thick flat phantom filled with head simulating liquid of the following electrical parameters at 450 MHz:

Relative Dielectricity	45.3	± 5%
Conductivity	0.87 mho/m	± 5%

The DASY3 System (Software version 3.1d) with a dosimetric E-field probe ET3DV6 (SN:1507, Conversion factor 7.2 at 450 MHz) was used for the measurements.

The dipole was mounted on the small tripod so that the dipole feedpoint was positioned below the center of the flat phantom and the dipole was oriented parallel to the longer side of the phantom. The standard measuring distance was 15mm from dipole center to the liquid surface including the 6mm thick phantom shell. The included distance holder was used during measurements for accurate distance positioning.

The coarse grid with a grid spacing of 20mm was aligned with the dipole. The 5x5x7 fine cube was chosen for cube integration. Probe isotropy errors were cancelled by measuring the SAR with normal and 90° turned probe orientations and averaging.

The dipole input power (forward power) was 396 mW ± 3 %. The results are normalized to 1W input power.

2. SAR Measurement

Standard SAR-measurements were performed with the phantom according to the measurement conditions described in section 1. The results have been normalized to a dipole input power of 1W (forward power). The resulting averaged SAR-values are:

averaged over 1 cm ³ (1 g) of tissue:	5.03 mW/g (Advanced Extrapolation)
averaged over 10 cm ³ (10 g) of tissue	3.31 mW/g (Advanced Extrapolation)

Advanced extrapolation has been applied to the measured SAR values to compensate for the probe boundary effect (see DASY User Manual for details).

Note: If the liquid parameters for validation are slightly different from the ones used for initial calibration, the SAR-values will be different as well.

3. Dipole Impedance and Return Loss

The impedance was measured at the SMA-connector with a network analyzer and numerically transformed to the dipole feedpoint. The transformation parameters from the SMA-connector to the dipole feedpoint are:

Electrical delay:	1.438 ns	(one direction)
Transmission factor	0.996	(voltage transmission, one direction)

The dipole was positioned at the flat phantom sections according to section 1 and the distance holder was in place during impedance measurements.

Feedpoint impedance at 450 MHz	$\text{Re}\{Z\} = 41.9 \Omega$
	$\text{Im}\{Z\} = -1.8 \Omega$
Return Loss at 450 MHz	-20.8 dB

4. Handling

Do not apply excessive force to the dipole arms, because they might bend. Bending of the dipole arms stresses the soldered connections near the feedpoint leading to a damage of the dipole.

5. Design

The dipole is made of standard semirigid coaxial cable. The center conductor of the feeding line is directly connected to the second arm of the dipole. The antenna is therefore short-circuited for DC-signals.

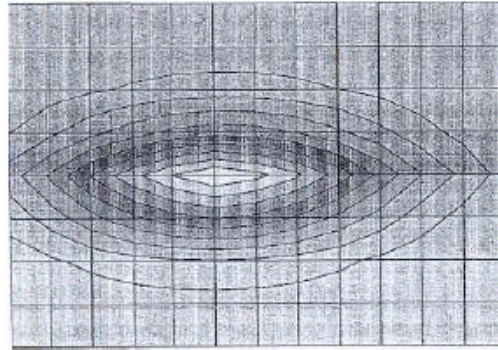
6. Power Test

After long term use with 100W radiated power, only a slight warming of the dipole near the feedpoint can be measured.

ation Dipole D450V2 SN:1010, d = 15 mm

cy: 450 MHz; Antenna Input Power: 396 [mW]

1 Name: Calibration (6mm shell thickness), Grid Spacing: Dx = 20.0, Dy = 20.0, Dz = 10.0

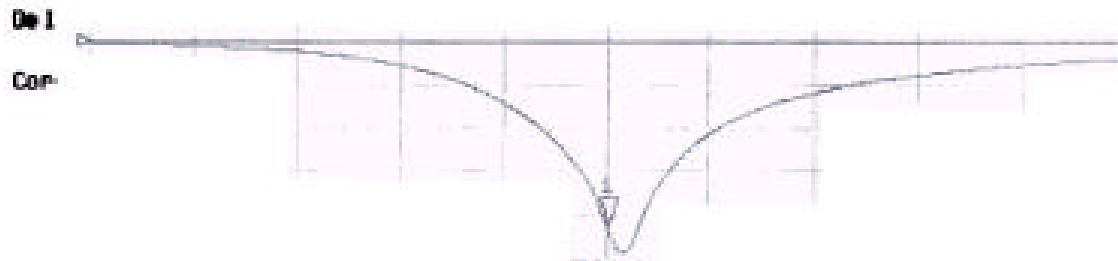
T3DV6 - SN1507; ConvF(7.20,7.20,7.20); Crest factor: 1.0; Head 450 MHz: $\sigma = 0.87$ mho/m $\epsilon_r = 45.3$ $\rho = 1.00$ g/cm³2): Peak: 3.07 mW/g ± 0.01 dB, SAR (1g): 1.99 mW/g ± 0.04 dB, SAR (10g): 1.31 mW/g ± 0.05 dB, (Advanced extrapolation)
ion depth: 12.7 (11.4, 14.3) [mm]SAR_{avg} [mW/g]

2.17E+0
.95E+0
1.74E+0
1.52E+0
1.30E+0
1.09E+0
8.68E-1
6.51E-1
4.34E-1
2.17E-1

& Partner Engineering AG, Zurich, Switzerland

CH1 S11 L08 5 dB/REF 0 dB

24 Jan 2003 14:41:45
11-20.047 dB 450.000 000 MHz

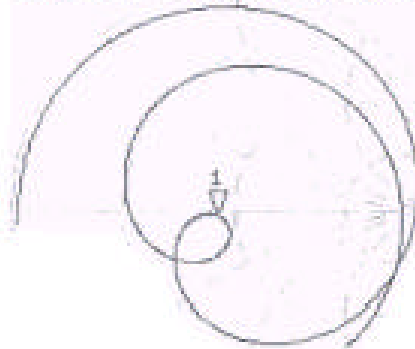


CH2 S11 1 U F8

B: 41.863 n -1.8185 n 195.34 pF

450.000 000 MHz

Cor



CENTER 450.000 000 MHz

SPAN 500.000 000 MHz

Schmid & Partner Engineering AG

Zeughausstrasse 43, 8004 Zurich, Switzerland, Phone +41 1 245 97 00, Fax +41 1 245 97 79

Calibration Certificate

Dosimetric E-Field Probe

Type:

ET3DV6

Serial Number:

1604

Place of Calibration:

Zurich

Date of Calibration:

August 26, 2002

Calibration Interval:

12 months

Schmid & Partner Engineering AG hereby certifies, that this device has been calibrated on the date indicated above. The calibration was performed in accordance with specifications and procedures of Schmid & Partner Engineering AG.

Wherever applicable, the standards used in the calibration process are traceable to international standards. In all other cases the standards of the Laboratory for EMF and Microwave Electronics at the Swiss Federal Institute of Technology (ETH) in Zurich, Switzerland have been applied.

Calibrated by:

D. Vetter

Approved by:

René Kaya

DASY3 - Parameters of Probe: ET3DV6 SN:1604

Sensitivity in Free Space

NormX	1.73 $\mu\text{V}/(\text{V/m})^2$
NormY	1.68 $\mu\text{V}/(\text{V/m})^2$
NormZ	1.72 $\mu\text{V}/(\text{V/m})^2$

Diode Compression

DCP X	93	mV
DCP Y	93	mV
DCP Z	93	mV

Sensitivity in Tissue Simulating Liquid

Head	900 MHz	$\epsilon_r = 41.5 \pm 5\%$	$\sigma = 0.97 \pm 5\% \text{ mho/m}$
Head	835 MHz	$\epsilon_r = 41.5 \pm 5\%$	$\sigma = 0.90 \pm 5\% \text{ mho/m}$
ConvF X	6.5 $\pm 9.5\%$ (k=2)		Boundary effect:
ConvF Y	6.5 $\pm 9.5\%$ (k=2)		Alpha 0.36
ConvF Z	6.5 $\pm 9.5\%$ (k=2)		Depth 2.82
Head	1800 MHz	$\epsilon_r = 40.0 \pm 5\%$	$\sigma = 1.40 \pm 5\% \text{ mho/m}$
Head	1900 MHz	$\epsilon_r = 40.0 \pm 5\%$	$\sigma = 1.40 \pm 5\% \text{ mho/m}$
ConvF X	5.5 $\pm 9.5\%$ (k=2)		Boundary effect:
ConvF Y	5.5 $\pm 9.5\%$ (k=2)		Alpha 0.50
ConvF Z	5.5 $\pm 9.5\%$ (k=2)		Depth 2.46

Boundary Effect

Head	900 MHz	Typical SAR gradient: 5 % per mm	
Probe Tip to Boundary		1 mm	2 mm
SAR _{be} [%]	Without Correction Algorithm	11.1	6.6
SAR _{be} [%]	With Correction Algorithm	0.4	0.6
Head	1800 MHz	Typical SAR gradient: 10 % per mm	
Probe Tip to Boundary		1 mm	2 mm
SAR _{be} [%]	Without Correction Algorithm	12.3	8.1
SAR _{be} [%]	With Correction Algorithm	0.1	0.1

Sensor Offset

Probe Tip to Sensor Center	2.7	mm
Optical Surface Detection	1.3 $\pm$ 0.2	mm

Engineering**Zeughausstrasse 43, 8004 Zurich, Switzerland, Phone +41 1 245 97 00, Fax +41 1 245 97 79**

Additional Conversion Factors

for Dosimetric E-Field Probe

Type

ET3DV6

Serial Number:

1604

Place of Assessment

Zurich

Date of Assessment:

October 4, 2002

Probe Calibration Date:

August 26, 2002

Schmid & Partner Engineering AG hereby certifies that conversion factor(s) of this probe have been evaluated on the date indicated above. The assessment was performed using the FDTD numerical code SEMCAD of Schmid & Partner Engineering AG. Since the evaluation is coupled with measured conversion factors, it has to be recalculated yearly, i.e., following the re-calibration schedule of the probe. The uncertainty of the numerical assessment is based on the extrapolation from measured value at 900 MHz or at 1800 MHz.

Assessed by:

Conversion Factor ($\pm$ standard deviation)**150 MHz ConvF $9.2 \pm 8\%$**
 $\epsilon_r = 52.3$
 $\sigma = 0.76 \text{ mho/m}$
 (head tissue)
300 MHz ConvF $8.0 \pm 8\%$
 $\epsilon_r = 45.3$
 $\sigma = 0.87 \text{ mho/m}$
 (head tissue)
450 MHz ConvF $7.3 \pm 8\%$
 $\epsilon_r = 43.5$
 $\sigma = 0.87 \text{ mho/m}$
 (head tissue)
2450 MHz ConvF $4.7 \pm 8\%$
 $\epsilon_r = 39.2$
 $\sigma = 1.80 \text{ mho/m}$
 (head tissue)
150 MHz ConvF $8.8 \pm 8\%$
 $\epsilon_r = 61.9$
 $\sigma = 0.80 \text{ mho/m}$
 (body tissue)
450 MHz ConvF $7.7 \pm 8\%$
 $\epsilon_r = 56.7$
 $\sigma = 0.94 \text{ mho/m}$
 (body tissue)
2450 MHz ConvF $4.3 \pm 8\%$
 $\epsilon_r = 52.7$
 $\sigma = 1.95 \text{ mho/m}$
 (body tissue)

Body 450MHz Liquid Validation, Ambient Temp = 23°C, Liquid Temp = 21°C, 6/21/03

frequency	e'	e''
400000000.0000	57.5419	38.0810
402000000.0000	57.5038	38.0074
404000000.0000	57.4069	38.0280
406000000.0000	57.3978	38.0670
408000000.0000	57.2122	37.9350
410000000.0000	57.2289	37.9087
412000000.0000	57.2416	37.8085
414000000.0000	57.2321	37.8265
416000000.0000	57.2279	37.7233
418000000.0000	57.1640	37.6652
420000000.0000	57.0797	37.6561
422000000.0000	56.9378	37.5576
424000000.0000	56.9524	37.4313
426000000.0000	56.8959	37.3892
428000000.0000	56.7846	37.2439
430000000.0000	56.6720	37.2157
432000000.0000	56.5434	37.2641
434000000.0000	56.4087	37.0549
436000000.0000	56.2332	36.9942
438000000.0000	56.1269	36.8832
440000000.0000	56.9235	36.8310
442000000.0000	56.8930	36.7404
444000000.0000	56.6851	36.7164
446000000.0000	56.5756	36.7042
448000000.0000	56.4269	36.6654
450000000.0000	56.2034	36.6941
452000000.0000	56.2340	36.1017
454000000.0000	56.2117	36.0265
456000000.0000	56.0821	36.0357
458000000.0000	56.9410	35.9613
460000000.0000	56.8405	35.8402
462000000.0000	56.6582	35.7667
464000000.0000	56.5663	35.6204
466000000.0000	56.4381	35.5754
468000000.0000	56.4375	35.5286
470000000.0000	56.2583	35.3903
472000000.0000	56.5039	35.3447
474000000.0000	56.7028	35.2373
476000000.0000	56.8482	35.1381
478000000.0000	56.8471	35.1325
480000000.0000	56.9365	35.0755
482000000.0000	56.8392	35.9634
484000000.0000	56.9961	35.0662
486000000.0000	57.0535	35.0615
488000000.0000	57.0241	35.0574
490000000.0000	57.1851	35.0711
492000000.0000	57.2021	35.0103
494000000.0000	57.1952	35.0283
496000000.0000	57.1918	35.0734
498000000.0000	57.2971	35.0576
500000000.0000	57.2705	35.0894

$$\sigma = \omega \epsilon_0 \epsilon'' = 2 \pi f \epsilon_0 \epsilon'' = 0.9186$$

where $f = 450$

$$\epsilon_0 = 8.854 \times 10^{-12}$$

$$\epsilon'' = 36.6941$$

Head 450MHz Liquid Validation, Ambient Temp = 23°C, Liquid Temp = 21°C, 6/21/03

frequency	e'	e''
400000000.0000	45.2315	36.2608
402000000.0000	45.2417	36.2740
404000000.0000	45.1256	36.0832
406000000.0000	45.1032	35.8220
408000000.0000	45.1096	35.7273
410000000.0000	44.4222	35.6790
412000000.0000	44.5486	35.5652
414000000.0000	44.8272	35.7827
416000000.0000	44.8289	35.4282
418000000.0000	44.6692	35.1592
420000000.0000	44.6173	34.9601
422000000.0000	44.4251	34.9134
424000000.0000	44.3426	34.7900
426000000.0000	44.3486	34.8898
428000000.0000	44.4665	34.6845
430000000.0000	44.0195	34.5353
432000000.0000	43.8738	34.4850
434000000.0000	43.8585	34.4106
436000000.0000	43.7204	34.3614
438000000.0000	43.7323	34.4181
440000000.0000	43.6832	34.2378
442000000.0000	43.6970	34.3032
444000000.0000	43.6956	34.2138
446000000.0000	43.5746	34.2057
448000000.0000	43.5837	34.2350
450000000.0000	44.1970	34.4722
452000000.0000	43.3953	34.0714
454000000.0000	42.3570	34.1660
456000000.0000	43.2130	34.1099
458000000.0000	43.2474	34.1613
460000000.0000	43.2569	34.1495
462000000.0000	43.1954	34.0912
464000000.0000	43.0758	34.1066
466000000.0000	43.0365	34.1189
468000000.0000	43.0816	34.0464
470000000.0000	43.0229	33.8955
472000000.0000	42.8922	33.9413
474000000.0000	42.9907	33.8058
476000000.0000	42.8658	33.7448
478000000.0000	42.7935	33.6800
480000000.0000	42.7046	33.5666
482000000.0000	42.7893	33.5552
484000000.0000	42.7334	33.4102
486000000.0000	42.7166	33.4143
488000000.0000	42.5751	33.3804
490000000.0000	42.6430	33.2631
492000000.0000	42.6483	33.1524
494000000.0000	42.6135	33.0729
496000000.0000	42.6625	32.9041
498000000.0000	42.6331	32.8746
500000000.0000	42.5711	32.8970

$$\sigma = \omega \epsilon_0 \epsilon'' = 2 \pi f \epsilon_0 \epsilon'' = 0.8629$$

where $f = 450$
 $\epsilon_0 = 8.854 \times 10^{-12}$
 $\epsilon'' = 34.4722$

3 - EUT DESCRIPTION

FCC ID:	Q5EPT320802
Applicant:	Kirisun Electronics (Shenzhen) Co., Ltd.
Product Description:	FM Handheld Transceiver (prototype)
Product Name:	PT3208(2)
Serial Number:	None
Transmitter Frequency:	450.0504 – 469.9504 MHz
Maximum Output Power:	4.14W
Dimension:	8.5" L x 1.1"W x 2.3"H approximately
RF Exposure environment:	Occupational Population
Applicable Standard	FCC CFR 47, Part 90
Application Type:	Certification

¹ Specific Absorption Rate (SAR) is a measure of the rate of energy absorption due to exposure to an RF transmitting source (wireless portable device).

² IEEE/ANSI Std. C95.1-1992 limits are used to determine compliance with FCC ET Docket 93-62.

Note: The test data was good for test sample only. It may have deviation for other test samples.

4 - SYSTEM TEST CONFIGURATION

4.1 Justification

The system was configured for testing in a typical fashion (as normally used by a typical user).

4.2 EUT Exercise Procedure

The EUT exercising program used during SAR testing was designed to exercise the various system components in a manner similar to a typical use. The EUT was tested by pushing the PTT bottom during the testing.

4.3 Special Accessories

All interface cables used for compliance testing are shielded as normally supplied by INMAC, Monster Cable and their respective support equipment manufacturer. The EUT is featured shielded metal connectors.

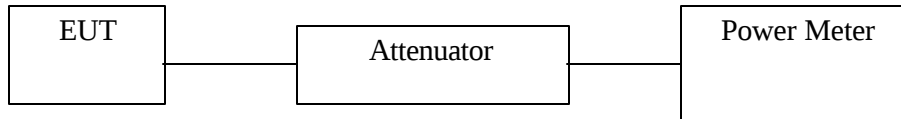
4.4 Equipment Modifications

No modification(s) were made to ensure that the EUT complies with the applicable limits.

5 - CONDUCTED OUTPUT POWER MEASUREMENT

5.1 Measurement Procedure

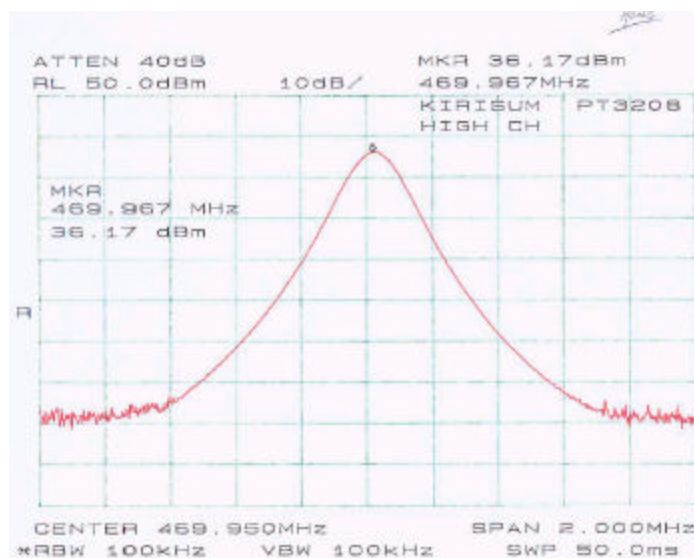
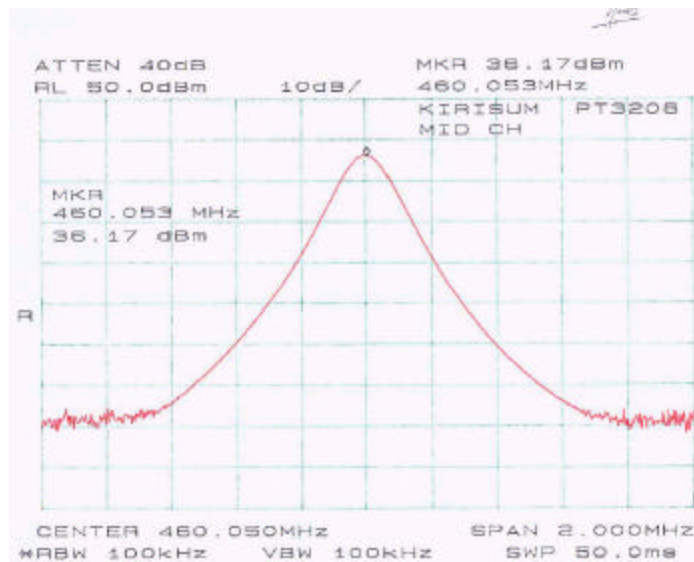
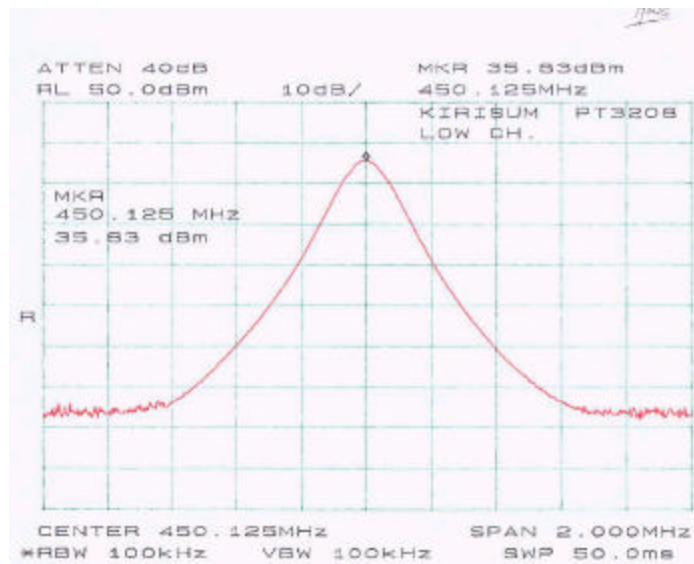
1. Place the EUT on a bench and set it in transmitting mode.
2. Remove the antenna from the EUT and then connect a low loss RF cable from the antenna port to a spectrum analyzer.
3. Add a correction factor to the display.



5.2 Test Results

Channel	Output Power in dBm	Output Power in W
450.125	35.83	3.83
460.053	36.17	4.14
469.967	36.17	4.14

Note: The power output may depend on the intended use of the EUT. For all tests, the EUT was set to maximum conditions.



6 - DOSIMETRIC ASSESSMENT SETUP

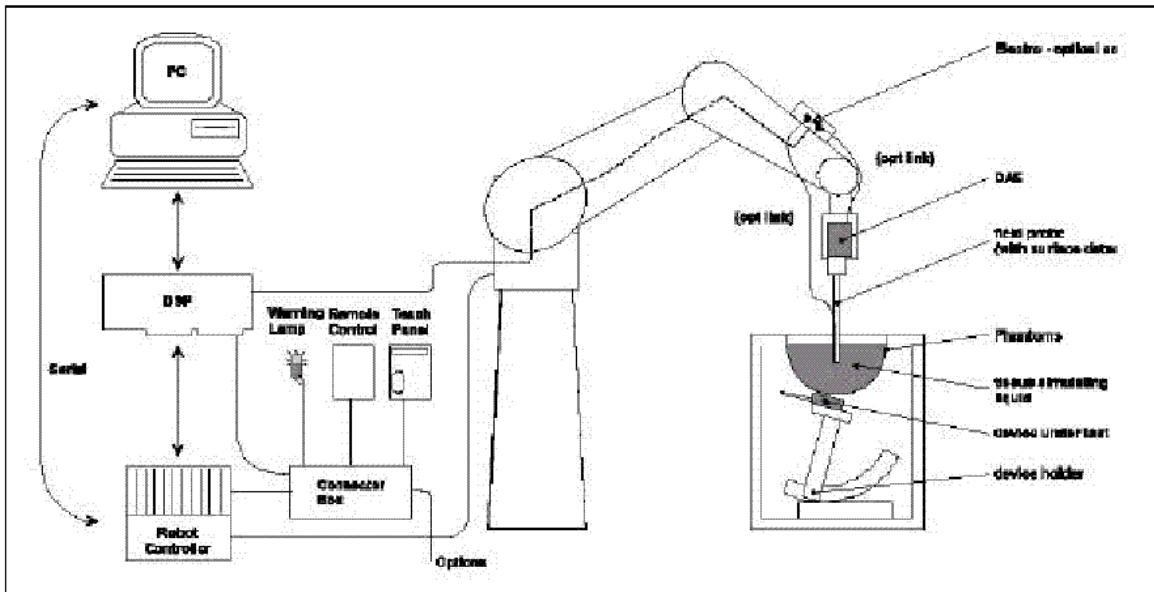
These measurements were performed with the automated near-field scanning system DASY3 from Schmid & Partner Engineering AG (SPEAG). The system is based on a high precision robot (working range greater than 0.9m) which positions the probes with a positional repeatability of better than $\pm 0.02\text{mm}$. Special E- and H-field probes have been developed for measurements close to material discontinuity, the sensors of which are directly loaded with a Schottky diode and connected via highly resistive lines to the data acquisition unit. The system is described in detail in [3].

The SAR measurements were conducted with the dosimetric probe ET3DV6 SN: 1604 (manufactured by SPEAG), designed in the classical triangular configuration [3] and optimized for dosimetric evaluation. The probe has been calibrated according to the procedure described in [7] with accuracy of better than $\pm 10\%$. The spherical isotropy was evaluated with the procedure described in [8] and found to be better than $\pm 0.25\text{dB}$.

The phantom used was the "Generic Twin Phantom" described in [4]. The ear was simulated as a spacer of 4 mm thickness between the earpiece of the phone and the tissue simulating liquid. The Tissue simulation liquid used for each test is in according with the FCC OET65 supplement C as listed below.

Ingredients (% by weight)	Frequency (MHz)									
	450		835		915		1900		2450	
Tissue Type	Head	Body	Head	Body	Head	Body	Head	Body	Head	Body
Water	38.56	51.16	41.45	52.4	41.05	56.0	54.9	40.4	62.7	73.2
Salt (Nacl)	3.95	1.49	1.45	1.4	1.35	0.76	0.18	0.5	0.5	0.04
Sugar	56.32	46.78	56.0	45.0	56.5	41.76	0.0	58.0	0.0	0.0
HEC	0.98	0.52	1.0	1.0	1.0	1.21	0.0	1.0	0.0	0.0
Bactericide	0.19	0.05	0.1	0.1	0.1	0.27	0.0	0.1	0.0	0.0
Triton x-100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	36.8	0.0
DGBE	0.0	0.0	0.0	0.0	0.0	0.0	44.92	0.0	0.0	26.7
Dielectric Constant	43.42	58.0	42.54	55.2	42.0	55.9	39.9	53.3	39.8	53.6
Conductivity (s/m)	0.85	0.83	0.91	0.97	1.0	0.98	1.42	1.52	1.88	1.81

6.1 Measurement System Diagram



The DAS3 system for performing compliance tests consist of the following items:

1. A standard high precision 6-axis robot (Stäubli RX family) with controller and software.
2. An arm extension for accommodating the data acquisition electronics (DAE).
3. A dosimetric probe, i.e., an isotropic E-field probe optimized and calibrated for usage in tissue simulating liquid. The probe is equipped with an optical surface detector system.
4. A data acquisition electronic (DAE), which performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. The unit is battery powered with standard or rechargeable batteries. The signal is optically transmitted to the EOC.
5. A unit to operate the optical surface detector, which is connected to the EOC. The Electro-optical coupler (EOC) performs the conversion from the optical into a digital electric signal of the DAE. The EOC is connected to the PC plug-in card. The functions of the PC plug-in card based on a DSP is to perform the time critical task such as signal filtering, surveillance of the robot operation fast movement interrupts.
6. A computer operating Windows 95 or larger
7. DAS3 software
8. Remote control with teaches pendant and additional circuitry for robot safety such as warning lamps, etc.
9. The generic twin phantom enabling testing left-hand and right-hand usage.
10. The device holder for handheld EUT.
11. Tissue simulating liquid mixed according to the given recipes (see Application Note).
12. System validation dipoles to validate the proper functioning of the system.

6.2 System Components

ET3DV6 Probe Specification

Construction Symmetrical design with triangular core

Built-in optical fiber for surface detection System

Built-in shielding against static charges

Calibration In air from 10 MHz to 2.5 GHz

In brain and muscle simulating tissue at

Frequencies of 450 MHz, 900 MHz and

1.8 GHz (accuracy $\pm 8\%$)

Frequency 10 MHz to > 6 GHz; Linearity: ± 0.2 dB

(30 MHz to 3 GHz)

Directivity ± 0.2 dB in brain tissue (rotation around probe axis)

± 0.4 dB in brain tissue (rotation normal probe axis)

Dynamic 5 mW/g to > 100 mW/g;

Range Linearity: ± 0.2 dB

Surface ± 0.2 mm repeatability in air and clear liquids

Detection over diffuse reflecting surfaces.

Dimensions Overall length: 330 mm

Tip length: 16 mm

Body diameter: 12 mm

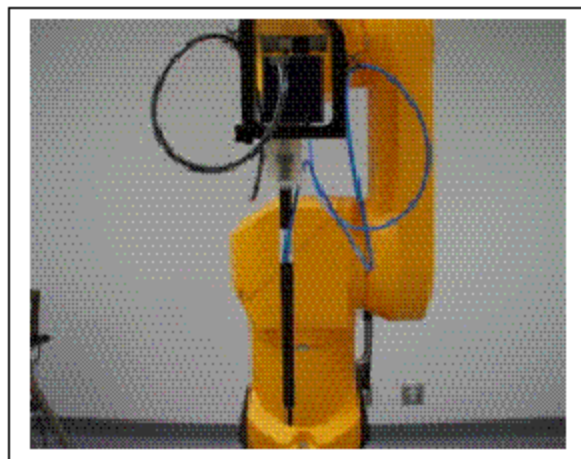
Tip diameter: 6.8 mm

Distance from probe tip to dipole centers: 2.7 mm

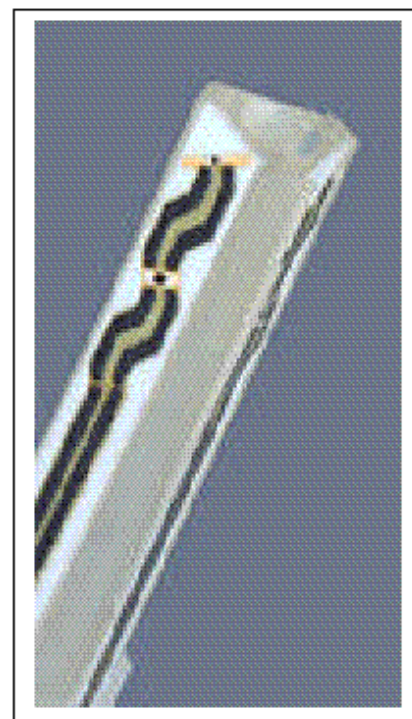
Application General dosimetric up to 3 GHz

Compliance tests of mobile phones

Fast automatic scanning in arbitrary phantoms



Photograph of the probe



Inside view of
ET3DV6 E-field Probe

The SAR measurements were conducted with the dosimetric probe ET3DV6 designed in the classical triangular configuration and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multi-fiber line ending at the front of the probe tip. It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY3 software reads the reflection during a software approach and looks for the maximum using a 2nd order fitting. The approach is stopped when reaching the maximum.

E-Field Probe Calibration Process

Each probe is calibrated according to a dosimetric assessment procedure described in [6] with accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure described in [7] and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe are tested.

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies below 1 GHz, and in a waveguide above 1 GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity and at the proper orientation with the field. The probe is then rotated 360 degrees.

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium correlates to temperature rise in dielectric medium. For temperature correlation calibration a RF transparent thermistor-based temperature probe is used in conjunction with the E-field probe.

Data Evaluation

The DASY3 software automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software:

Probe Parameter:	-Sensitivity	Norm _i , a _{i0} , a _{i1} , a _{i2}
	-Conversion Factor	ConvFi
	-Diode compression point	Dcp _i
Device parameter:	-Frequency	f
	-Crest Factor	cf
Media parameter:	-Conductivity	ó
	-Density	ñ

These parameters must be set correctly in the software. They can either be found in the component documents or be imported into the software from the configuration files issued for the DASY3 components. In the direct measuring mode of the multi-meter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as:

$$V_i = U_i + (U_i)^2 \text{ cf} / \text{dcp}_i$$

With V_i = compensated signal of channel i (i =x, y, z)
 U_i = input signal of channel i (i =x, y, z)
 cf = crest factor of exciting field (DASY parameter)
 dcp_i = diode compression point (DASY parameter)

From the compensated input signals the primary field data for each channel can be evaluated:

$$\begin{aligned} \text{E-field probes:} \quad E_i &= \sqrt{\frac{V_i}{\text{Norm}_i \cdot \text{ConvF}}} \\ \text{H-field probes:} \quad H_i &= \sqrt{V_i} \cdot \frac{a_{i0} + a_{i1}f + a_{i2}f^2}{f} \end{aligned}$$

With V_i = compensated signal of channel i (i = x, y, z)
 Norm_i = sensor sensitivity of channel i (i = x, y, z)
 $\text{V}/(\text{V}/\text{m})^2$ for E-field probes
 ConvF = sensitivity enhancement in solution
 a_{ij} = sensor sensitivity factors for H-field probes
 f = carrier frequency [GHz]
 E_i = electric field strength of channel i in V/m
 H_i = diode compression point (DASY parameter)

The RSS value of the field components gives the total field strength (Hermitian magnitude):

$$E_{\text{tot}} = \text{Square Root} [(E_x)^2 + (E_y)^2 + (E_z)^2]$$

The primary field data are used to calculate the derived field units.

$$\text{SAR} = (E_{\text{tot}})^2 \cdot \sigma / (\tilde{n} \cdot 1000)$$

With SAR = local specific absorption rate in mW/g
 E_{tot} = total field strength in V/m
 σ = conductivity in [mho/m] or [Siemens/m]
 $\tilde{n}$ = equivalent tissue density in g/cm^3

Note that the density is normally set to 1 (or 1.06), to account for actual brain density rather than the density of the simulation liquid.

The power flow density is calculated assuming the excitation field as a free space field.

$$P_{\text{pwe}} = (E_{\text{tot}})^2 / 3770 \text{ or } P_{\text{pwe}} = (H_{\text{tot}})^2 \cdot 37.7$$

With P_{pwe} = equivalent power density of a plane wave in mW/cm^3
 E_{tot} = total electric field strength in V/m
 H_{tot} = total magnetic field strength in V/m

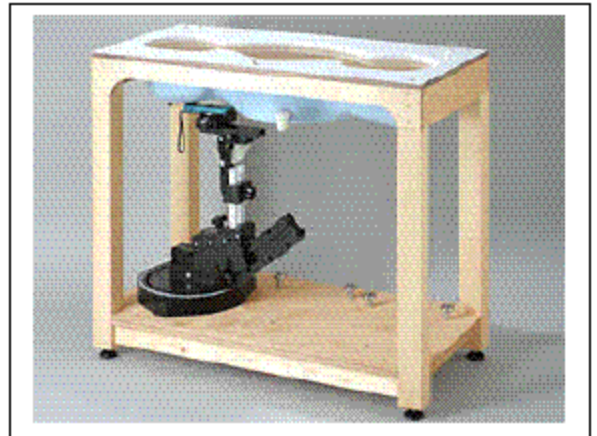
Generic Twin Phantom

The Generic Twin Phantom is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least 90% of all users [9][10]. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid. Reference markings on the Phantom allows the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot.

Shell Thickness 2 ± 0.1 mm

Filling Volume Approx. 20 liters

Dimensions 810 x 1000 x 500 mm (H x L x W)

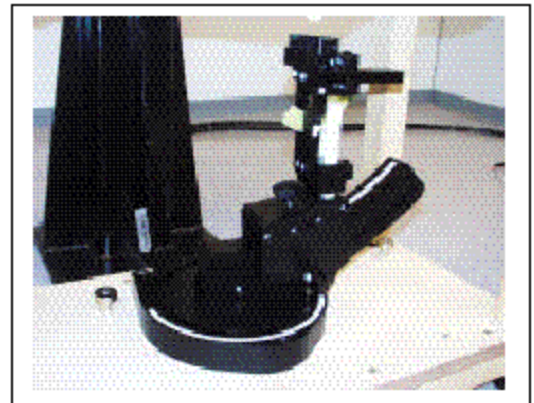


Generic Twin Phantom

Device Holder

In combination with the Generic Twin Phantom V3.0, the Mounting Device enables the rotation of the mounted transmitter in spherical coordinates whereby the rotation points is the ear opening. The devices can be easily, accurately, and repeatedly positioned according to the FCC and CENELEC specifications. The device holder can be locked at different phantom locations (left head, right head, flat phantom).

* Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produced infinite number of configurations [10]. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.



Device Holder

6.3 Measurement Uncertainty

The uncertainty budget has been determined for the DASY3 measurement system according to the NIS81 [13] and the NIST1297 [14] documents and is given in the following Table.

Measurement Uncertainty Analysis per IEEE P1528-2002								
Description	Section	Reported Variance (%)	Probability Distributio n type	Divisor	Ci (1g)	Ui (1g)	Vi	welc/satt series term
Probe Calibration	E.2.1	4.80	N	1	1	4.80	1.00E+09	5.30842E-07
Axial isotropy	E.2.2	4.70	R	1.732	0.707107	1.92	1.00E+09	1.35563E-08
Hemispherical isotropy	E.2.2	9.60	R	1.732	0.707107	3.92	1.00E+09	2.35957E-07
Boundary effects	E.2.3	8.30	R	1.732	1	4.79	1.00E+09	5.27377E-07
Linearity	E.2.4	4.70	R	1.732	1	2.71	1.00E+09	5.4225E-08
System Detection Limit	E.2.5	1.00	R	1.732	1	0.58	1.00E+09	1.11124E-10
Readout Electronics	E.2.6	0.00	N	1	1	0.00	1.00E+09	0
Response time	E.2.7	0.00	R	1.732	1	0.00	1.00E+09	0
Integration time	E.2.8	0.00	R	1.732	1	0.00	1.00E+09	0
RF Ambient conditions	E.6.1	3.00	R	1.732	1	1.73	1.00E+09	9.00106E-09
Probe positioning mechanical tolerance	E.6.2	0.40	R	1.732	1	0.23	1.00E+09	2.84478E-12
Probe positioning wrt phantom shell	E.6.3	2.90	R	1.732	1	1.67	1.00E+09	7.8596E-09
Extra/inter-polation & integration algorithms for max SAR evaluation	E.5.2	3.90	R	1.732	1	2.25	1.00E+09	2.57079E-08
Test sample positioning	8, E.4.2	6.00	R	1.732	1	3.46	1.00E+09	1.44017E-07
Device holder distance tolerance	E.4.1	5.00	N	1	1	5.00	1.00E+09	0.000000625
Output power and SAR drift measurement	8, E.6.6.2	5.00	R	1.732	1	2.89	1.00E+09	6.94526E-08
Phantom uncertainty, shell thickness tolerance	E.3.1	4.00	R	1.732	1	2.31	1.00E+09	2.84478E-08
Liquid conductivity, deviation from target values	E.3.2	5.00	R	1.732	0.64	1.85	1.00E+09	1.16522E-08
Liquid conductivity, measurement uncertainty	E.3.3	5.00	N	1	0.64	3.20	5	20.97152
Liquid permittivity, deviation from target values	E.3.2	5.00	R	1.732	0.6	1.73	1.00E+09	9.00106E-09
Liquid permittivity, measurement uncertainty	E.3.3	5.00	N	1	0.6	3.00	5	16.2
								689
Probe isotropy sensitivity coefficient	0.5							
Combined Standard Uncertainty						12.65	%	
Expanded Uncertainty, 95% confidence		k=	2.004			25.34	%	

7 - SYSTEM EVALUATION

7.1 Simulated Tissue Liquid Parameter Confirmation

The dielectric parameters were checked prior to assessment using the HP85070A dielectric probe kit. The dielectric parameters measured are reported in each correspondent section:

7.2 Evaluation Procedures

Maximum Search

The maximum search is automatically performed after each coarse scan measurement. It is based on splines in two or three dimensions. The procedure can find the maximum for most SAR distributions even with relatively large grid spacings. After the coarse scan measurement, the probe is automatically moved to a position at the interpolated maximum. The following scan can directly use this position for reference, e.g., for a finer resolution grid or the cube evaluations.

Extrapolation

The extrapolation can be used in z-axis scans with automatic surface detection. The SAR values can be extrapolated to the inner phantom surface. The extrapolation distance is the sum of the probe sensor offset, the surface detection distance and the grid offset. The extrapolation is based on fourth order polynomial functions. The extrapolation is only available for SAR values.

Boundary Corrections

The correction of the probe boundary effect in the vicinity of the phantom surface can be done in two different ways. In the standard (worse case) evaluation, the boundary effect is reduced by different weights for the lowest measured points in the extrapolation routine. The result is a slight overestimation of the extrapolated SAR values (2% to 8%) depending on the SAR distribution and gradient. The advanced evaluation makes a full compensation of the boundary effect before doing the extrapolation. This is only possible of probes with specifications on the boundary effect.

Peak Search for 1g and 10g cube averaged SAR

The 1g and 10g peak evaluations are only available for the predefined cube 4x4x7 and cube 5x5x7 scans. The routine are verified and optimized for the grid dimensions used in these cube measurements. The measured volume of 32x32x35mm contains about 35g of tissue. The first procedure is an extrapolation (incl. Boundary correction) to get the points between the lowest measured plane and the surface. The next step uses 3D interpolation get all points within the measured volume in a 1mm grid (35000 points). In the last step, a 1g cube is place numerically into the volume and its averaged SAR is calculated. This cube is the moved around until the highest averaged SAR is found. This last procedure is repeated for a 10g cube. If the highest SAR is found at the edge of the measured volume, the system will issue a warning,; higher SAR values might be found outside of the measured volume. In that case the cube measurement can be repeated, using the new interpolated maximum as the center.

7.3 System Accuracy Verification

Prior to the assessment, the system validation kit was used to test whether the system was operating within its specifications of $\pm 10\%$. The validation results are tabulated below. And also the corresponding SAR plot is attached as well in the SAR plots files.

IEEE P1528 recommended reference value

Frequency (MHz)	1 g SAR	10 g SAR	Local SAR at surface (above feed point)	Local SAR at surface (v=2cm offset from feed point)
300	3.0	2.0	4.4	2.1
450	4.9	3.3	7.2	3.2
835	9.5	6.2	14.1	4.9
900	10.8	6.9	16.4	5.4
1450	29.0	16.0	50.2	6.5
1800	38.1	19.8	69.5	6.8
1900	39.7	20.5	72.1	6.6
2000	41.1	21.1	74.6	6.5
2450	52.4	24.0	104.2	7.7
3000	63.8	25.7	140.2	9.5

Validation Dipole SAR Reference Test Result for Body (450 MHz)

Validation Measurement	SAR @ 9.225mW Input averaged over 1g	SAR @ 1W Input averaged over 1g	SAR @ 9.225mW Input averaged over 10g	SAR @ 1W Input averaged over 10g
Test 1	0.0451	0.89	0.0315	3.4
Test 2	0.0447	4.85	0.0312	3.38
Test 3	0.0448	4.86	0.0313	3.39
Test 4	0.0450	4.88	0.0313	3.39
Test 5	0.0451	4.89	0.0313	3.39
Test 6	0.0450	4.88	0.0315	3.4
Test 7	0.0451	4.89	0.0314	3.4
Test 8	0.0449	4.87	0.0312	3.38
Test 9	0.0449	4.87	0.0312	3.38
Test 10	0.0448	4.86	0.0311	3.37
Average	0.0449	4.874	0.0313	3.388

System validation result

4/29/03

Ambient Temperature (°C): 23.0

Relative Humidity (%): 49.3

Simulant	Freq [MHz]	Parameters	Liquid Temp [°C]	Target Value	Measured Value	Deviation [%]	Limits [%]
Body	450	ϵ	21	56.7	56.2	-0.88	± 5
		σ	21	0.94	0.92	-2.13	± 5
		1g SAR	21	4.874	4.82	-1.11	± 10
Head	450	ϵ	21	43.5	44.2	1.61	± 5
		σ	21	0.87	0.86	-1.15	± 5
		1g SAR	21	4.9	4.80	-2.04	± 10

ϵ = relative permittivity, σ = conductivity and $\rho=1000\text{kg/m}^3$

Note: Forward power = 25.5dBm = 354.8mW (body)

Forward power = 24.89dBm = 308.32mW (head)

450 MHz Body Liquid (Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

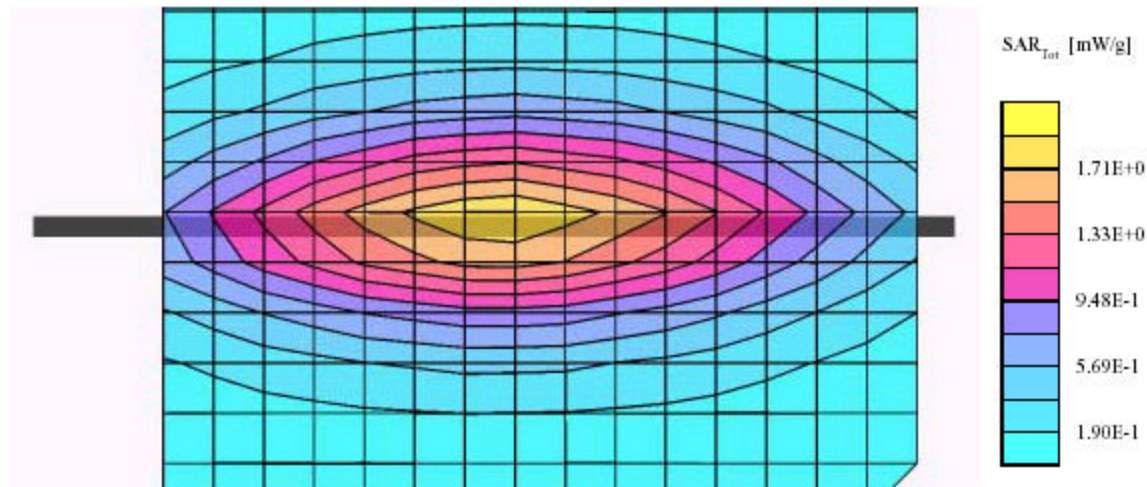
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 450 MHz

Probe: ET3DV6 - SN1604; ConvF(7.70,7.70,7.70); Crest factor: 1.0; (Head liquid) 450 MHz: $\sigma = 0.92 \text{ mho/m}$, $\epsilon_r = 56.2$, $\rho = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 1.71 mW/g, SAR (10g): 1.14 mW/g, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.00 dB



450 MHz Head Liquid (Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

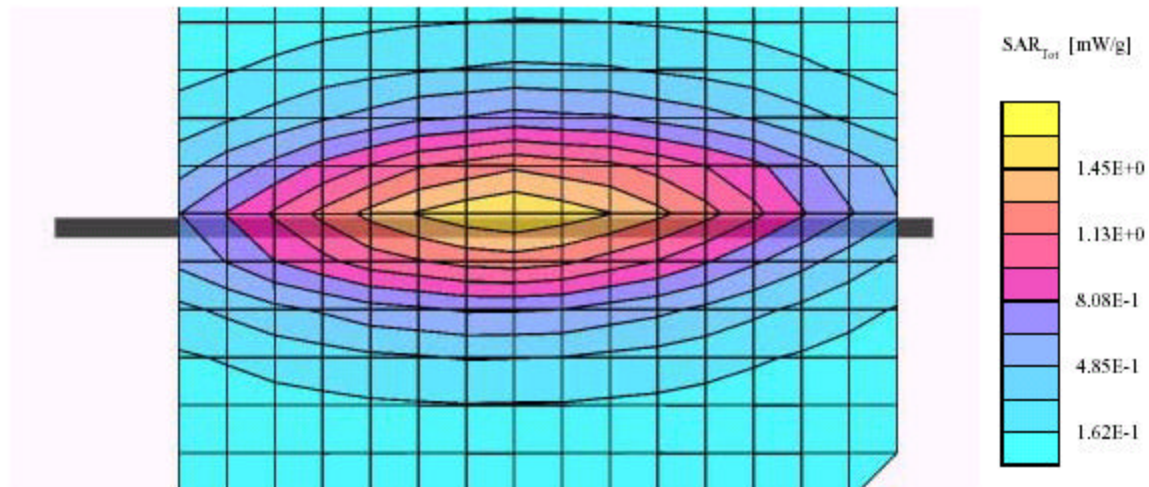
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 450 MHz

Probe: ET3DV6 - SN1604; ConvF(7.30,7.30,7.30); Crest factor: 1.0; (Head liquid) 450 MHz: $\sigma = 0.86 \text{ mho/m}$, $\epsilon_r = 44.2$ $\rho = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 1.48 mW/g, SAR (10g): 0.963 mW/g, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: 0.01 dB



7.4 SAR Evaluation Procedure

- a. The evaluation was performed in the applicable area of the phantom depending on the type of device being tested. For device held to the head during normal operation, both the left and right ear positions were evaluated in accordance with FCC OET Bulletin 65, Supplement C (Edition 01-01) using the SAM phantom. For body-worn and face-held devices a planar phantom was used. The EUT in the test setup for body-worn and face-held devices was placed in three different positions (relative to the phantom): with belt clip, without belt clip and 2.5cm facing left head side and 2.5cm facing right head side.
- b. The SAR was determined by a pre-defined procedure within the DASY3 software. Upon completion of a reference and optical surface check, the exposed region of the phantom was scanned near the inner surface with a grid spacing of 20mm x 20mm.
- c. A 5x5x7 matrix was performed around the greatest special SAR distribution found during the area scan of the applicable exposed region. SAR values were then calculated using a 3-D spline interpolation algorithm and averaged over spatial volumes of 1 and 10 grams.
- d. The depth of the simulating tissue in the planar used for the SAR evaluation and system validation was no less than 15.0cm.
- e. For this particular evaluation, a stack of low-density, low-loss dielectric foamed polystyrene was used in place of the device holder.
- f. Re-measurement of the SAR value at the same location as in a. If the value changed by more than 5%, the evaluation was repeated.

7.5 Exposure Limits

Table 1: Limits for Occupational/Controlled Exposure (W/kg)

Whole-Body	Partial-Body	Hands. Wrists. Feet and Ankles
0.4	8.0	20.0

Table 2: Limits for General Population/Uncontrolled Exposure (W/kg)

Whole-Body	Partial-Body	Hands. Wrists. Feet and Ankles
0.08	1.6	4.0

Note: Whole-body SAR is averaged over the entire body, partial-body SAR is averaged over any 1 gram of tissue defined as a tissue volume in the shape of a cube SAR for hands, wrists, feet and ankles is averaged over any 10 grams of tissue defined as a tissue volume in the shape of a cube.

Population/Uncontrolled Environments are defined as locations where there is the exposure of individual who have no knowledge or control of their exposure.

Occupational/Controlled Environments are defined as locations where there is exposure that may be incurred by people who are aware of the potential for exposure (i.e. as a result of employment or occupation).

Population/uncontrolled environments Partial-body limit 1.6W/kg applied to the EUT.

8 - TEST RESULTS

This page summarizes the results of the performed dosimetric evaluation. The plots with the corresponding SAR distributions, which reveal information about the location of the maximum SAR with respect to the device could be found in the following pages.

According to the data in section 8.1, the EUT complied with the FCC 2.1093 RF Exposure standards, with worst case of **4.89mW/g**.

8.1 SAR Test Data

Ambient Temperature (°C): 23.0

Relative Humidity (%): 51.1

Worst case SAR reading

EUT position	Frequency (MHz)	Conducted Power (W)	Test Type	Antenna Type	Liquid	Phantom	Notes / Accessories	Measured (mW/g)		Limit (mW/g)	Plot #
								100% duty cycle	50% duty cycle		
back in touch with phantom	450	3.83	Body worn	Built-in	body	flat	headset	8.43	4.215	8	1
back in touch with phantom	460	4.14	Body worn	Built-in	body	flat	headset	9.78	4.89	8	2
back in touch with phantom	470	4.14	Body worn	Built-in	body	flat	headset	9.54	4.77	8	3
2.5 cm head separation to phantom	450	3.83	Face-held	Built-in	head	flat	none	8.21	4.11	8	4
2.5 cm head separation to phantom	460	4.14	Face-held	Built-in	head	flat	none	8.52	4.26	8	5
2.5 cm head separation to phantom	470	4.14	Face-held	Built-in	head	flat	none	6.56	3.28	8	6

8.2 Plots of Test Result

The plots of test result were attached as reference.

Kirisun, PT3208 (2) (Back in touch to flat phantom with headset, Low channel, Ambient

Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

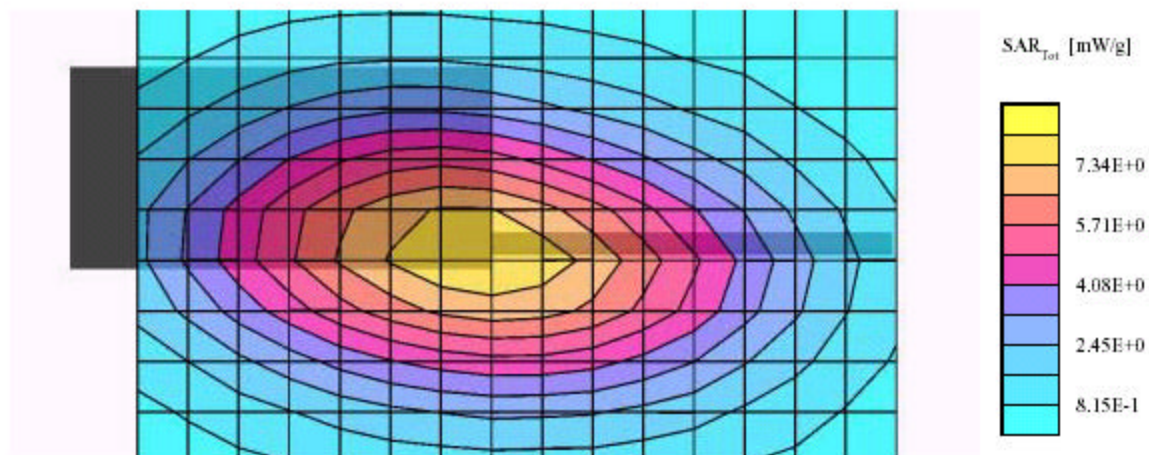
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 450 MHz

Probe: ET3DV6 - SN1604; ConvF(7.70,7.70,7.70); Crest factor: 1.0; (Body liquid) 450 MHz: $\sigma = 0.92 \text{ mho/m}$ $\epsilon_r = 56.2$ $\rho = 1.00 \text{ g/cm}^3$

Cubes (2): SAR (1g): $8.43 \text{ mW/g} \pm 1.44 \text{ dB}$, SAR (10g): $5.78 \text{ mW/g} \pm 1.76 \text{ dB}$, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.03 dB



Plot #1

Kirisun, PT3208 (2) (Back in touch to flat phantom with headset, Middle channel, Ambient

Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

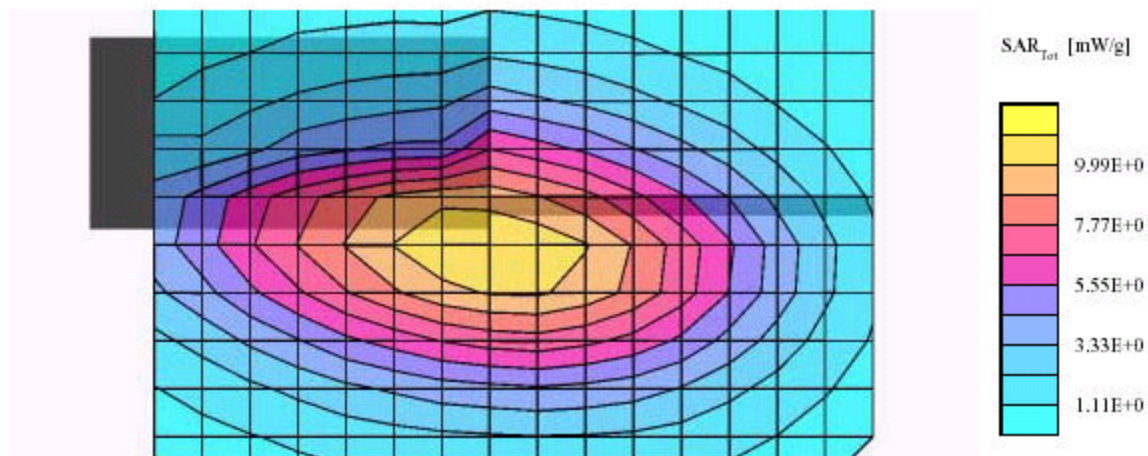
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 460 MHz

Probe: ET3DV6 - SN1604; ConvF(7.70,7.70,7.70); Crest factor: 1.0; (Body liquid) 450 MHz: $\sigma = 0.92 \text{ mho/m}$ $\epsilon_r = 56.2$ $\rho = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 9.78 mW/g, SAR (10g): 7.07 mW/g, (Worst-case extrapolation)

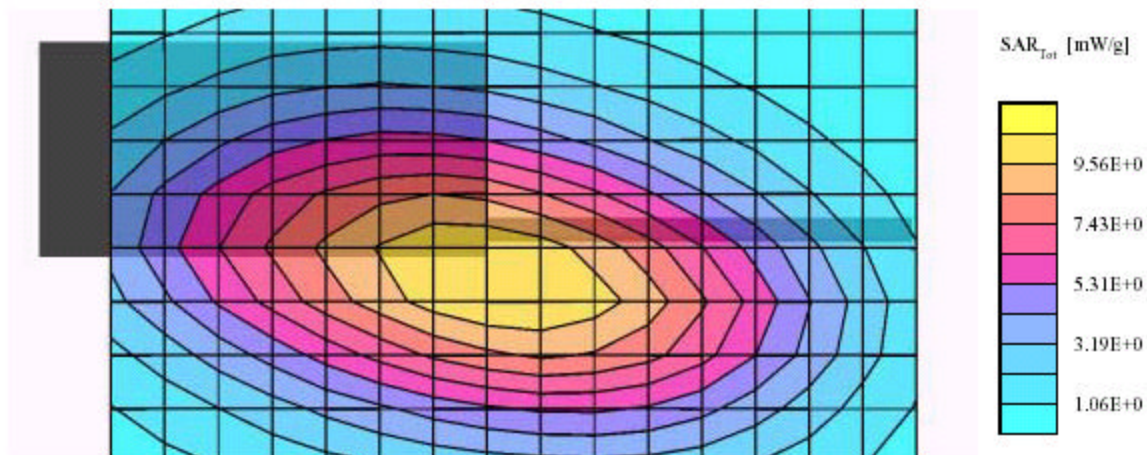
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.02 dB



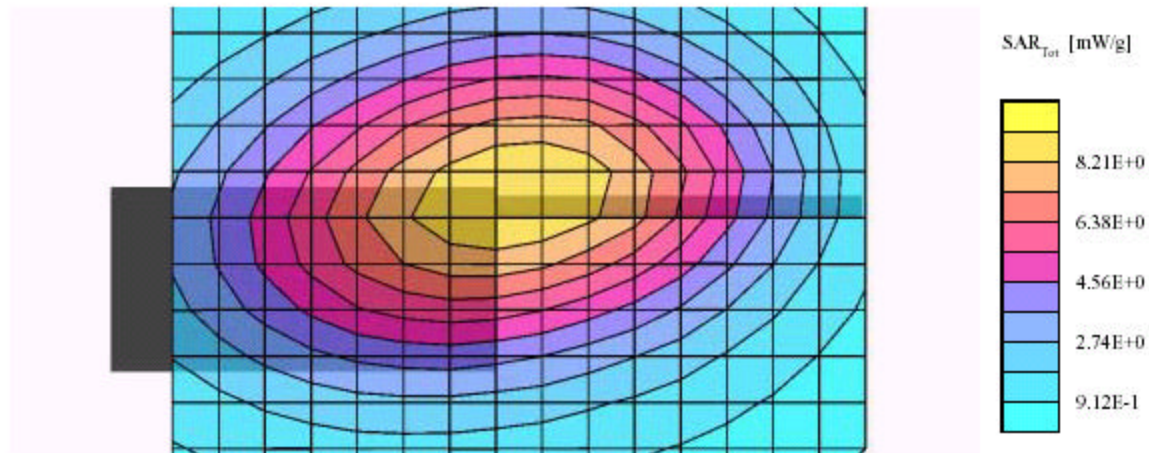
Plot #2

Kirisun, PT3208 (2) (Back in touch to flat phantom with headset, Middle channel, Ambient
Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/21/2003)
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 470 MHz
Probe: ET3DV6 - SN1604; ConvF(7.70,7.70,7.70); Crest factor: 1.0; (Body liquid) 450 MHz: $\sigma = 0.92 \text{ mho/m}$ $\epsilon_r = 56.2$ $\rho = 1.00 \text{ g/cm}^3$
Cube 5x5x7: SAR (1g): 9.54 mW/g, SAR (10g): 6.78 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.00 dB



Plot #3

Kirisun, PT3208 (2) (2.5 cm separation to flat phantom, Low channel, Ambient Temp = 23
Deg C, Liquid Temp = 22 Deg C, 6/21/2003)
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 450.12 MHz
Probe: ET3DV6 - SN1604; ConvF(7.30,7.30,7.30); Crest factor: 1.0; (Head liquid) 450 MHz: $\sigma = 0.86 \text{ mho/m}$, $\epsilon_r = 44.2$, $\rho = 1.00 \text{ g/cm}^3$
Cube 5x5x7: SAR (1g): 8.21 mW/g, SAR (10g): 5.85 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: -0.02 dB



Plot #4

Kirisun, PT3208 (2) (2.5 cm separation to flat phantom, Middle channel, Ambient Temp = 23

Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

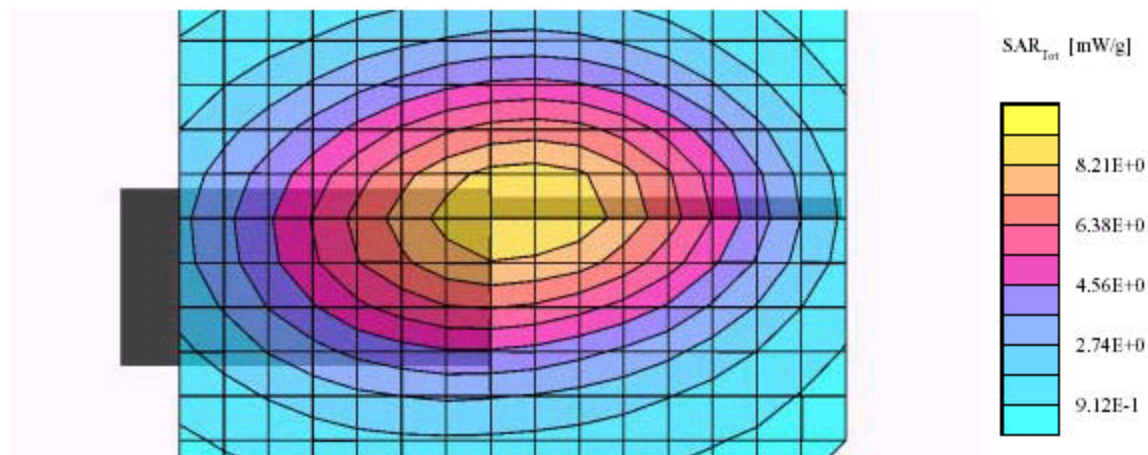
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 460.05 MHz

Probe: ET3DV6 - SN1604; ConvF(7.30,7.30,7.30); Crest factor: 1.0; (Head liquid) 450 MHz: $\sigma = 0.86$ mho/m $\epsilon_r = 44.2$ $\rho = 1.00$ g/cm³

Cubes (2): SAR (1g): 8.52 mW/g ± 0.38 dB, SAR (10g): 5.97 mW/g ± 0.33 dB, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.03 dB



Plot #5

Kirisun, PT3208 (2) (2.5 cm separation to flat phantom, High channel, Ambient Temp = 23

Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

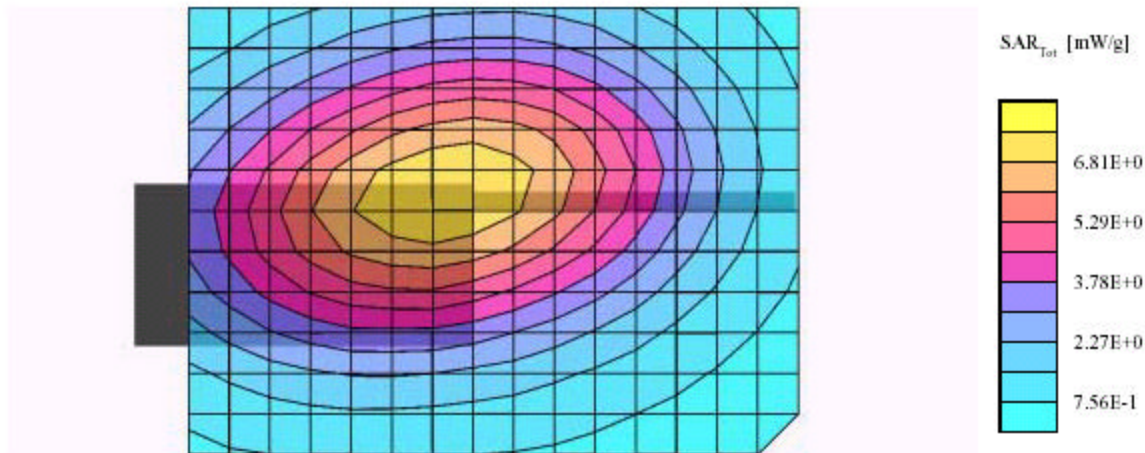
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 450 MHz

Probe: ET3DV6 - SN1604; ConvF(7.30,7.30,7.30); Crest factor: 1.0; (Head liquid) 450 MHz: $\sigma = 0.86 \text{ mho/m}$, $\epsilon_r = 44.2$, $\rho = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 6.56 mW/g, SAR (10g): 4.70 mW/g, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.02 dB



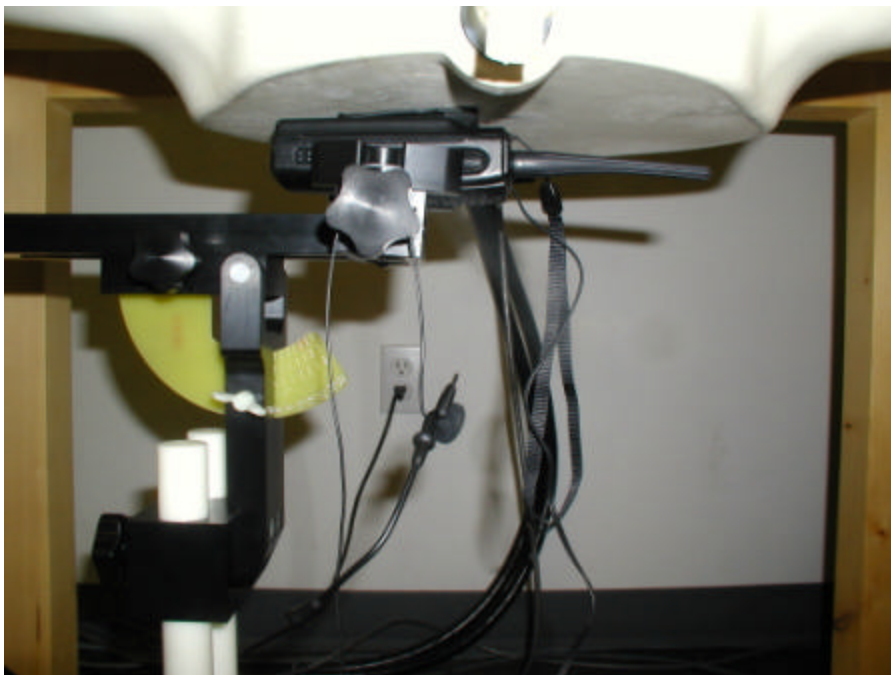
Plot #6

EXHIBIT A - SAR SETUP PHOTOGRAPHS

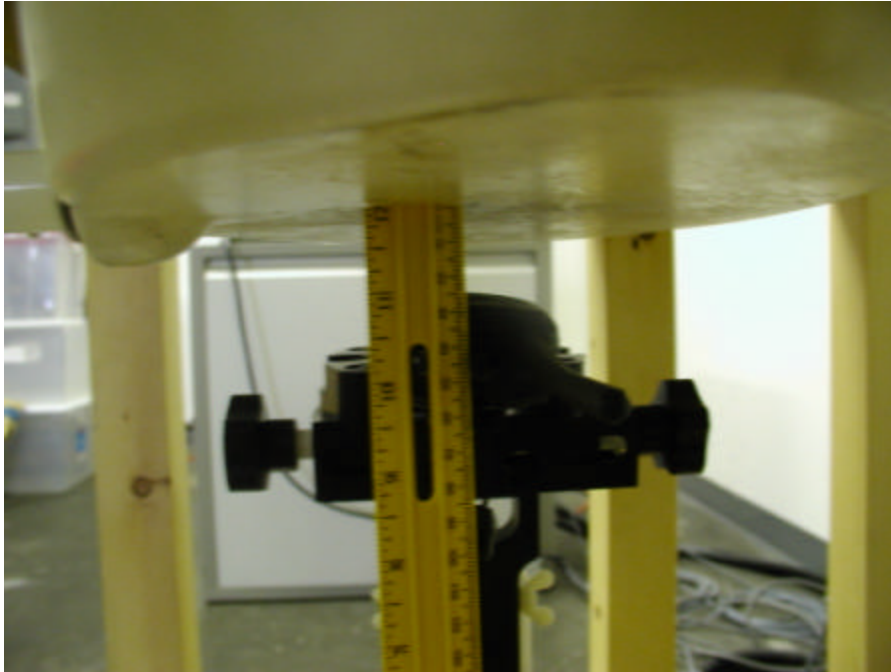
Back in Touch with Phantom with Headset – Front View



Back in Touch with Phantom with Headset – Side View



2.5cm Separation with Flat Phantom – Front View



2.5cm Separation with Flat Phantom – Side View



EXHIBIT B - EUT PHOTOGRAPHS

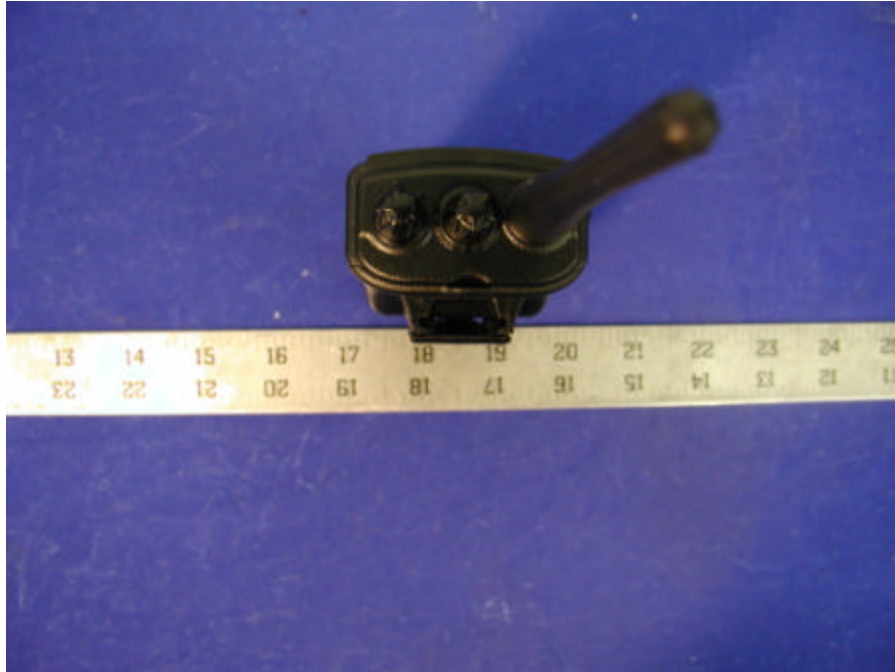
Chassis - Front View



Chassis – Rear View



Chassis – Top View



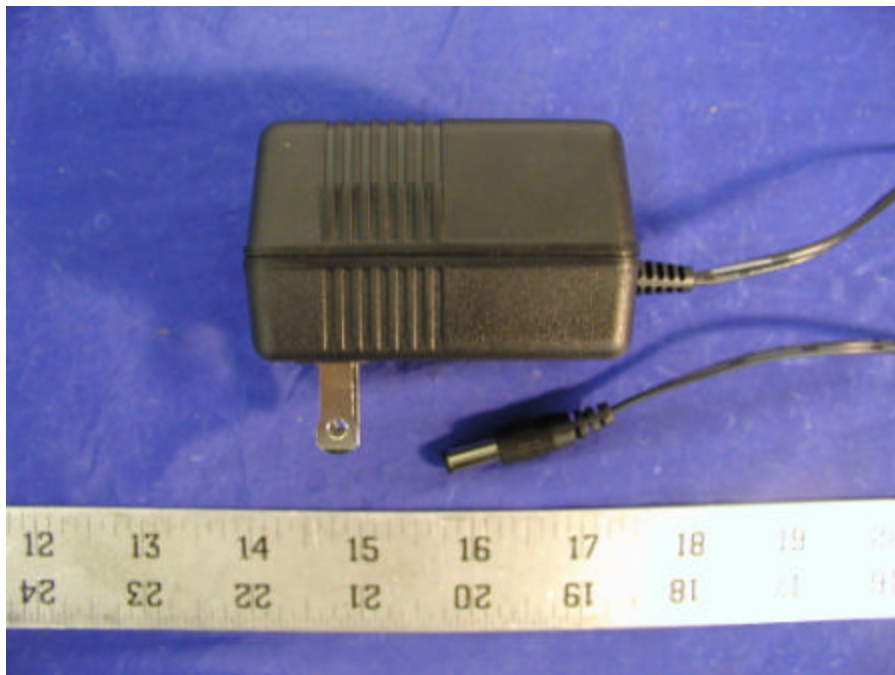
Chassis – Side View

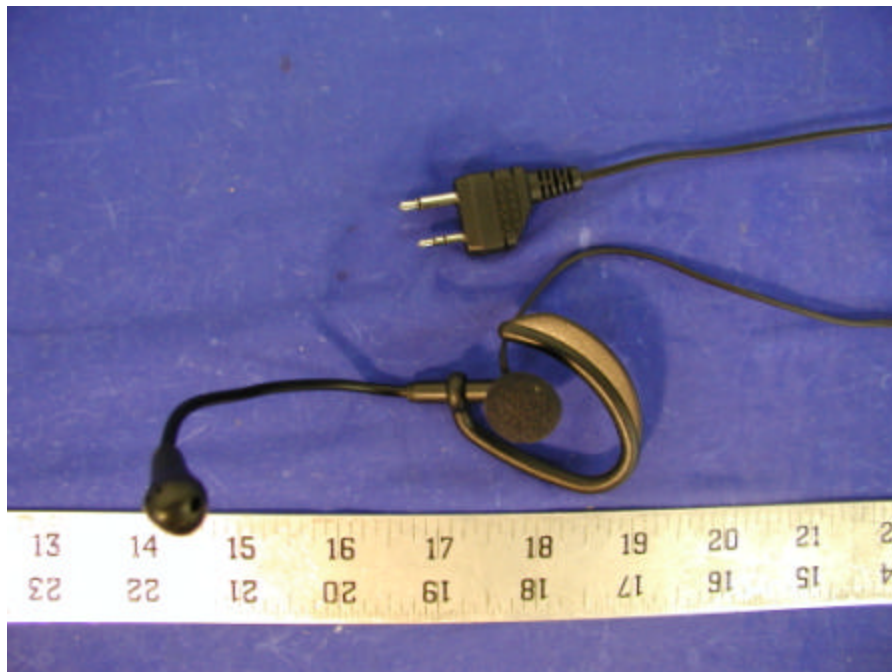


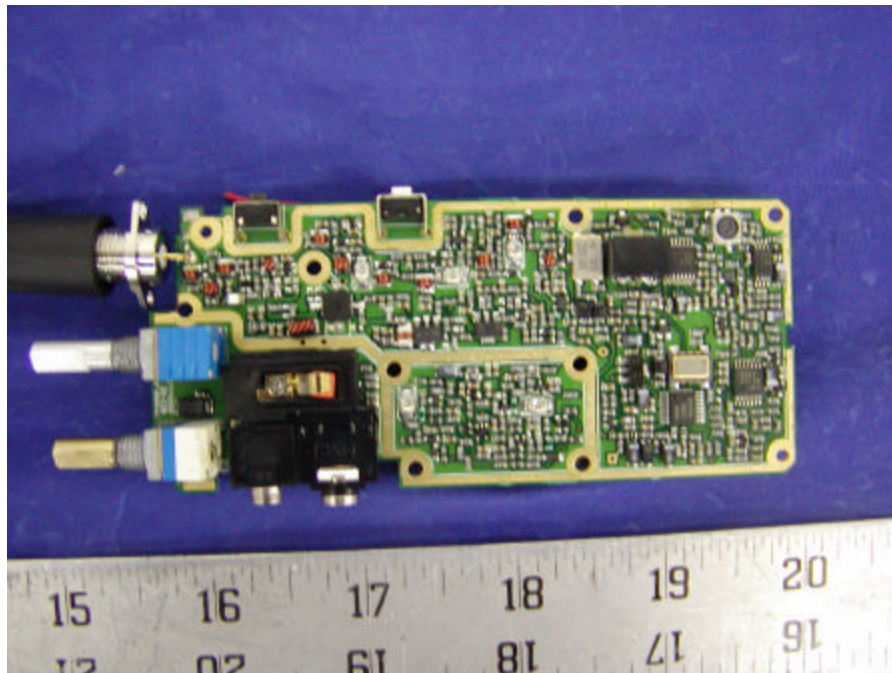
Antenna View



Power Adapter View



Power Charger View**Earphone and Microphone View**

Back Cover Off View**Board Component View**

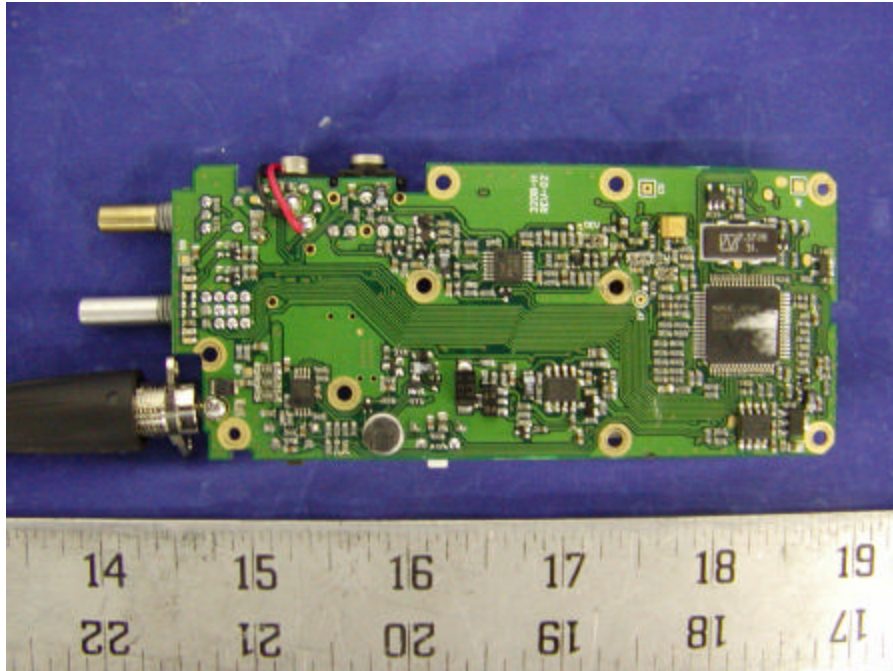
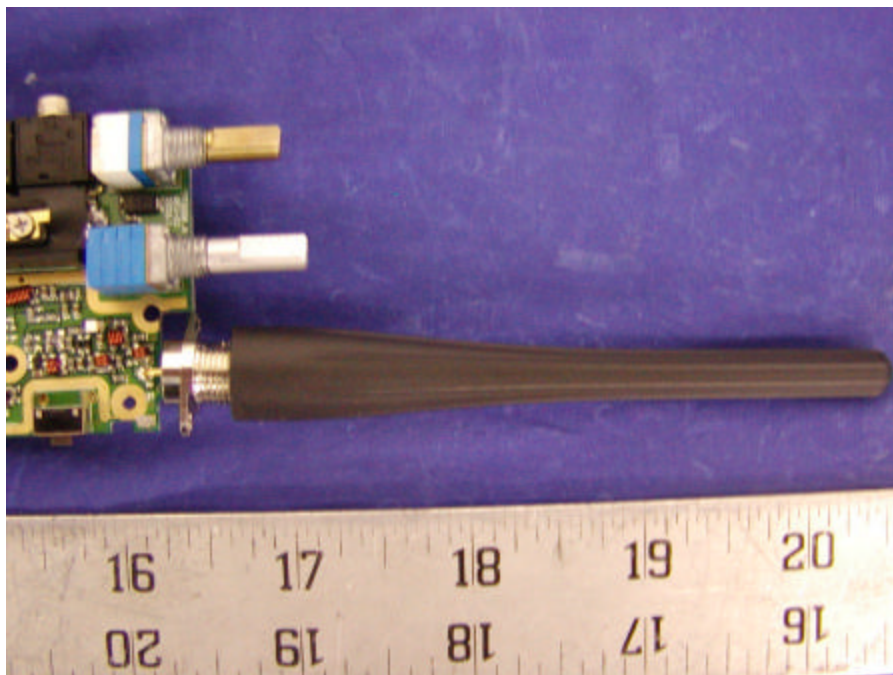
Board Solder View**Antenna Connection View**

EXHIBIT C – Z-Axis

Kirisun, PT3208 (2) (Back in touch to flat phantom with headset, Middle channel, Ambient
Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/21/2003)

SAM Phantom; Section; Position : Frequency: 470 MHz

Probe: ET3DV6 - SN1604; ConvF(7.70,7.70,7.70); Crest factor: 1.0; (Body liquid) 450 MHz: $\sigma = 0.92 \text{ mho/m}$ $\epsilon_r = 56.2$ $\rho = 1.00 \text{ g/cm}^3$

: , 0

Z-Axis: Dx = 0.0, Dy = 0.0, Dz = 2.0

